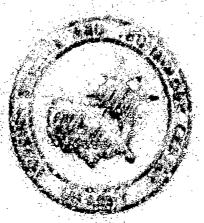
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Part I of the book (the only part included here) presents descriptions of the in-line and V-shaped engines, transmissions, transfer cases and drive axias of the III trucks. Presentation includes technical farvious, liz-assembly, repair and assembly of the components described. Also included in each section are tables presenting mominal and repair dissessions for all the parts of the various components, where

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Section I. Gameral Information on the Motor Vehicles

Chapter 1. Brisf technical characteristics of the motor vehicles

The ZIL-164A series of motor vehicles was produced by the plant in the period from 1962 to the end of 1954. The ZIL-104A was the change-over model Letween the ZIL-164 and the ZIL-136, whose production was begun at the end of 1964 and continues to the present time.

Production of the 3-axle cross-country ZIL-157K motor vehicle cyries was begun at the end of 1961. The 7IL-157K is also a change-over model between the ZIL-157 and the ZIL-131. The ZIL-157K is still being produced at the present time.

At the end of 1966, the plant began production of the ZIL-131, a new series of 3-axis cross-country motor vehicles.

The new ZIL-130 and ZIL-131 motor v hickes differ advantageously from the ZIL-164 and ZIL-157. Design of the new motor vehicles and the characteristics of their examplie's eignificantly improved: productivity, load capacity, dynamics, power reserve, and reliability of the motor; reliability of the transmission and running gear; improved working conditions for the driver, and decreased labor consumption in technical servicing. Improved terrese crossing capabilities and ability to ford streams should be added to the items listed for the cross-country vehicles.

A distinct paculiarity of the EIL-130 and EIL-131 vehicles is that their engine power and remembered design and running goars are rated for systematic operation of these motor vehicles as tractors with trailers and semi-erailers. Performance and over-all weight of tractor-trailer combinations are presented in appendices

3 and 6 (see Part 2).

The new motor vehicle models are naturally more complex than the old ones, and require higher skills in driving, technical maintanance and rapair

Specifications for the ZIL-130 and ZIL-131 motor vehicles were determined to a significant degree by the requirements of GOST (All-Union State Standard) 9314-59, which sot the allowable load limits for motor vehicle road beds. In this GOST, all motor vehicles and tractor-trailer combinations are broken down into groups according to axle load: group A and group B. Group A is intended for use on category I and II roads, allowing a maximum load on a single axle of ten tens, and group B is intended for use on all roads allowing a maximum load on a single axle of six tons (for group B dum,) trucks, a load of 6.5 tons is allowed). For tandsmidily axis carriages used on 3-axis motor vehicles with a distance between the carriage axis of less than three meters, a maximum load (on the tandem carriage) of 18 tons is allowed for group A transport means, and 11 tons is allowed for group B.

Por elimination of increased drive wheel skidding in 2-axle motor vehicles, it has been established that the optimum distribution of weight for a truck must be 30% on the front axle and 70% on the rear axle (see Appendix 3, Part 2).

At the beginning of its production, the ZIL-130 had a dual payload capacity: 5.5 and 4 tons, meaning that its payload capacity was equal to 5.5 tons when used on category 1 and II roads, and 4 tons on roads of the overall network. The weight of a towed trailer was equal to 6.4 tons. Later, beginning in 1966, with the special agreement of the Committee on Standards of the USSR Council of Ministers, in connection with the inconvenience caused by the dual payload capacity, the payload capacity for the single truck was set at 5 tons for all roads except category IV and V local use access roads. The weight of a lowed trailer was increased to 8 tons. In connection with this, the gross weight on the rear axle of a loaded truck of the ZIL-130 series was increased from 6 to 7 tons.

It should be noted that for 211-130 motor vehicles going out of the country, where allowable gross weight on a single axle is greater than 6 tons, the plant established psyload capacity at 6 tons (gross weight on the rear axle of a cargo truck in this case is equal to 8 tons).

Design features of the moror vehicles

The SIL-130 motor vehicle (Photo 1-1) is the basic model of the series of 2-axis cargo trucks with rear axis drive. It has a 1 X 2 wheel fermula and a whose base of 3800 ms. The truck is powered by the SIL-130 model 8-cylinder

Dimensions and weight data on the motor vehicle are presented in Appendix 4 (see Part 2), and characteristics of the assemblies are given in corresponding chapters.

V-shaped carbur¢ted engine, which has a maximum power of 150 hp. It has a single disk clutch and a five-speed transmission with two synchronizers for second-third and fourth-fifth gears. Fifth gear is straight drive. The steering mechanism is equipped with hydraulic power which is mounted in the mechanism itself. The truck has a confortable three-place all-metal cab with a wide panoramic windshield. The bed is a metal-wood combination. The truck is intended for continuous work with a trailer whose overall weight is 8 tons. The payload capacity of the initial model of the truck was 5.5-4 tons, overall trailer weight was 6.4 tons, and maximum speed was 85 kilometers per hour. In 1966, the ZIL-130 was designated ZIL-130-66. The base ZIL-130 model of 1966 production differs from the initial base model by a number of improved assemblies and parts, and also with an increased payload capacity of 5 tons and a trailer payload capacity of 5 tons (with a trailer gross weight of 8 tons). The GEP-817 trailer was a special creation for work with the ZIL-130 truck, and its bed disensions are as follows: length, 4700 mm; width, 2350 mm; and side height, 572 mm. Top speed of the truck was increased to 90 kilometers per hour.

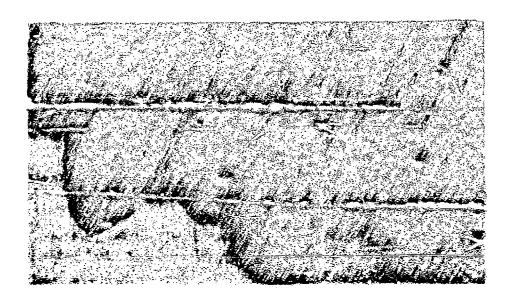


Plate 1-1 21L-130 truck

Improvement of essenties on the IIL-130 truck was conducted systematically by the plant; therefore, beginning in 1968, the plant designated the base truck as the IIL-130-68, although the external parameters of the technical specifications were not changed. The plant is also preparing introduction of a number of improvements for the corresponding IIL-130-70 truck.

The ZIL-IKVI truck (Plate 1-2) is a saddle tractor-truck, one of the modifications of the ZIL-130 truck series. Wheelbase is 3300 mm. The truck is intended for use with a semi-trailer, with an injtial overall weight of 10.5 tens, and beginning with output of the ZIL-136Vl-66 model, 12.4 tens. The truck differs from the base model by a short frame and Cardan drive, reduction year with a higher gear ratio, and absence of a bed, which is replaced by the saddle for connection with a trailer. The spare tire bracket is missing on the tractor-truck.

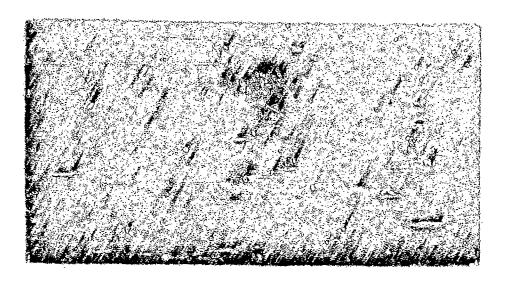


Plate 1-2. ZIL-130V1 (ZIL-130V1-66) saddle tractor-truck

The OdAZ-885 type semi-trailer, especially developed for work with the 21L-13OV1=65 tractor-truck, has a gross unight of 12.4 tons, and a payload capacity of 9 tons.

The ZIL-1306 truck (Place 1-3) is a long wheel base traceor-truck, one of the basic modifications of the LiL-130 truck series. Wheel base is 4500 ---. The truck is intended for examporting leads with low specific weight. It differs from the base model by its increased length of frame, and bed. All other indicators, including changes according to the verm of output, fully correspond to the base model.

these sis with a metal noppor bed which tips up to the rear. Wheel have is 1300 mm and payload expecity of 4.5 tons. The truck differs from the base model by its shurtened frame and which tips up to the bed, the power take off box (with the pump driving oil into the dump raising mechanism) is scented on the

transmission.

The ZIL-130D1 chassis does not have a towing mechanism. The plant puts out the ZIL-130D2 chassis for the ZIL-MMZ-555 dump truck, which is to be used with a trailer whose gross weight is 7.5 tons. The ZIL-130D2 chassis is equipped with a tewing mechanism, pneumatic power for trailer brakes, and electric power for the trailer taillights. The hydraulic drive for raising the trailer had is installed by the Mytishchinskii Machine Building Plant during assembly of the raising mechanism. Dump trucks which are equipped for work with a trailer are designated ZIL-MZ-555A.

The ZIL-157K truck (Plate 1-5) is the base model of the 3-axle multipurpose cross-country truck with drives on all three axles, uniform wheel setting, and a centralized system of regulating air pressure in the tires. The wheel formula is 6 % 6. The truck is different from the ZIL-157 by installation of a number of ascemblies from the ZIL-130: single disk clutch, 5-speed transmission equipped with two synchronizers, interchangeable carden drive, and also interchangeable transfer case and some parts of the brake system. The truck has a 6-cylinder in-line carbureted engine of 110 hp. The running gear consists of three drive axles, of which the front axle has steering knuckles and indopendent spring suspension, and the rear two axles do not have steering knuckles and are suspended from the balancing carriage, which is equipped with one pair of springs. The steering mechanism does not have hydraulic power. Tire pressure can be regulated. Detailed specifications are given in Appendix 1 (see Part 2). The truck is equipped with an all-metal cab and wooden bed. Payload capacity of the truck is 2.5 tons on dirt roads and 4.5 tons on roads with asphalt covering. Top speed is 65 kilometers por hour. The truck can work with a trailer whose gross weight is 3.6 tons.

The ZIL-157KG truck is one of the modifications of the ZIL-157K truck, differing by a shielded electrical system.

The ZIL-157KV truck (Photo 1-6) is a saddle tractor-truck built on the basis of a ZIL-157K, and intended for work with a semi-trailer which has an allowable gross weight of 6.25 tons on dirt roads, and 11.15 tons on asphalt roads. A saddle arrangement for connecting a semi-trailer is installed on the tractor-truck. The rear wheel carriage and frame are covered by fenders. The spare tire rack has two receptables: one for a tractor-truck spare, and the other for a semi-trailer spare. The ZIL-157KV truck may be specially ordered units with a shielded electrical system and in this case it is designated ZIL-157KVG.

The ZIL-157KE truck is one of the modifications of the ZIL-157K truck series, and differs from the ZIL-157K by the fact that is is produced only in the form of a chassis, intended for assembly of special bodies or units and has fuel tanks on either side of the cab with a capacity 150 liters each.

Weight of the towed trailer may be increased to 8.6 tons, but on roads with cobblegravel surface covering , maximum speed of the tractor-trailor combination must mot
exceed AU km per hour, and on dirt roads 20 km, per hour.

on the enhance of a body the total weight of the unit or loaded hely would be interested by 170 bilegroups, the weight of the had, even specifications of the base trade.

The 'ff 107KH may also be especially ordered with a whielded electrical and the this case the chasts is designated 211-157KEG.

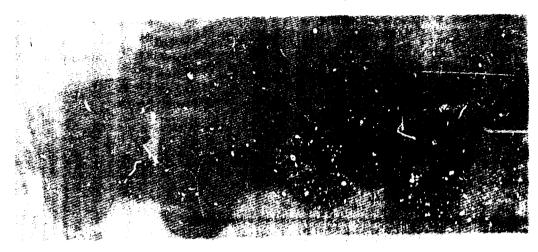


Plate 1-3. MINTIOG tractor-truck with extended whool base



Plate 1-4. ZIL-MMZ-555 dump truck

The ZIL-131 truck (Mate 1-7) is the base model of the series of 3-exic sultipurpose cross-country trucks with drive on all three axies. Wheel formula is a X 6. The truck is powered by an 8-cylinder V-shaped carbureted ISO hp meter. All electric equipment is shielded. The clutch is single disk, and the transmission is 5-speci with two synchronizers for second-third and fourth fifth gears. Fifth gear is straight drive. The transfer case is twin-sheft, having high, low, and neutral speeds. The torque swhent in the transfer case is transmitted to the carden shafts, one of which connects the transfer case to the front axie and the second of which connects the transfer case to the middle axie and through it to the roar one. The front axie has independent suspension, and the two rear ones are suspended from the balancing carriage with one pair of springs. Hydraulic power steering is associated in the strering mechanism. The truck is equipped with a three-place all-metal cab and a wooden platform having metal bindings and metal cross hars. Lateral extensions on the sides of the bed form folding benches, and provisions are made for installation of an additional bench in the widdle of the bed.

Payload aspecity of the truck for operation on different roads with various coverings, including off-road conditions, is 3.5 tons, and on roads with hard surfaces and good composition. 5 tons. Weight of the towed trailer on mixed roads is 4 tons, and on hard roads, 6.5 tons.

The truck is equipped with 12.00.20 tires with centralized control of air pressure in them. For increased cross-country capability, the truck is equipped with a winch. The truck can ford atresss 1.4 meters in depth.



Plate 1-5. ZIL-157% truck

i financione and weight data on the vehicle are given in Appendices 3 and 5 (see Firt 7), and apacifications of assemblies are given in corresponding chapters.

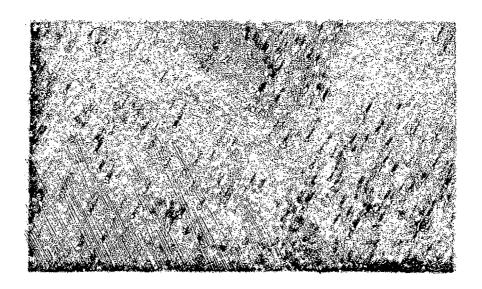
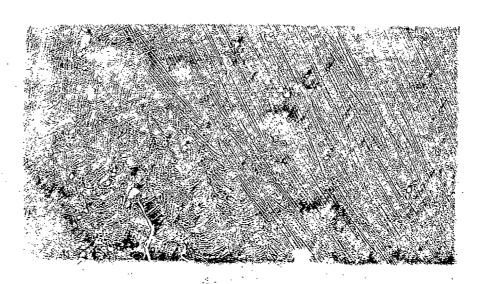


Plate 1-6. ZiL-157KV saddle tractor-truck



Place 1-7, 211-151 rouck

The Itt-131A truck is a modification of the CH-131, and differs from the base truck by the non-shielded instruments of its electrical equipment.

The ZIL-131V truck (Fiere 1-8) is a saidle eractor-cruck created on the base of the ZIL-131 and intended for work with a special resistration where gross weight is:

On all types of road, including off-road conditions, 7.5 toes; On improved dire roads, 10 tons; On roads with apphals or concrete surfaces, 12 tons.

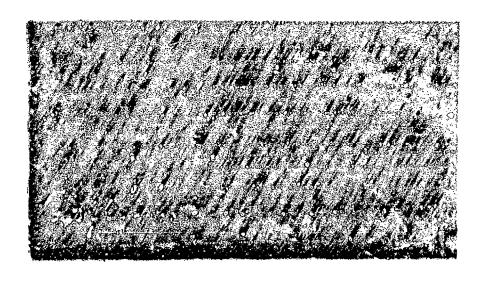


Plate 1-8. Zil-151V saddle tractor-truck

The tractor truck has a saddle errongement for connecting the trailer installed on it, and a rear wheel carriage and frame are covered by fenders. The Apare tire bracket has two receptacles, one for a tractor-truck tire, and a second for a trailer tire.

tractor-trailer combinationers shown in Plate 1-9.

Rollebility Indices of the Motor Validies

Reliability is no. a new operational property of motor vehicles. In 1958, during T.A. Chudekov's development of his tethod for evaluating motor vehicles. Design a according to measured values of various operational properties; this property was included among the Besic ones. In the last five as seven years, the quasilon of increasing product reliability in exchine constitution has received much assentian, and therefore the question of reliability of machines in general, and in extended the first in particular, has made a significant more forward.

Enliability is an angregate property, evaluated according to operational and tenshical properties of tensante absorblies and of the associat abtor subject, according to indicators of longeviey, freedom from trouble, repair. April (chapterility to technical service and repair), and, finally, preservability.

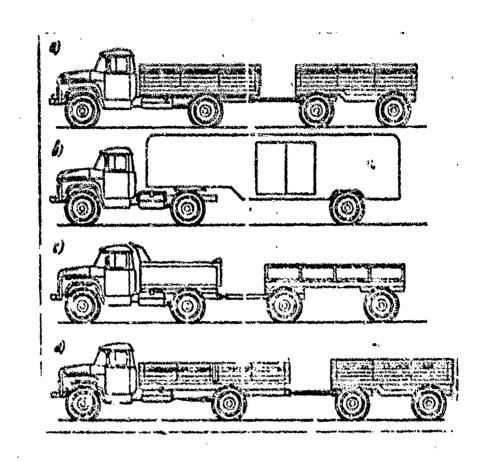


Plate 1-9. Assembled treator-trailer combination. a) paneltype truck and two-male tradies; b) tractor-truck and weak tradies; c) damp truck and two-male tradies; d) long chambers panel-type truck and two-make tradies.

Expirit ectentiate and engineers, vorking in the area of theor vehicle reliability, are developing a system of indicators with which it could be provide to objectively evaluate the complex property of religibility and the employers of which is assembled. This work is settle not completed, but your expositions have received general recognition and aiready but your expices and propositions have received general recognition and aiready recognizes as objection for determination of parfection of motor vehicles and their assemblies, and may be need for planning purposes.

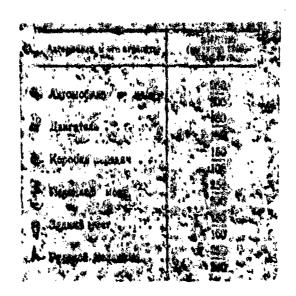


Table 1-%. Longavity of 2-axle ZIL-130 motor vehicles and their basic assemblies (for category Y operational conditions), 1000 km.

Key: a) motor vehicle and its assemblies

b) 211-130 (produced 1964-1966)

c) motor vehicle as a whole

d) engino

e) gransmission

f) front sxle

elga rear (a

h) steering mechanism

NOTE: 1. The numerator shows operation of new essentiles before repair and the denominator shows their operation after major overhaul.

2. The plant is conducting systematic work on increasing lengevity of essemblies, and the data presented may be increased for motor vehicles of later manufacture.

 Longovity shown in the table may be reduced in the following circumstances:

by 10% for saddle tractor-trucks and trucks systematically used with one trailer, working primarily in conditions of category I operation;

by 15% for saddle tractor-trucks working with semi-trailers and trailers, or for trucks with two trailers working primarily in conditions of category I operation;

by 20% for trucks used primarily under conditions of category if operation;

by 50% for tractor-trucks using one trailer in conditions of category II operation;

by 35% fer saddle tractor-trucks working with a semi-trailer or a trailer, or for trucks with two trailers, working in conditions of category II operation:

by 40% for trucks and tractor-trucks working primarily in conditions of category III operation in the regions of the far north or equal conditions.

It is recognized by all that reliability in motor vehicles and their parts may be assured only by the joint efforts of the workers of the manufacturing plants and those of motor vehicle transport.

For solving problems connected with determination of reliability, workers in the automobile industry need systematic and reliable information from motor transport enterprises.

Hethods of assembling information and transmitting it to the plants are now being worked out, and at the plants, they serve to determine service periods and find means of perfecting assembly construction.

Hormative service periods for motor vehicle construction products are at present worked out for only 2-axle general purpose motor vehicles. These norms are worked out in kilometers of running for motor vehicles with carbureted engines (for category I operational conditions with observance of instructions on operations, technical service, and repair).

Data on longavity of 2-axle ZIL motor vehicles and their basic assumblies are presented in Table 1-1.

Controlled fiel consumption of the trucks is given in Table 1-2.

a.	', A	HOTEL	a,	•	٠,	₽,	Parti.	id h
	150 H 130 6 130 6 130 6 130 H 131 H	Hacco	• •	A	Chi		202222	1

Table 1-2. Controlled fuel consumption of the trucks

Key: a) trucks

b) fuel consumption, liters

1) ZIL-130 and dump truck on its chassis

2) ZIL-130-66 5) ZIL-130 VI

4) ZIL-137K

5) ZIL-157KV

6) ZIL-131 and ZIL -131A

7) ZIL-131V

Note: Controlled fuel consumption on a 100-kilometer course is that consumption of fuel by a fully broken in and tuned, loaded truck, weasured in sugger on a dry, herisontal section of road with an asphalt-concrete covering, having a vise no greater than 1.50, with movement of the truck in straight drive at a speed of 30-40 kilometers per hour. Temporature of the liquid in the engine cooling system must be 80-90°C.

Chapter 2. Technical maintenance and repair of the trucks

Yechnical maintenance

Technical maintsquares is the aggregate of the technical activity on the

truck whose fulfillment assures its maintenance in a condition of technical residence. The period and amount of technical maintenance foresees its planning and preventive conduct through an earlier established run of the truck. Timely conduct of the operations of inspection, connection tightening, adjustment, and lubrication prevents the possibility of failure occurence in the truck's assemblies.

Significantly improved technical mainterme and continuing repair may be expected if an effective system of technical diagnosis is developed. Transfer from use of average statistical quantities and periodic technical service to determination of actual requirements for each motor vehicle in various preventive operations would allow significant decreases in labor expenditure on technical servicing, increased technical readiness of the motor vehicle, and would allow a decrease in the number of spare parts.

Technical diagnosis equipped with modern equipment can provide high reliability of the set diagnosis, and also allow timely and qualitative elimination of the occurence of poor adjustment in the motor vehicle's assembles.

The motor vehicle plant collectives and workers of motor vehicle transport are constantly faced with the task of systematically reducing lebor consumption on technical maintenance. The basic directions toward the achievement of this goal are: adaptation of new or improved construction solutions, use of improved oils and lubricants, determination of more rational technical service areas and scopes, and, finally, mechanization and improvement of the technical service processes.

Experimentation on the ZIL-130 produced in 1964 and 1965, conducted by NIIAT (State Scientific Research Institute of Automotive Transport), together with the plant imeni I.A. Likhachev and NANI (Scientific Research Institute for Monor Vehicles and Automobile Engines) showed the possibility of significantly increasing the run between technical services. Table 2-1 presents the period of technical services for 2-axis and 3-axis motor vehicles. Considering the improvements of the ZIL-130 and ZIL-131 trucks and the conducting of additional research, these periods may be even further extended.

Technical service of trucks breaks down into the following types according to partial, scope of operations performed, and labor consumption: DS (daily service: TS-1 (first technical service): TS-2 (second technical service).

The back purpose of TS-1 and TS-2 is to decrease intensity of parts' wear and increase parts' longsvity and reliability by finding and preventing deficiencies through timely performance of control, lubricating, tightening, adjusting, and other work.

Basic date on motor vehicle assumbly adjustment and control are presented in Assendix & (see Part 2).

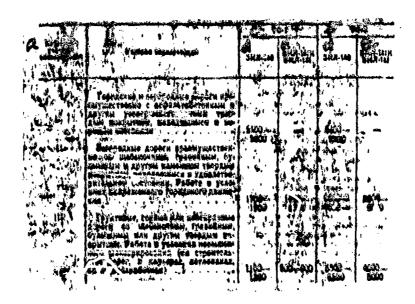


Table 2-1. Notor vehicle technical service periods, km

Key: a) operating conditions category

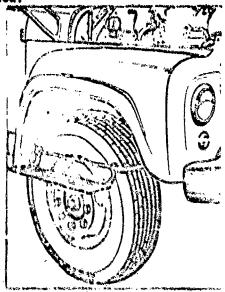
- b) operating conditions
- e) technical service 1
- b) ZIL-130
- e) ZIL-157K, ZIL-131
- f) technical service 2
- Urban and suburban roads, primarily with asphalt, conceste, and other improved hard surfaces, in good condition
- 11) Suburban roads, primarily with subble, gravel, cobblestone, and other hard stone surfaces, in satisfactory condition. Work under conditions of heavy urban traffic
- III) Dirt, sountain, or unrepaired roads, with rubble, gravel, cobblestone, or other hard surfaces. Work under conditions of increased maneuvering (on construction roads, in quarries, foundation pits, or in timber developments)

Note: A run of less than the recommended is set for heavier operating conditions, and also with operation of dump trucks and trucks with trailers and sami-trailers. If the average monthly run of the truck is less than the TS-1, it should be performed no less frequently than once per month, and the TS-2 should be performed at least twice per year.

Technical service of a motor vehicle foresees use of only those oils and lubricants recommended by the plant.

Organization of qualified technical service of the motor vehicle at the motor transport enterprise does not free the driver from the necessity of daily checking the technical condition of the motor vehicle. It as mercessary to check the level of cooling liquid, fuel, and oil, check for leaks, condition of tires, springs, illumination, and signal equipment, lasten to all arising noises and knocks, determine their reason, and if possible eliminate them.

To ease uccess to the under-hood area of the ZIL-130 and ZIL-131 trucks during technical service of the motor and its assemblies, use of a step (Plate 2-1) which can be manufactured (Plate 2-2) at the motor transport enterprise is recommended.



Place 2-1. Step installation on front wheel of ZIL-130 truck

Daily technical service (DE) control work

Before moving out outo the line, inspect the track and check: its completeness, condition of registration numbers, glass and rear view mirror, paint, proper operation of door mechanisms and had latches, springs, wheels and tires, steering wheel free play, power steering condition, operation of st, wi and illustration lights, windshield wipers and washers (on the ZIL-150 are ZIL-141 trucks), thack for looks in the hydraulic power steering system and brake system, and check the fuel and engine cooling systems.

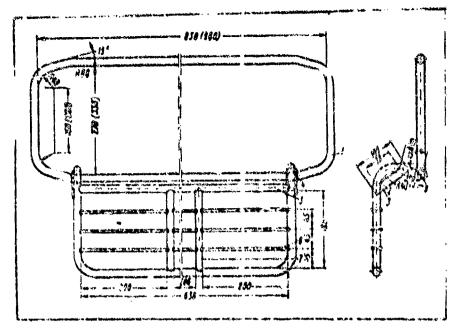


Plate 2-2. Step (dimensions in parent) les for ZIL-131 truck):

1) support ring 2) bracket 3) corner plate 4) support ring 5) longitudinal cross bar 6) longitudinal grid 7) lateral cross bar 8) bracket collar

With the presence of a trailer, check the coupling and open the brake system connecting valves on the tractor-truck and the trailer.

For trucks with a winch, ensure that the winch cable is tightly wound on the drum, the cable hook is securely festened, the trum engagement lever is in the neutral position and securely festened with a lock.

After starting the engine, crankshaft revolutions should not be forced until cooling liquid reaches a temperature of 50°C; and at the beginning of movement, check brake and steering adjustment.

During movement of the motor vehicle, keep checking instrument readings, listen for unexpected noises, attempt to determine the resson for thes (and, if necessary, stap the truck and aliminate them).

On returning to the line in a truck with a V-engine, after shutting down the engine, if the filter has crude cleaning, turn its lever. Sweep out the truck cab and platform.

Gil and fuel tasks. Check the level and, if necessary, add oil to the engine crankcase.

Check fuel level in tank "d add if necessary.

Check water level in radiator. During open storage and a cold time of year, drain the water from the cooling system at the end of the working shift. For this, the radiator cap must be opened. Cleaning and washing tasks. Sweep out the cab and platform. Wash the truck. Wips off the radiator face, cowling, funders, headlamps, parking lights, turn indicators, taillights, cab windows, and registration numbers.

First technical service (TS-1)

During first technical service, it is necessary to perform all daily technical service tasks and, besides this, the following casks.

Control tasks. In the assemblies and systems of the truck, it is necessary to check:

In the engine -- tightness of the cil and cooling systems; Drive belt tension;

Fastuning of motor mounts, intake and exhaust menifolds, and assemblies on the motor:

Condition and tightness of the caps of the fini tank, radiator, and crank care filler:

Religility of the throttle linkage connection with the lever and that of the heke cable with its lever;

Adjustment and work of the throttle and choke;

Blectric system - restaning, insulation, and operation of the illusination and signal devices: headlamps, parking lights, turn indicators, taillights, stop signal, hera, and dashboard;

Clutch - presence of apring stratching; free and full pocal travel and, if necessary, edjustment;

Transmission and transfer case - fastening of the transmission to the bell housing and of the transfer case to the frame cross sember (for ZIL-157K and 21L-151):

In the Carden drive -- condition of universal joints;

Pastoning bolt tension on the support plates of the needle bearings;

Festening of flange baies on propeller shafts and the intermediate bearings; In the drive extensible of the case cover and the differential itself in 1-axie trucks and helf-shaft flanges.

Busing the Aret 75-1 on the ILL-131 truck, the justee factoning the reduction gour to the axis rollers located inside the case must be eightened. It is necessary to recove the side covers of the case before tightening. Tight. ening torque pust be 9-11 kg-poters. In future, this operation is performed

during TS-2; to the experience section and front auto--tightness of the hydrolic

steering system (for IIL-120 and III-IS1 enucks);

Tighthese of the steering box and pitman are of the rechantes; Tension on the stop nut edipiting the pitain are that serve, without changing the position of the scree;

Tightness of nuts of the ballioint and spindle levers:

Free play in the Steering wheel and slack in the steering shaft universal joints;

Tightness of steering mechanism universal shaft wedges (for ZIL-130 and ZIL-131 trucks):

Amount of play in front wheel bearings, and if necessary, adjust bearing tightness;

In the brakes -- condition and tightness of hydraulic lines and control machanisms, and bleed if necessary:

Rod end pins in brake housings and amount of free and working travel of the brake pedal;

Brake ever drive;

Condition of the pneumatic drive safety valve; condition of the hand brake drive and action, with brake adjustment if nocessary;

In the running gear--condition of frame, springs, spring hangers and shock absorbers;

Tightening of the spring snackle nuts and fastening bolts of the front spring hangers, and also the U-bolts of the front spring brackets. On the IIL-187K and IIL-181 trucks, tighten the rear spring hub bracket study and the bolts for fastening the balancing suspension axis brackets. On new trucks, the nuts of the front shock absorber reservoirs must be tightened once during operation (during the third TS-1);

Tightening of sway bar nuts;

Condition of the rubber axie travel bumpers;

Condition of tires and air pressure in them, inflate if necessary, remove foreign objects from tire tread and between dual whoels;

Tightness of connection in pipes and flexible lines of the tire air regulation system;

In the cab, body, and taligate -- Fastening of bed U bolts to truck frame; Condition of support and and coupling machanism on a saddle tractor-truck; Fastening of the cab;

Pastening of the fenders and mud guards;

Lubricating and cleaning tasks. Perfore all lubricating operations in accordance with the truck's lubrication chart (Appendices 10 and 11, see Part 2);

Drain condensation from the air tanks of the air brake system.

Checking the Erack after technical service. Check work of the engine, instruments, operation of the steering mechanism, brakes, and other assemblies and mechanisms of the truck while moving.

Curing technical service of dump tracks and tractor-tracks, additionally check:

Fuscating of the sub-frame to the frame;

in a tractor-truck, condition of the support and coupling or towing mechanism:

Pastaning of the cover on the dump body as ess brackets;

Condition of the body rest and its fastening to the sub-frame;

Condition of the tailgate and its locking machinism and suspension:

Fastening of the power take-off box to the transmission;

Absence of leaks in the hydraulic system of the raising mechanism; Oil lovel in the raising mechanism tank, with addition as necessary; lubricate the dump body access, ball joint fastenings, and hydraulic lift suspensions through the pressure lubricating fittings.

On tractor-trucks, grease the support and coupling towing mechanism.

Second technical service (TS-2)

During the second technical service, it is necessary to perform all operations of TS-I and, besides, this, all the following tasks.

Control tasks. In the truck's assemblies and systems, it is necessary to check:

In the engine -- fastening of the radiator, its casing, and hood latch;

Condition of the louvres and fan;

Fastening of the compressor and its operation;

Pastening of the pulley, fan blades, and water pump;

Condition and Lestuning of the intake and exhaust water hoses and the overflow pipe, catch basin, and lower and side splash panels; Tightness of cylinder head nuts and bolts (check on a cold engine); Pastenings of the radiator, fuel tank, and preheater control panels; Cleanliness of the crankcase ventilation system valve. Clean the valve every other TS-2. During engine oil change, wash the coarse oil cleaning filter element and the oil filler pipe filter in kerosene. On trucks with in-line motors, the fine cleaning filter should be changed and sediment removed (from the sediment bowl) during oil change; at the seme time the oil is changed, clean the dirt off the inside surface of the centrifugal oil cleaning filter jacket cover and wash the filter screen in gasoline or kerosene;

Clearance between the valves and the push rods on in-line engines (adjust if necessary). On the engines in the ZIL-130 and ZIL-131 trucks and their modifications, it is necessary to check the clearance between the

valves and the rocker arms every other TS-2.

During each removal of the engine oil pan, clean residual coked oil from the oil pickup screen;

Compression in motor cylinders (every other TS-2), condition of the water pump body, drain cocks, water hoses and lines of the oil and water

radiators, and diffusers and spacing rods of the radiator;

In the fuel system--absence of fuel leaks, and fastening of the carburetor,

fuel rump, and tanks;

Condition of the fine cleaning filter (remove and wash if necessary); Pusi level in the carburetor float chamber, checked through the control operture with a control pipe with the engine running at idle. It is recommended that the carburetor be removed from the engine, dismantled, and clemed twice a year;

Clean and check the engine speed governor. It is necessary to check the basic carburetor parts once per year. Once per year (in the pring), it is recommended that the fuel pump be removed and checked on an instrument;

Base of starting and operation of engine;

Pusi consumption during movement of the truck in a measured distance; Cleanliness of the filtering element of the fuel filter and sedimentation cowl (wash if necessary);

Cleanliness of the fuel pump screen (clean if necessary). During operation of the Eruck in sandy desert areas, clean the screen every TS-1;

Brain the residue from the fuel tanks. For trucks with V-engines, fue! sediment should be drained twice per year. When the fuel tanks when accessary, no less than once per year (in the Spring);

In the electrical system-degree of charge of the storage battery under load, removing and secharging the battery if necessary;

Condition of the commutator, brushes, and brush holders of the generator and the starter (for ZIL-130 and ZIL-131 trucks, every other TS-2);

Operation of the voltage regulator with volt-amp meter, dismantling and adjusting voltage regulator if necessary;

Cleanliness of spark plugs, cleaning them and setting the clearance between electrodes when necessary:

Condition of the distributor points or trucks not having transistorized ignition systems), cleaning them and setting the clearance between them when necessary. Rub the inside surface of the distributor cap, the side electrodes of the cap, the rotor and blade with a clean cloth soaked in gasoline:

Installation and operation of lights;

In the transmission and transfer case--operation of the transmission and transfer case;

Pastening of the top and side covers of the transmission case and bearing shaft covers;

Condition of seals and correctness of control lever locking of the transfer case;

Tightness of bearings, adjusting bearing sand drive control, if necessary (bearings are not adjusted in the transfer case of the 2IL-131);

Pastening of the line connecting the electric-air valve to the front axle drive engagement chamber (on the 21L-131 truck);

in the Carden drive--slack in the universals;

Fastening of the propellor shaft flanges and intermediate bearing bracket; Fastening of the intermediate bearing support, tightening the nut if necessary.

In the drive axles--lightness and condition of the axle and reduction gear carriage; tightness of the kingpin bearings on the front axle and main drive conic gear bearings of the drive axles of 3-exle trucks, adjusting if necessary. Exchange the upper and lower kingpin bearings on 3-exle trucks (every 30,000 kilometers of running);

Adjust hab begrings of front and year wheels every other TS-2;

Tightening of fastening of drive pinion flange and differential housing in 2-axis trucks (every 20,000 kilemeters);

Support places of the deferential planetary gears and half-shaft gears on drive axles of 3-axle tracks (every 30,000-50,000 kilometers), for which

it is necessary to dispassable the axis. The plate must be replaced in case of excessive wear:

In the steering mechanism and front extr--condition of the front axis beam; Angles of installation and rotation of the front wheels, adjusting if necessary:

Pastening of the steering column to the brucket in the cab and of the steering wheel to the shafe;

Axial play in the front axle spindle bearings of 3-axle trucks, adjusting if necessary.

Wash the filter screeks of the hydraulic power steering pump every other TS-I (for IIL-130 and IIL-151 trucks);

In the brakes -- fastening if the brake valve to the frame;

inviro exert leady to treateuth

Pastening of the hand brake drum on the power shaft;

Every other TS-2, simulteneously with oil changes, in the hub bearings, check: fastening of the brake wheel chamber to the brackets and the brackets to the aule housing:

Condition of brake shore, limings, drums, springs and wheel bearings; Pestening of the spreader can support and brake shoe bins of the front and rear wheels:

Fastening of backing plates to the spindles and rear exle housing; Fastening of eir tanks;

In the running gear--absence of misalignment of the front and rear exle; Condition of the towing and support-coupling mechanism;

Clessiness of the pipes and house of the air pressure regulation system for tires on 3-axle trucks, blowing out the pipes and hoses when necessary;

Fastening of the balancing suspension bracket on 3-exle trucks. Every other TS-2, regave the hubs of the balancing machanism, wash them in kerosome, check the seals and packing rings, and adjust them;

Pastening of the front spring, pillow block, and shock absorber. Hele sure there is no oil leakage from the shock absorber, and replace the fluid or the shock absorber when necessary;

Condition and fastening of the whoels; when necessary, rotate wheels in accordance with the tire rotation diagram. Front wheels of the ZIL-ISO truck must be balanced:

In the ceb, bed, and tuiligate -- featening of the fenders, running boards, sudguards, fuel tank to its brackets, and the brackets to the frame; Lub-ication. Perform all lubricating operations in accordance with the truck lubrication chart.

Chacking the truck ofter technical servicing. Check operation of the engine, steading mechanism, broken, and other assemblies, mechanism, and parts of the vehicle while rinning.

During technical service of shap trucks and tractor-trucks, additionally check: fastening of the pump and its central valve, and the power take off lever bracket:

Fastening of elements of the tailgate locking installation control cochaniss and adjustment of the drambar of its drive: Remove the drainplug from the raising mechanism housing and drain the residue:

Change (according to chart) the oil in the raising mechanism and clean the oil tank filter elegent.

In a tractor-truck, check (while uncoupled) the support and coupling or towing machenism, tighten the plate to the frame and the saddle bracket to the plate, and labricate the support and coupling or towing mechanism.

Twice per year (before caset of the fell-winter or spring-summer periods), check:

Clearance between valve stems and rocker arms, adjusting if necessary; Cleanliness of the engine crankcase ventilation valve, cleaning if necessary; Operation of the thereastat and removal of scale from the engine cooling system when necessary;

Condition of generator brushes and commutator;

Puel tank cleanliness, draining residue when necessary;

Condition of starting prehester;

Density of electrolyte in the storage battery, charging the battery when necessary:

Operation of the brakes, adjusting them necessary; Cisanimess of the drain holes in the cab doors.

Additional technical service in special operating conditions.

In low air temperatures and in the regions of the fer north, it is recommended to: use transmission indricant recommended by the plant for areas of the far north;

Fill the engine cooling system with low freezing point liquid;

Start the engine only using the starting prohester:

So as not to here tires and to prevent preseture transmission parts wear, sovement of the vehicle must be started smoothly, without interruptions, and for the first 15-30 minutes, it should be moved in first or second gear at a speed of 5 kilometers per hour;

Park the vehicles on parking places in shelters which are protected from the wind, and tightly cover the motor with covers:

the wire, and tightly cover the motor with conver; Wessere the storage battery and place it in a were location;

Here the winch case before using it;

to not park the truck with reduced air pressure in the tires;

Closely check the air seel of the tires during inflation or parking:

To staid freezing the brakes to the draws during long stands, do not brake the tracks; the handbrake should not be set on the truck or the trailer (or seal-trailer):

Release the sir firs the brake system of the truck and trailer (or soliteriler) through the velves on the sir chambers of the wheels of the truck (truck-train). In this case, it is necessary to set blocks.

In sandy desert regions under conditions of very sandy locations, it is recommended that parts be disassembled and essential during technical service in sholters or tents:

Clean the vents of all assemblies and check condition and fastening of the protective boots on the propellor shafts daily;

Systematically clean sand from the radiator and engine;

Clean sand from the air filter, wash the acreens, and check the level and cleanliness of oil in the air filters daily:

Check the level of electrolyte in the storage battery dealy and fill it with distilled water early:

Cican sand and dirt from the surface of the storage battery and the holes in its case regularly:

Fay particular attention to tire conditions during control inspections while running:

turing TS-1, clean the filters and residue from the engine fuel system, check operation of the fuel tank air vents, clean the valve pipes, and the line connecting the main and suxiliary tank;

During extended stands at high temperature, it is recommended that the storage battery be removed from the truck and stored in a cool place.

Technical Service of Trailers and Semi-trailers

Wide use of the ZIL-carge trucks as tractor-trucks in truck-trains makes preventive maintenance on the trailer assembly necessary long with that of the tructor-eruck.

Construction of trailers and semi-trailers decrees a period and character of work conducted on their technical service which is identical to that of traiter-trucks.

Delly servicing of trailers and semi-trailers includes clerning and washing, and control and inspection operations. Checking the condition of springs, tires, fasturing of wheels and the coupling machanisms with the tractor-truck, condition of brakes, illumination and signal lights require special attention.

The scope of the first technical service for trailers and semi-trailers additionally includes tightening and lubricating operations. Special ettention should be paid to the condition of the coupling mechanism (the connecting pin and its exis), the towing installation of the tractor-truck, condition of the saddle installation and its festening to the frese, and condition of springs, rods, and the turning mechanism.

The scope of the second technical service forcess deeper proventive maintenance of the trailer or semi-trailer, including lubrication of the hubs, checking condition of the brake valves, and checking synchronicity of brake wear on the trailer and tractor-track.

Labrication of the Truck

Service life of the truck depends on its timely and careful life cation,

to well as on the quality of the oils and grosses used.

Appendix 10 (see Part 1) presents a lubrication chart for a 1-axie truck, and Appendix 11 presents a lubrication chart for a 3-axie cross country truck.

Labor consumption is given for conditions of category II operation, and therefore, for category I operations, labor consumption must be decreased by 20%, and for category III operations, it should be increased by 25%.

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Table 2-2. Technical service and continuing maintenance labor consumption

(ey: a) type of technical service, maintenance, and labor consumation

b) IIL-1303 (produced 1964-66)

c) labor consumption, man hours: US, TS-1, TS-2 \(\frac{1}{2}\) izenific labor consumption,

†) Transfic labor consumption, man house per 1000 km run: DS, TS-1, TS-2 •) total specific labor consumption for technical service (man hrs. per 1000 km run)

f) specific labor consumption for continuing maintenance, man hrs. on 1000 km run

2 Lever consumtion norms are given for the base truck.

S Heres developed by NIIAT, ZIL, and NAMI.

¹ Designation of the cile and greases used for the ZIL trucks is given in appendix 9 (se. Part 2).

Labor consumption of technical service and continuing maintenance of other trucks increases by comparison with the basic models:

By 10% for saddle tractor-trucks and trucks working with trailers; By 10% for dump trucks and by 20% during work at short distances (less than 5 km) or with trailers.

The plant is conducting systematic work on improvement of the tricks produced, and therefore, for ZIL-130 trucks of later production, the labor consumption norms may be decreased.

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Table 2-3. Distribution of labor con sumption of TS-1 according to type of work, 1

Key: a) type of work

- b) 21L-130
- c) ZIL-184Z-555
- d) control
- e) tightening
- f) edjusting
- g) lubricating and filling h) electrical
- i) work on fuel system service
- i) work on tire service

Rapair

The mission of repair is elimination of deficiencies arising in the truck or in its parts by the must effective means, with the fullest use of the entire resource of parts or essemblies.

Mater vehicle repair production has at ite disposal large reserves of economic effective ess and usage of the resource of all parts and assemblies is today practically impossible without using repair or exchange of some parts with retention of others.

A tumpelor	3K4-100	SH'S-MIS-MS
Общей оснотр валь- рабоми К пределимо В Регулеровениме Спекточени Закатрегелимеление У Ребора по обсерния выно вистемы вита- ния В Раборы по обсер-	20.8 20.5 20.5 20.5 20.5 20.5 20.5 20.5 20.5	10.7 10.7 7.5 10.8 10.8

Table 2-4. Distribution of labor consumption of TS-2 according to type of work, %

Key: a) type of work

b) ZIL-130

c) ZIL-MIZ-555

d) general truck inspection

e) control

f) tightening

g) edjusting

h) lubricating

i) electrical

j) work on fuel system wervice

k) work on tire service

A large amount of research has shown that any disassembly and essembly of an assembly, even if the part is not repaired, decreases its service life by 200. This takes place because of the fact that during each disassembly, the character of fit and relative position of the run-in assembly surfaces of the parts are unaviolably changed. This attests first to the fact that (iscassembly of parts should take place only when it is an estual necessity and second, to the fact that any measures used during disassembly to secure the best installation of the parts in their same places (punching, marking with paint, or making marks on the assembled part) are highly profitable in the practice of conducting all types of repair.

A proposition on technical sorvicing and repair of running year was established to the effect that repair breaks down into two types: continuing and major. Construction features of new truck models such as the ZIL-150 and the ZIL-151, especially in the areas of engines, with their high service life, give basis for a large number of specialists to speak out for resurrection of the rules of the earlier-dropped "medium" type of repair.

Actually, the presence of low-wear cylinder sleeves, crankshafts and canshafts which are tempored as the result of heating in a large number of the engines coming in for major overhaul has excluded the necessity for work on these basic parts and, in practice, made major overhaul of those engines no more than a deepened check on the technical condition of the assembly, with weaking, edjustment, and exchange of some parts.

This scope includes the idea of "medium overhaul" and must apparently serve as the basis for remeval of this type of overhaul in the rules.

All existing types of repair may be performed either on separate assemblies or on the motor vehicle as a whole. The assembly method of repair is most widely used.

In recent years, the idea of maximum centralization and specialization of repair of separate parts without sanding the entire assembly to the repair plant has received increasing acceptance. Such centralization for repair of cylinder pleaves and their assemblies, pistons, and rings to overhaul dimensions, or of crankshafts with their assembly with repair bearings, renewal of worm out valves, carburetors, and a large list of other parts would allow creation of a new type of motor vehicle repair enterprise. Highly specialized, mechanized, and fitted with modern equipment, the motor vehicle repair enterprises, putting out high quality production on the basis of rebuilt used parts, could successfully significantly raise the effectiveness of repair activity and, most important, free the industrial plants from shipment of a large quantity of spare parts.

Continuing maintenance of the motor vehicle (assembly) has the purpose of eliminating naticed deficiencies, for the most part by means of rebuilding or exchanging deficient parts, companynts, and assemblies. The mission of decreasing three-def expenditures for spare parts sharply poses the task of collecting parts and assemblies removed in the process of continuing maintenance and sending those which can be rebuilt to shops of the motor vehicle transport enterprises or to special repair plants.

Major overhead of a mestor vehicle (assembly) is intended to renew the weeking empablify lost during the process of operation. The quality of perference of sajor overhead take provide a between-overhead run of 80% of the run of a new sorer vehicle (assembly), counting the fact that in the process of operation, due to again of parts, their wear, and the poorer condition of assembly, their decreased resource is unaviousble. Northwide practice in motor vehicle temper production knows, however, that under conditions of high decrease for temperatical condition of the repaired parts in modern repair temperation, the astrice partial of assemblies after major overhead is no lower that that of new ones.

Achievement of this rapair quality must also become a mission for the motor valida repair enterprises.

Positive vision of this mission may be achieved only when the technical equipment and this present in motor vehicle repair production correspond to the level present in motor vehicle production. This is possible only under

conditions of organization of industrial major overhaul huilt at the enterprises of second production of overhauled products with a sharp increase in the size of motor vehicle repair enterprises and their narrow specialization for overhaul of a determined make of motor vehicle.

The major reasons for service life decrease in overhauled components and assemblies are:

Unsatisfactory washing and cleaning of the part; Changed parts assembly fit in comparison with original; Non-observance of parts bolt torque; balance norms, and weight differences assigned by the plant.

The basic technical requirements for sections conducting overhaul, aside from dependence on where the overhaul is performed, must be the following.

The sections must be equipped with the necessary pullers, mandrels, attachments, and tools.

During disassambly, it is necessary to: press out parts with pullers, drifts, mandrels, or light taps with a copper (wooden) mallet; carefully remove inserts, separating them from their adjoining surfaces; maintain integrity of paired gears.

The dismantler must know the parts subjected to punching or marking by another means, for keeping their balance or observing the character of fit.

With defective parts, in checking their technical condition, dirt, scale, coke, and corresion should be carefully cleaned from them. Parts control begins with a careful inspection. Parts of the steering mechanism and brake drive must be checked for absence of cracks by magnetic defectoscopy.

Before 2000mbly, all parts must arrive for assembly free from dirt, scale, or coke.

Oil passages must be cleaned and checked.

Painted parts having a damaged lacquared layer must by repainted. The internal hollows of the cooling system on the surfaces contacting hot water are not painted.

Nicks, burrs, and shallow marks must be smoothed, and defective threads must be repaired (nicks are not allowed in parts which may be stress concentrators).

All cavities of the lubricating and cooling systems must be checked for tightness.

Roller bearings may be used without exchange if they satisfy the requirements for the technical conditions for overhauled bearings of GOST 6275-57.

Working edges of packing seals must not have breaks, cracks, or traces of rubber layer separation. Besides this, rubber parts must not have evident signs of stretching.

Fastening parts (bolts, nuts, pins) must not have spoiled threads (more than two threads).

Only new lug washers, cotter keys, and safety wire may be used.

Assembly must take place under conditions providing cleanliness of assembled components. The assembly sections for components must be equipped with work benches or stands, eliminating component assembly on the floor. Assembly of parts and components must take place according to drawings and schematics from the plant.

During engine assembly, soft cloths and not textile ends should be used for wiping.

During assembly, rubbing surfaces of parts should be lubricated with clean oil. It is recommended that all insorts except those specially stipulated be lubricated with scaler before being installed. Scating of bushings, scals and bearing rings is accomplished with special mandrels. During tightening of connections which are backed with rubber inserts, excessive force should not be used, or the insert will be ruined.

Increased assembly accuracy when using parts with wear (within allowable limits) is necessary to achieve the individual coupled detail of the part.

Boarings

In the process of use, various defective parts having ball or roller bearings are discovered. The most characteristic of these are shown in Table 2-5.

During disassembly of the parts, force during bearing pressing must be applied to the face of the outside race (when pressing the bearing from the body) and to the face of the inside race (when removing the bearing from a shaft). Forced transmittal through the rolling body or through the separators is not allowed.

Bearings removed from disassembled parts must be carofully washed. They are considered usoful for repeated installation in an assembled part if they correspond to the requirements of GOST 6275-57 for ball and roller bearings.

Use of bearings with traces of corresion, burns, cracks, chips, dents, impressions, and other mechanical damage on the amenday or working surfaces of the ring or rotating body is not allowed.

Bearing assembly should take place so that during their installation on a shaft, pressing force is applied to the inside race, and during their assembly in a body, it should be applied to the outside race.

Defact symptom

Defect cause

Excessively high temperature or noise during operation of the part

Overtightening the bearing during adjustment; absence of lubrication in the part; bearing misalignment; excessive wear or destruction of bearing parts; dirt in bearings.

Throwing of lubrication from the part

Wear of bearings; damage to packing insulation; excessive lubrication; liquified grease due to bearing overheating

Table 2-5. Symptoms and causes of bearing defects

Hydraulic, screw, or other presses are used for pressing boarings. Assombly tubes, sockets, mandrels, and insert rings are used as attachments. If unavoidable, pressing bearings on a shaft with hamzer blows on an assombly cup at allowed. Hammer blows on the bearing ring are not allowed.

Normal work of the bearing may be assured only if precise coincidence of the case of the shaft and body is established.

His lignment of the axes will cause overloading of the rotating body and premature bearing breakdown. Overtorquing bearings is just as dangerous as undertorquing them.

Tightening of bearings and bearing assemblies must be accomplished with special care so at to assure their long and proper operation.

Section II. Engines

Chapter 5. The in-line engine

Layout

Production of the in-line four-stroke six-cylinder carbureted engine began in 1947 with the ZIL-120 model, and then the ZIL-164, ZIL-164A, ZIL-157, and ZIL-157K. These engines were installed in the ZIL-150, ZIL-151, ZIL-164, ZIL-164A, ZIL-157, and ZIL-157K motor vehicles (Plates 3-1, 3-2, 3-3). Basic data on the ZIL-157K engines are presented in Table 3-1.

Beginning in 1947, the engine was modernized several times. In particular, engine power of the later models of the ZIL-157K was increased to 109 hp after installation of a two-throat carburetor and an intake manifold with separated intake chambers. The engine serial number is stamped on a flat surface located on the left side of the cylinder block at the top of its plans opposite the first cylinder. Additionally, the number is stamped on the factory plate located on the right side of the driver's seat frame.

Crankshaft and camshaft mechanisms

The cylinder block (Plate 3-4) is cast of SCh 24-44 cast iron (GOST 1412-54). The double walls of the block form the water jacket along the entire length of the cylinders. For equal valve seat cooling, a brass water distributing pipe is installed in the block.

The bell housing is cast iron. Roar motor mounts are cast together with the bell housing.



The cylinder head is made of an aluminum alloy. Compression chamber displacement is 140.5 cm³. Deviation over 2.3 cm³ between separate chambers is not allowed.

Spark plug holes in the cylinder head have a thread of 14 mm and a pitch of 1.25 mm. A steel-asbestos gasket is installed between the head and block, and the smooth side of the gasket should be against the head during assembly. Some engine modifications use a copper-asbestos gasket.

The head is festened to the cylinder block with 25 bolts and 7 stude. Three front stude are also used to fasten on the compressor, and four rear ones are used for fastening the attachment to lift the engine.

The pistons are cast of an aluminum alloy. A label is placed on the top of each piston: dimensional piston group according to skirt diameter, weight group of the piston, and dimensional group of the piston according to piston wrist pen hole. Piston dimensions and piston ring groove profile are shown in Place 3-5.

Wrist pins (Plate 3-6) are hollow and manufactured of low-caroon steel. The exterior surface is subjected to surface temporing with high-frequency current to a depth of 1.0-3.0 mm.

() (la passerge	вереметре» Всенакия
С Максинальная мощность при 2800 об/мин. з. с	100
(по бераничителю ческа обо- ротов), я с	164
HOMENT ROW 1100-	34
Г Ливиотр цваниара и вод порыня, ма Ф Степень сматия Б Рабочий объем, а	101,6×114.3 6,3* 5,38

Table 3-1. Parameters for 311-157k

Key: a) parameters

b) excent of parameters

c) maximum power at 2800 spm, hp

d) power at 2600 rpm (according to rpm governor), hp

e) saxiaum torque at 1100-1400 rpm, kilogram meters

f) cylinder bore and piston travel,

g) compression ratio, 6.21

h) displacement, moters

 $^{^{1}}$ The compression ratio of export engines is 6.5.



Finte 3-1. ZIL-157K truck engine

The piston rings (Plate 3-7) are cast of cast iron, alloyed copper, and titanium, with a hardness of HRB 98-106. The middle compression ring has a groove along its exterior diameter, and the top compression ring has a groove along its interior diameter.

The top compression ring is chromed

Connecting rods (Plate 3-8) are forged steel, with an I-shaped section.

The crankshaft is a steel forging. To increase wear resistance, the crankshaft and connecting red hearing surfaces are subjected to surface tempering with high-frequenct current to a depth of 2.5-6.5 mm.

Surface hardness of the shaft surfaces after temporing is HRC 52-62. The crankshaft is balanced. The allowable imbalance is not greater than 150 gram cm.

Imbalance is eliminated by drilling holes in the Aurface face from the side of the shaft crank. Crankshaft bearings, main and connecting rod, are equipped with thin-walled interchangeable inserts, made of bimetallic bands. As an anti-friction alloy, the inserts use an ATL-6-6 alloy (antimony 5.5-6.5%; tin 5.5-6.5%; lead remainder).

Thickness of the anti-friction alloy on the inner side of the insert is 0.230-0.305 mm for main journals and 0.180 0.305 mm for connecting rod journals.



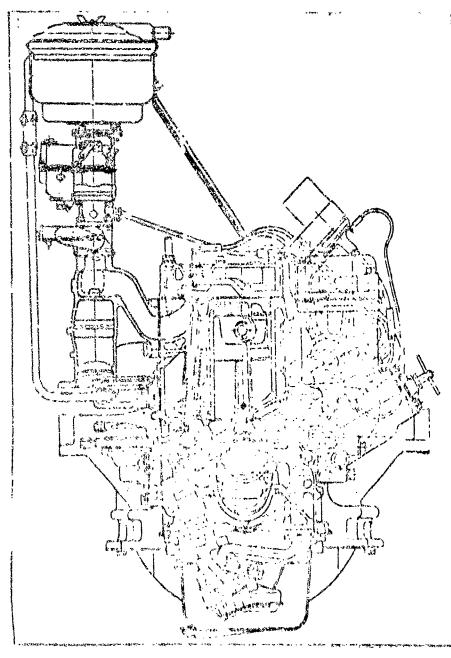


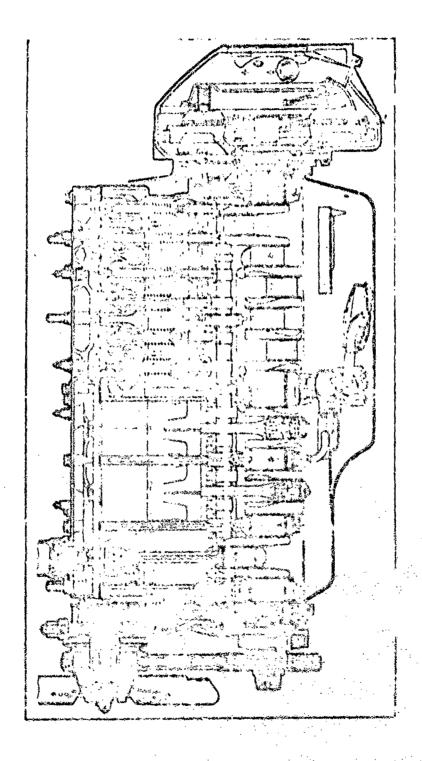
Plate 3-2. Lateral section of ZIL-157K engine

The flywheel (Plate 3-9) is gest iron with a steel-roothed rim for engine starting with the searter.

The rim and flytheel are press-fitted.

The camphaft is seed, forgod, and its bearing surfaces, can lobes, eccentric and goar tooth are hardened with high-intensity heating.

after hardening, the bearing surfaces have a hardness of HRC 54-62, and the cas lober nave a hardness of HRC 65-62.



ate 3-5. Longivudinal section of 21L-157K engine.

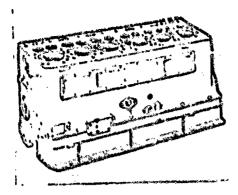


Plate 3-4. Cylinder block

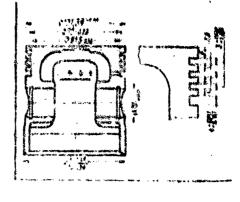
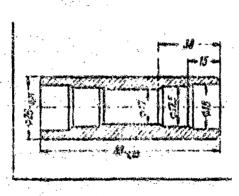


Plate 3-5. Piston



Pleto 5-6. Pisten wrist pin

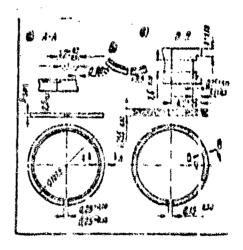


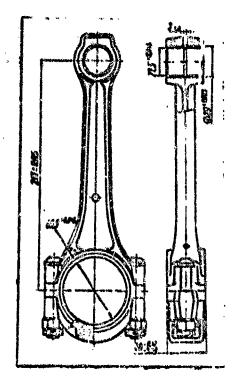
Plate 3-7. Piston ring:
a) top compression ring; b) oil ring; c) specification for piston ring ropair disension

Profiles of the cambeft lobes and eccentric are shown in Plate 3-10.

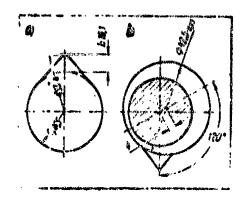
The shaft is installed in the cylinder block in four sliding bearings which are bimetallic bushings pressed into receptacles in the block. The camelet is presented from moving in a longitudinal direction by a flenge fitted on it and featured by two boils to which access is gained through holes in the camelett gray.

The small cambaft ster (Plate 3-12, a) is steel.

The large complete goer (Place 5-12, b) is cast iron. Fastering of the goer outo the cambait is shown in Place 3-15.







Piste 3-8. Connecting rod

Plate 3-9. Flywheel

Plate 3-10. Profile a) lobe b) eccentric

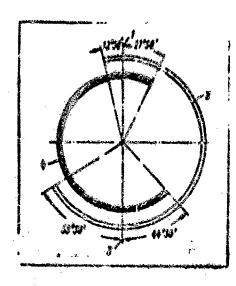
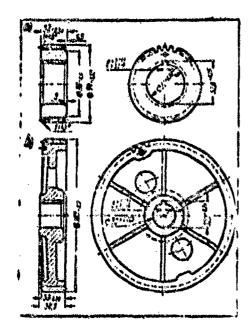
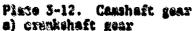


Plate 3-11. Diagram of gas distribution phases: 1) TDC 2) intake 3) BDC 4) exhaust

The cambaft garr cover (Plate 3-14) is cast iron and installed on a graket. Cantering of the cover on the block is accomplished by two locating sloeves through which the cover festening bolts run. A pin for adjustment of the ignition system is sorewed into the cambaft goar cover. Seal 1 of the Cont end of the createners is present into a receptable in the cover. The seal is self-tipleming, and rubber with a motal body.





b) cambart gear

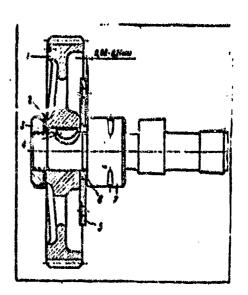


Plate 3-13. Fastening gear onto campheft

- 1) gear 2) lock wesher 5) nut
- 4) key 5) support flange
- 6) specing ring 7) camshaft'

In all instances when there is noticeable wear, visible cracks, or other design on the working surface of the seal, and also in cases when the rubber of the seal is hardened or stretched, the seal is subject to replacement.

West on the bearing surface under the bracket of the front motor mount is allowed to a dismeter of 91.65 mm.

Valves. Intake valves (Plate 3-15) are manufactured of chromed steel.

Exhaust valves are cosposite, with the head exhustactured of heat-resistant chromium-silicon steel, and the stee welded to it manufactured of chromium steel. Exhaust valves for engines working with a 6.5 compression ratio are starged and one-piece (of steel with increased heat resistance). Valve spring

Table 3-2. The camphaft provides the following phases of gas distribution (Plate 3-11):

Intake valve opening12°30'	before TDC
Intake valve closing59*30*	after BDC
Exhaust valve opening44°30'	before EDC
Exhaust valve closing	after TDC

plates are fastened with a thrust lock. As the result of action of burning gases, corrosion, shock loads, and also deposits of tarry substances in the process of operation of the engine, tightness of the working surfaces of the valves is destroyed.

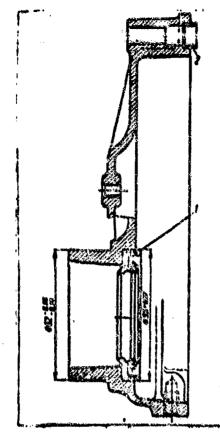
Destruction of the valve seal with proper clearance between the tappets and valves and proper work of the carburetor and ignition is discovered by the characteristic of popping from the muffler and carburetor; the engine begins to run with a miss, and does not develop full power.

The valve springs are steel and are wound out of wire (65 G steel). Valve tappets and guides. The tappets are steel (Plate 3-16) and the valve guides are cast iron, made in the form of two removable sections for each of the six tappets.

The adjusting boit 1 of tappet 3 is installed with a stop nut which featens the boit in any position determined during adjustment of the clearance between the tappet and the valve. Boit thread dimensions are NO X 1. In case of wear on the working surface of the bolt head, it is polished on an abrasive stone. Deviation of the bolt sphere relative to its threads is no greater than 0.1 mm on a radius of 5 mm. Wear on the spherical surface of the tappet plate must not exceed 0.10 mm, and wear on the tappet stem must be no greater than 0.04 mm.

The inteke and exhaust manifolds (Plate 3-17) are single iron castings with a central upper flange for mounting of the carburetor and a central lower flange for connection with the exhaust gas collector pipe. The manifolds are intended for use with a 2-throat carburetor with separated intake ports for the front three and the back three engine cylinders. Contact planes of both manifolds and the gaskets beneat them are identical and interchangeable.

Angles of gas distribution phases are given for the moment of beginning and end of closing of the valve with a clearance between the valve and tappet of 0.25 am.



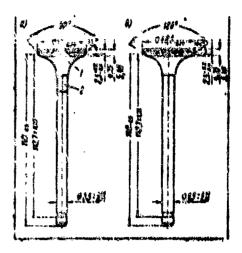


Plate 5-15. Engine valves: a) exhaust b) intake 1) head 2) welding of head to valve atom

Plate 3-14. Cemshaft gear cover

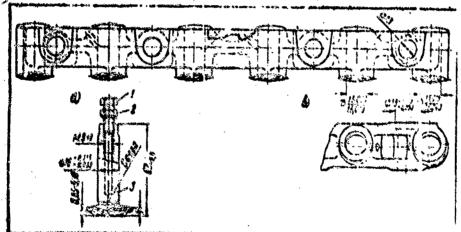


Plate 5-16.
Tappet and tappet guiding section:
a) tappet guiding section
1) adjusting bolt
2) stop nut

- 3) tappet

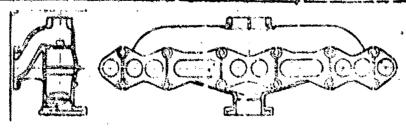


Plate 3-17. Intake and exhaust manifolds

Lubrication system

The engine lubrication system (Plate 3-18) is combined. The engine is equipped with an oil radiator (Plate 5-19) and a two-section oil pump (Plate 3-20) whose upper section supplies the engine lubrication system and whose lower section pumps oil to the radiator.

The main and connecting rod bearings of the crankshaft, camshaft bearings, breaker -- distributor drive shaft and camshaft gear are lubricated under pressure.

Cylinders, piston wrist pins, camehfft lobes, tappets, and valve stems are lubitated by splashing.

Oil filtering in the system takes place sequentially in the screen filter of the floating oil pickup 17 (see Plate 3-18) of the pump and in the plate coarse cleaning filter. Part of the cil (5-8%), besides this, passes through the fine cleaning filter (Plate 3-21) with a changeable filtering element 11.

Working pressure in the lubricating system is 3-4 kg/cm². This pressure is sustained with a spring reduction valve located in the body of the oil pump. With proper operation of the reduction valve, oil pressure in the lubrication system of a warm engine at 1000 crankshaft revolutions per minute must be no lower than 2.5 kg/cm². If a deviation from the assigned control pressure is observed during checking, it is necessary to remove the reduction valve in the assembly and check the condition of its parts.

The oil radiator is fastened by four bolts to brackets which are welded on the frame of the water radiator louvres. Removing the radiator from the truck, it is necessary to wash it out with a degressing solution and hot water. Tightness is then checked with air at a pressure of 4 kg/cm² in a water bath. An observed stream is eliminated by soldering with light solder. Small holes in the radiator body are climinated with welding and consequent cleaning. Blockage of tubes is allowed, but no more than three.



Plate 3-19. Oil radiator and lines:
1) radiator core 2) L-connection
3) radiator valve 4) hose 5) oil intake line 6) hose 7) oil outlet line
8) hose class

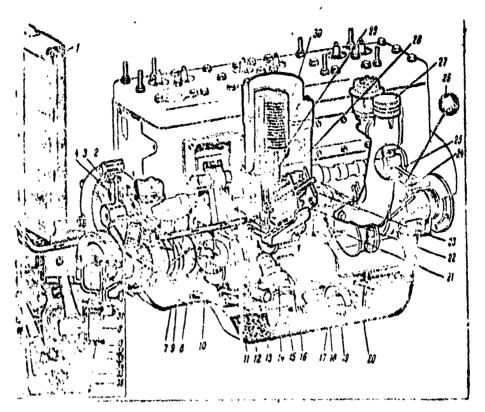


Plate 3-18. Engine lubrication system:

1) oil radiator 2) oil passage to front camshaft bearing 3) opening for oil spleshing on camshaft gear 4) oil passage to support flange 5) oil outlet line 6) oil inlet line 7) main oil line 8) oil passage in crankshaft 9) oil outlet line 10) oil radiator shut off valve 11) oil lines to compressor 12) oil passage to filters 13) top section safety valve 14) top section 15) bottom section 16) lower section intake pipe 17) upper section floating oil pickup 18) eil pan 19) drain plug 20) dip stick 21) cleaning plates of coarse cleaning filter 22) filtering plates of filter 23) filter lever 24) oil pressure sending switch 25) oil passage to rear camshaft bearing 26) oil pressure indicator 27) oil filler pipe 28) oil filter body 29) filter central tube 30) fine cleaning filter element 31) oil filter bypass ball valve 32) upper section driven gear 33) apper section driving gear 34) lower section ball by-pass valve 35) lower section driven gear 36) lower section driving gear

Cooling system

The cooling system (Plate 3-22) of trucks intended for work in temporate climatic zones in closed, with forced liquid circulation. Pressure in the engine cooling system is automatically regulated by valves in the radiator cap and may reach 0.3 kg/cm². At this pressure, water in the system will not boil until it reaches 105 C.

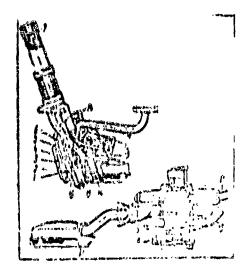


Plate 3-20. Two-section oil pump:

1) lower section driving gear 2) lower section body 3) separating plate
4) upper section body 5) pump drive shaft 6) upper section driving gear
7) pump drive gear 8) lower section intake pipe 9) lower section by pass valve 10) floating oil pickup 11) upper section oil line 12) upper section oil line 12) upper section valve 13) lower section oil line 14) driven gear shaft 13) lower section driven gear

Tractor-trucks working with heavy semi-trailers and trucks intended for use in tropical climates are also equipped with a closed type cooling system with forced liquid circulation and introduction of a condensation tank into the system.

Pressure in the system is regulated by valves in the condensation tank cap, and may reach 0.65 kg/cm². With this pressure in the system the water will boil at 114° C.

The condensation tank has a volume of 4 liters, is equipped with a neck for fastening the cap to (Plate 3-23), and has a valve 7 located at the bottom part of the tank for release of water. The tank is bolted onto the cab firewall breath the engine hood.

With an increase in water temperature in the engine, the pressure in the cooling system increases, and part of the water is converted into steam which flows along pipe 3 to the condensation tank 4, in which, passing through a layer of water, it is converted to water.

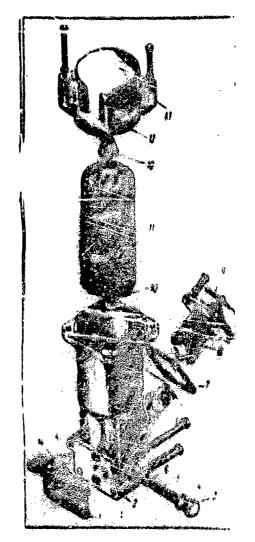


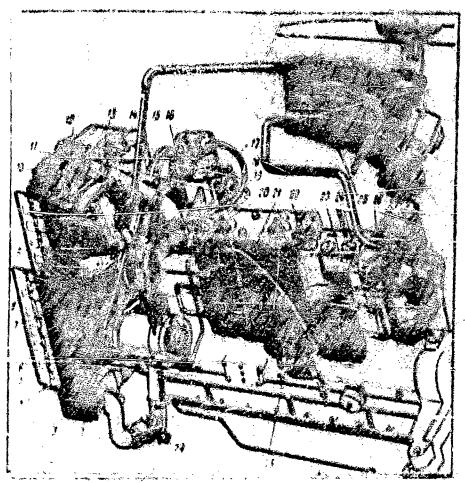
Plate 3-21. Oil filter parts:

1, 7, and 12) gaskets 2) filter body
3 and 14) plugs 4) backing ring
5 and 10) springs 6) by-pass valve bowl
8) coarse cleaning filter element
9) coarse cleaning handle 11) fine
cleaning filter element 13) filter body
cover

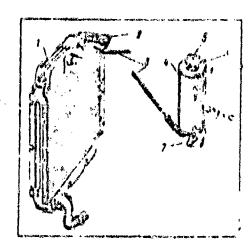
With a decrease in cooling system temperature, pressure in the radiator decreases and a vacuum is formed in the top radiator tank, as the result of which water from the condensation tank is drawn back into the radiator. Water level in the condensation tank therefore changes, depending on the cooling system temperature, and it should not be filled more than half way.

The heavy duty cooling system is composed of a four-row radiator with a tight rubber plug and pipe 3 for exhaust of ateam into the condensation tank. The fan pulley on these engines has a smaller dismeter, increasing the number of fan revolutions and increasing the offectiveness of the cooling system.

The water pump, fan, thermustat, and water distribution pipes for the cooling systems of all in-line angines are identical. Louvres are not installed on trucks intended for use in the tropics.



Piete 3-22. Engine cooling system 1) radiator exhaust hose 2) radiator fastening frame 3) fan shroud 4) touvre festening frame 5) louvre flap 6) flap axis 7) fan and water pump drive pulley 3) rudiator pipe 9) fan 10) louvre control red | 11) louvie centrol angle lever 12) flap drive rod 13) radiator intaké pipe 14) redictor filler nock 18) pipe for carrying cooling liquid from heater 16) hose for carrying cooling liquid from compressor head hollow 18) cylinder head pipe 19) therwastat 20) water pump 21) cylinder block water jacket 22) cylinder hoed water jacket 23) water Astributing pipe 34) cylinder block water jacket inspection plate 25) cab heater 26) cooling liquid temperature sending switch 27) cooling liquid temperature indicator 28) valva for draining liquid from water jacket and cylinder head 29) valve for draining radiator liquid



Fiate 5-23. Connection of condensation tank to radiator:
1) radiator 2 and 5) caps
3) pipe for anheusting steam from radiator to tank 4) condensation tank 6) steam exhaust pipe 7) drain cock

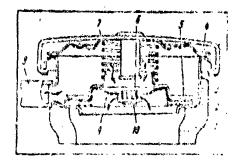


Plate 3-24. Radiator cap:
1) filler neck 2) release valve
3) cap body 4) spring supporting
plate 5) release valve plate
6) return valve spring 7) release
valve spring 8) steam exhaust pips
9) inlet valve cup 10) inlet valve

Overflow pressure in the cooling system is automatically regulated by the release valve 2 (Plate 3-24) of the cap, which is installed on the radiator filler neck in the first case (with a pressure of 0.5 kg/cm²), and on the neck of the condensation tank 4 (see Plate 3-23) in the second case (with a pressure of 0.65 kg/cm²). The caps are identically constructed, but equipped with different springs 7 (see Plate 3-24) in the release valves. The pressure for which the cap is regulated is stamped on its exterior surface.

The air inlet valve 10 of the cap opens and connects the hollow of the radiator with the atmosphere as a vaccous which is equal to 0.01-0.13 kg/cm2.

If the runder backing ring of the valves on the cap is missing or damages, the cooling system will cease to work as a closed one, cooling liquid will beil at 100°C and engine overheating will occur significantly sooner. In this case, the cap should be replaced with a new one or its sealing ring should be replaced.

The cooling system thermostat is a liquid type installed in pipe 3 (Plate 1-25) of the cylinder head. Valve 4 of the the mostat begins to open at a cooling liquid temperature of 70 ± 2°C. At a loner liquid temperature, the belows is in a compressed position, so that valve 4 of the thermostat is closed, as the result of which the cooling liquid does not reach the radiator. When cooling liquid temperature reaches higher than 70 ± 2°C, the thermostat believe begins to expand, opening valve 4. At a temperature of 83 ± 2°C, the valve 4 is fully opened (height of velve raising is no less than 9 cm), so that cooling liquid from the cylinder freely passes to the radiator.

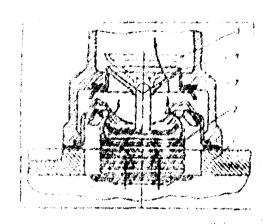


Plate 3-25. Schematic of theremostat operation:
1) cylinder head 2) thermostat bellows 3) cylinder head pipe 1) thermostat valve in closed position 5) thermostat valve in open position

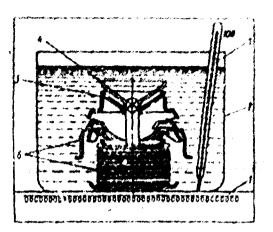


Plate 3-26. Schematic for checking the thermostat:
1) electric hot plate 2) pan
3) thermometer 4) valve position at the end of opening 5) valve position at the beginning of opening 6) thermostat



Plate 3-27. Radiator without fan shroud

Proper operation of the thermostat can be checked by heating it in water (Plate 3-26). Upon reaching a temperature of 70 ± 2°C, the valve of a properly working thermostat must begin to open. The thermostat is not disassembled and repaired.

The radiator (Plates 3-27 and 3-28) is tubed, with the cooling surface executed either in the form of plates or in the form of a corrugated band 0.05-0.13 was in thickness, arranged in serpentine fashion. The radiator pipes are manufactured of tombac (L90) [copper-zine slloy]. The cooling band (serpentine), like the cooling plates for radiators of tractor-trucks and trucks shipped to countries with tropical climates, are manufactured of MZ cupper.

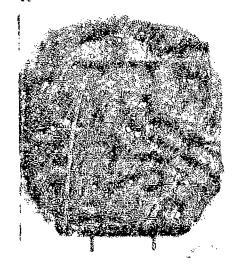
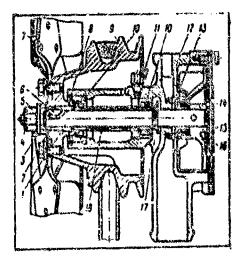


Plate 3-28. Radiator with fan shroud



TOPPH TERRIT CHECKER CONTINUES

Plate 3-29. Water pump with fan

1) shaft 2) conic bushing 3) washer

4) cotter key 5) nut 6) woodruff

key 7; fan 8) locking ring

n) pulley 10) bearing 11) grease

nipple 12) body 13) thrust washer

14) seal cup 15) vanez 16) spring

17) deflector 18) distance bushing

Tesing of the radiator for tightness is conducted with compressed air in a water bath with a pressure of 0.8 kg/cm² for radiators of normal duty and 1.8 kg/cm² for radiators for tropical duty. Upon discovery of a leak, up to five tubes are allowed to be closed off.

The radiator is installed in the truck in a motal frame, to which are fastened the louvres, radiator housing, and diffuser. Connection of this entire assembly to the truck frame is accomplished with two study welded to the bottom part of the radiator frame, with rubber cushions rounted on them.

The water pump (Place 3-29) is a contribugal one producing 240 liters/min at 2800 crankshaft tpm. The goar rates of the drive pulleys on the water pump and crankshaft are: 1.18: 1 for standard engines and 1.25: 1 for

eagings intended for use in the tropics

In the process of engine operation, bearing 10, the base hole widor the bearing in the body 12, the pushing essently and shaft 1 of the push wear out. Water push bearings are fitted with grease nipples, providing lubrication and protecting the bearings from dirt and cooling liquid which might reach them.

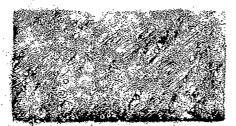
The fan is six bladed and installed on the front face of the water pump drive pulley. To increase exhaust of heat trou the radiator, the fan is encased in a shroud (diffuser), which promotes increased speed of the sir stress passing through the radiator. The shroud is fastened to the radiator frame.

Since December 1960, to increase fan offsetivenese, were efficient fans, with a blade installation angle of 35° instead of 30°, have been installed on all trucks, and the fan shreed (diffuser) has been semantal shortened.

The replacement for and fon shroud are interchangeable with the old ones.

Technical Servicing

Checking of cylinder head fastening bolts and duts is recommended to be conducted with a torque wrench (Plate 5-30). Torque must be within the limits 10-12 kg meters. Cylinder head must and bolt tightening should be accomplished in a determined sequence (Plate 3-31) on a cold engine.



Pirte 3-30. Checking torque on cylinder head fustoning nuts



Plate 3-31. Torquing sequence for cylinder head fastoning nuts

Clearence between the velves and teppete is chicked upon the appearance of valve noise, after which they are adjusted. Valve clearance adjustment should be performed separately for each cylinder, corresponding with the cylindering order (1-6-5-6-2-4). Clearance between the tappets and valves for intake and exhaust valves must be 0.20-0.25 as for engines with a 6.2 to 1 compression ratio, and must be 0.22-0.28 as for engines with a 6.5 to 1 compressions.

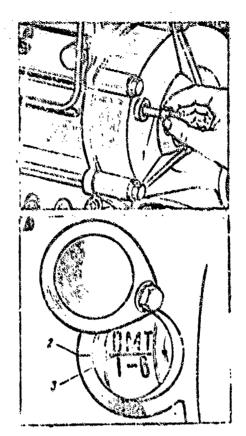


Plate 3-32. Method of setting piston of first cylinder at top dead center:

a) with a setting rod b) with mark on flywheel 1) setting rod 2 and 3) mark; on flywheel and case

Key: * TDC

Before adjusting clearance, it is necessary to:
Disconnect the fuel line from the fuel pump to the carburetor, restricting access to the valve boxes;
Disconnect the crankcase ventilation pipe and move it to the side:

Unsured bolts fastening the value box cover and remove the cover with its gasket. The value box cover should be removed carefully, attempting not to damage the sealing gasket.

Adjustment of intake and exhaust valve clearances should begin with the first cylinder, for which the piston is set at TDC on the compression stroke with a setting pin or according to markings on the flywheel.

In setting the number 1 piston at TDC, unscrew the setting finger 1 (Plate 3-52, a) and insert its other end in the same hole. Then, turning the crankshaft, continue until the end coincides with the hole in the campbaft gear. After setting the number I piston at TDC, serow the setting pin into its piece.

In setting the number I piston at TDC by the marks on the flywheel, the inspection hole cover on the bell housing must be open so that the flywheel rim is visible. Turning the engine crankshaft with a lever, the number i piston is set at TDC when the TDC mark S (Plate S-32, b) on the flywheel coincides with mark 2 on the bell housing. After setting the first cylinder at TDC, close the inspection hole cover and fasten it.

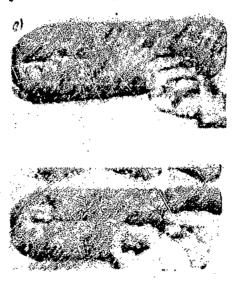
Clearance between the adjusting boits of the tappets and the valve stems is checked with a leaf gauge (Plate 3-33, a). If the clearance is outside the assigned limits, it must be adjusted. An adjustment is performed in this way:

Holding the tappet with one wrench on its flats, free the tappet adjusting bolt stop nut with another wrench:

Still holding the tappet, turn the tappet adjusting bolt until the required

clearance is attained;

Heiding the tappet adjusting boit with one wrench and the tappet with another, tighten the stop nut with third wrench (Plate 3-33, b).



Flate 3-35. Adjustment of valve clearance:

a) checking clearance with leaf gauge

b) adjusting clearence and Eightening stop

After adjusting the valves of the first cylinder, it is necessary to adjust the regaining valves in the same manner and replace the engine parts removed before valve adjustment.

Start the engine and listen to its operation. The warmed engine must work without valve noise, "couming" from the carburator and "backfiring" from the miffler.

Cocking compression in the engine cylinders. Compression in the engi-e cylinders (pressure of compression) lowers according to the amount of wear on the viston rings and cylinder walls.

The normal amount of compression in the cylinders of a warm engine sust be within the limits of 5.0-6.8 kg/cm². Compression adduction in the process of the engine's operation is allowed to 5.5-6.0 dk/cm2 for an in-line engine.

The difference between compression readings for separate cylinders must not exceed 0.7-1.0 kg/cm2.

Compression is taken on a warm engine. To check compression, it is necessary to:

Clean out the dirt collected in the spark plug depression:

Disconnect the spark plug lead and unscrew it;

Open the carburetor throttle and choke fully;

Insert the rubber tip of the compression gauge hose in the spark plug hole of the first cylinder and press it in tightly;

Rotate the crankshaft with the starter several times, to the compression

gauge fixes the maximum pressure in the cylinder;

Resove the rubber compression gauge tip from the spark plug hole, take the reading, and open the compression gauge release valve to release air; Repeat the operation for the remaining cylinders.

With a difference in pressure greater than 0.721.0 kg/mm2, pour 20-25 cubic cm of fresh oil into the cylinder with the lower compression and repeat the compression check. If the compression reading rises, this shows the presence of air leakage around the piston rings. If the amount of compression after pouring oil in the cylinder remains the same as the reading without oil. this points to leaks batween the valves and seats or valve burning.

Checking the coarse cleaning oil filter. It is necessary to clean the filter plates daily, turning the handle three to four rotations (Plate 3-34). The filter should be cleaned with the ongine fully were. Use of an extension lever to save turning of the filter handle is prohibited. If the filter handle is difficult to first, the cover bolts must be removed, and the filter removed and washed in ken tens.

When changing the oil in the engine crankcare, the fine cleaning filter element should be changed to residue should be resoved from the filter body by carefresing the plug with a wrench (Plate 7-3%). Before installation, the new filter element was be blown off with compressed air to remove pieces of card-oard, hair, and dust which settle between the cardboard plates and would clog oil lines in the future.



Plate 3-34. Cleaning the coarse cleaning oil filter blades



Plate 3-35. Removing the oil filter body drain plug

After changing the filter element, oil level in the crankcase should be checked and should be topped up if necessary. The fine cleaning filter cover bolts must be tightened gradually, criss-cross, so as to eliminate misaligning the cover and breaking its pars.

Adding and changing oil in the engine. Before adding oil to the engine, it is necessary to check the oil level in the crankcase. To check the oil level, it is necessary to stop the engine, wait a few minutes while the oil drains down, remove and wipe the oil dipatick, insert it to the stop, and remove it again. Oil level is determined according to marks on the dipatick. Oil must be (with full oil filters) at the level of the upper 4/4 mark on the oil dipatick. If the oil is located on the 2/4 mark, it is necessary to add.

When changing the oil in the engine crankcase, the used oil is drained while the engine is still warm. Not oil flows easily and washes dirt from the crankcase walls. The drain plug magnet should be cleaned. The fine closning oil filter element should be thanged simultaneously with changing the oil.

Fresh oil is poured in th ough the filler neck. After filling the crankesse with oil, it is necessary to run the engine for a short time to fill the librication system, then stop it and check the oil level on the dipatick.

The crankers air ventilation filter must be serviced at the same time that the engine crankers oil is thanged. Before servicing the ventilation filter, the case should be disassembled, closened, and carefully washed with

gasoline or kerusene.

In servicing the filter, pour oil used for the engine into a dish, place the filter screen half way into the oil, remove it and hold it for 7-10 seconds with the wetted end down, then shake it and place the screen in the filter body with the wetted end up. After servicing the filter, install the filter cover in its place.

The cooling system. During technical service, check the water level in the radiator, which must be 40 mm below the upper edge of the filler nock, or 70-80 mm lower for anti-freezing liquid. Clean and soft water is recommended for the system.

During hard freezing, it is necessary to warm the radiator using warming jackets on the radiator housing and on the engine hood. Working a cold engine leads to its intensive year.

During hard freezes, it is recommended that the system be filled with anti-freeze. The most widely used and reliable anti-freeze is type 40 (GOST 159-52), which freezes at a temperature of -40°C. Anti-freeze is poison, and it is therefore necessary to observe safety measures when handling it. During Winter, the cooling system should be filled with hot water, with the valves upon. The valves should be closed as soon as warm water begins to flow from them. Starting the engine without cooling liquid is not allowable, in that pouring cold water into a warm engine may cause cracks in the walks of the cylinder block and head. The condition of the radiator plug valves should be periodically checked and the condition of all gaskets should be systematically observed, not allowing liquid leaks from the cooling system.

The condensation tank should be filled to only half its volume (2 liters). Ine radiator must be periodically washed through from the outside with warm water, cleaning dust, dirt, and oil from it, and then blown out with compressed air. Special attention should be paid to the radiator during operation of the truck on dirt or dusty roads.

If "hard" water is used for engine cooling, scale will be formed in the cooling system. If scale is formed, or also if a significant quantity of cormsion products is observed in the water, the engine cooling system should be cleaned. It is recommended that the cooling system be cleaned once per year (preferably in Spring).

It is recommended that scale be removed from the engine cooling system in the following manner. To clean the cooling system, fill the radiator with a solution of approximately 20 grams of industrial Trilon per liter of water. After the truck has been worked for one day (no less than 6-7 hours), the spent solution is drained and the system is filled with a fresh one. Cleaning continues for 4-5 days. After completion of cleaning, the cooling system is

filled with a solution of 2 grams of Trilon per liter of water. The system may also be cleaned by adding hexameth (sodium hexamethylphosphate). The dose is 5-6 mg per liter of water.

When flushing the cooling system with water, the mequence of operations is an follows. First flush the cylinder block water jacket and then the radiator separately in the direction opposite water cir. Lation in the engine. The water hoses must be removed to flush the cooling system. Remove the thermostat pipe and take out the thermostat. Install the pipe, after which water at a pressure of 2-3 kg/cm² is directed into the thermostat pipe. During this, the drain valves must be open. Flushing must continue until clean water flows from the water pump pipe and the drain valves. After flushing, drain the water from the engine. The radiator is flushed separately. Water under pressure is directed into the bottom pipe of the radiator and flows out through the top pipe. The radiator cap must be closed. After the draining water becomes parfectly clear, install the water hoses connecting the engine to the radiator and close the drain valves.

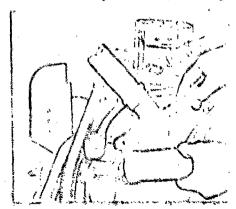
Before greasing the water pump bearings, it is necessary to clean dust and dirt from the lubricating point and unscrew the plug from the control opening. Grease is inserted with a grease gun through the grease nipple until all the old grease is forced out and fresh grease appears from the control opening (Piete 3-36).

After greasing the bearings, the plug is screwed into its place.

The drive bette of the fan, generator, and compressor, require periodic checking of their cension (Plate 3-57). They must be tight enough so that under a force of 3-4 kg, lateral deflection of the belt does not exceed 10-15 mm for the compressor drive belt and 15-20 mm for the generator drive belt.

Checking the amount of belt deflection is shown in Plate 3-38.

Tightening the generator belt is accomplished by moving the generator, and eightening the compressor belt is accomplished by moving the compressor.



Place 2-36. Grassing water pump bearings

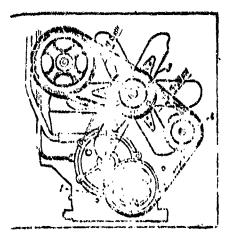


Plate 3-37. Checking drive belt tension:

1) crankshaft pulley 2) compressor pulley 3) water pump pulley 4) generator pulley

Disassembly and Assembly

Removing the power unit

The power unit (engine, clutch, and transmission) is easy to remove if the truck is parked on an inspection pit. This provides the best access to parts undermeath. Weight of the power unit is over 0.5 tons, and therefore for its removal it is necessary to use a hoist mechanism with corresponding load capacity and having a height to the hook of no less than 2 meters.

Before removing the power unit, it is necessary to drain the water from the cooling system; it is also desirable to drain the oil from the engine crankcase and from the transmission. It is recommended that small parts removed from the truck be collected in a separate can, and during disconnection of wires, screws and nuts should be screwed into place by hand.

Before removing the power unit from the truck, it is necessary to perform the following proparation tasks:

Remove the hood, together with the hood latch, also disconnecting the electric system wire from the fixtures and transfer blocks;

Disconnect the storage battery, removing the starter wire;

Disconnect the ground cable, unscrewing one cylinder head fastening bolt; Remove the connecting hoses of the cooling system radiator and heater, and disconnect the oil radiator hoses;

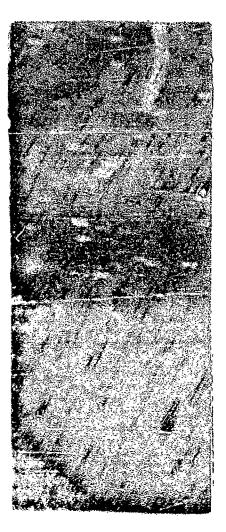
Remove the radiator louvres' drive rod. Free the radiator fastening and remove it together with the jacket, and remove the radiator hanger cushions:

Disconnect the carbuvetor linkage rod and the throttle and choke cables and remove the throttle return springs;

Unacrew the fastening boits of the bracket and remove it from the clutch housing:



Plate 3-38. Checking and adjusting fan and generator drive belt tension:
a) checking belt tension
b) changing belt tension and tightening nut



Disconnect the fuel line connecting the fuel tank and pump, and the air line running from the compressor head to the pressure regulator and to the air tank;

Disconnect the exhaust collector pipe from the exhaust manifold; Remove the inspection plate in the cab over the transmission;

Unscrew the transmission cover fastening bolts and remove the cover together with the shift lever;

Cover the transmission with a previously prepared piece of cardboard, fastening it with two or three holts to prevent foreign objects and dust from falling into the transmission;

Disconnect and remove the handbrake lever, the clutch pedal adjusting rod, and the handbrake drive rod;

Proc the bolts of the frent sotor mounts, of its two rear mounts, and also the engine brace rod fastening:

Unsersw the nuts and disconnect the propollor shaft flange, and unsersw the speedumeter drive sleeve;

Disconnect the transfer case control roi. If the truck has a winch, it is necessary to disconnect the universal shaft from the power take-off box and remove its slotted cover.

To remove the power unit from the truck, it is necessary to fasten a 1P-16550 hanger (Plate 3-39) on the extended cylinder head study, fasten the hook of the hoist installation into the hanger ring, carofully raise the power unit, move it forward and up, and set it on a stand or carriage. Remove the motor mount cushions from the frame cross member.

Engine Disassembly

Before disassembling the engine, it is necessary to clean the dirt and oil from 11, wash it with hot water, kerosene, or a degreesing solution, and blow it dry with compressed air.

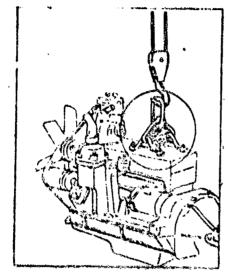


Plate 3-39. Hanger for removing power unit

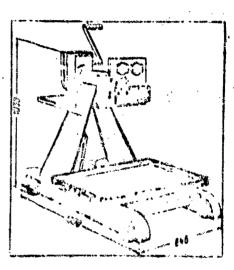


Plate 3-40. Model 2164 pertable stand for engine disassembly

A GARO model 2164 portable stand (Plate 3-40) or a carrying stand should be used for engine disassembly. For installing the engine on the stand, it is necessary to remove the oil filter body, and fasten the engine to the stand with bolts screwed into the threaded holes for fastening the filter body.

An engine on the GARO stard may be retated aroung a horizontal axis and fixed in any convenient position for its disassembly and assembly. The stand is equipped with wheals. A braking machanism has been provided for the front wheels of the stand for casters. The engine is turned on the stand with a worm reduction goar and manual drive. The maximum force applied to the drive crank is 16 kg.

When using a stand without the moving mechanism for engine disessembly, it is necessary to fasten the engine by its front care with screw clamps and fix the rear motor mounts to the stand frame with special study. In this case,

it is not necessary to remove the filter body. Rotation of the engine on the stand is accomplished manually around a horizontal axis. The engine may be fixed in a position convenient for its disassembly by an installing pin and a hole in the axis flange. W manisod tool: and attachments should be used for angine disassembly.

During engine disassamily, worn-in assembly surfaces of parts capable of future use without repair should be protected. Parts and standards removed from the engine should be placed on a rack or in a prepared can in which they are checked and deficiencies are eliminated after washing so that they may be returned for assembly.

When dissessiting an engine which operates on ethylated gasoline, safety measures should be observed.

Engine parts are interchangeable (although some require individual fitting when assembling the parts) and allow their non-individual replacement. Exceptions to this are the connecting rod caps and the main bearing caps. The former are machined in assembly with the connecting rods, and the latter are line bored together with the cylinder block. The connecting rods and their caps during assembly at the plant are stamped with numbers corresponding to their cylinder number, and the main bearing caps are stamped with numbers corresponding to their order in the block. The engine must be disassembled in the following order:

Unscrew the transmission fastening bolts with a box and wrench, separate it from the clutch housing with an assembly spade and, rocking it, remove the transmission with a nanger (Plate 3-41) and drawbar;

Disconnect the plates leading from the air filter to the compressor and to the valve cover, disconnect the brace, unscrew the top wing nut and remove the air filter:

Disconnect the fuel line and the vacuum line to the ignition vacuum advance, free the fastening nuts and remove the carbureter from the engine, and remove the insulating and backing gaskets; when unserwing the fastening nuts of the fuel lines, it is necessary to use two wrenches to protect them from damage. One of the wrenches prevents the sleeve from turning and the other unscrews the collar nut;

Disconnect the oil lines and water hoses of the compressor, remove the fastening nuts of the compressor and remove it from the engine. When disconnecting the compressor oil lines, it is also necessary to use two wranches:

theorew the boits fastening the 'ntake and the nuhaust manifolds and remove them together with the genket; the manifold bolts should be unscrewed with a socket wrench (Plate 5-42);

Unscrew the festening bolt of the ignition coil and remove it;
Before removing the distributor, the tensioning acrew (Plate 3-43, a)
should be loosened, after which the distributor is removed;
Unscrew the bolto and remove the timing adjustment plate (Plate 3-45, b);
Unscrew the stop serm of the distributor drive shaft (Plate 3-45, c) and

resove the shaft from its receptable (Place 3-45, d);

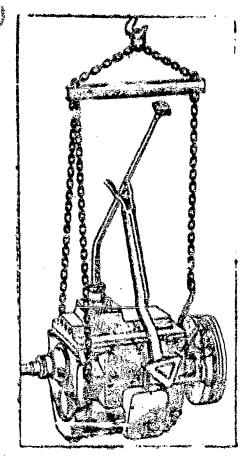




Plate 3-42. Removal of intake and exhaust manifolds

Plate 3-41 (left): Transmirsion hanger

Unscrew the spark plugs from the cylinder head;

Screw cylinder head removal lovers into second and fifth spark plug holes; Unscrow bolts and nuts of cylinder head fastening studs;

Unscrew bolts fastening the water outlet pipe to the cylinder head;

Remove the pipe with the steam gasket and thermostat:

Unserew the water connecting pipe to the compressor and the water valve to the heater from the cylinder head;

Remove the cylinder head from the block, attempting to avaid misslighment and damage to the gaskets;

Besove the bolts (Piet: 5-44, a) fastening the value covers, remove both covers with the bolt: and ring scals; if the ring gashets are melted onto the block, they must be carefully separated from the cylinder block surface with a screwdriver or sharp knife;

the crew the bolts and remove the cil filter body with its gasket, unverse the water temperature sending switch and the cil pressure sending switch; Loosen the plate tension bolt, remove the drive belt from the generator, unacrew the festening bolts and remove the generator;

that rew the funtening note of the furl purp and remove the purp with its grant;

Unsered the starter fastening bolts and, moving it from the receptacle in the clutch housing, remove the starter from the engine;

Remove the drive balt from the fen, unseres the fastening balts of the fan pump and remove the fan and water pump with its gasket:

For removal of the tappet guiding sections, unasted the boilts (Flate 1-64, b) fastening each section, and remove the front and rear sections and tappets as assembling with an assembly spade, shown in Flate 3-64, c; Mark the values with a punch or write on so 1 and of them their number according to order; install device 507-7097 on the cylinder plack (Flate 3-64) and, turning the puller acress, according to the value apring, remove the keys (Flate 3-64, and the apring with the value plate; release the device, remove it from the block, and marray; the value plate; release the device, remove it from the block, and marray; the value from the value from the value from the section in



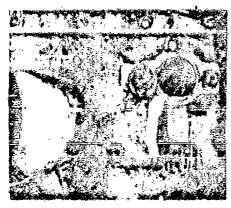
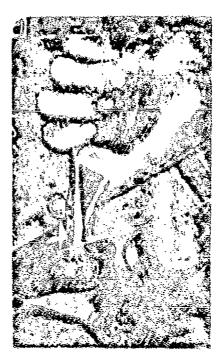


Plate 5-43. Removal of distributor and its drive: a) loosening the tension bolt of the distributor fastening; b) unscrewing timing adjustment plate bolts; c) loosening stop nut and unscrewing fastening bolt of drive shaft; d) removing drive shaft





the same way;

Rotate the engine on the stand trom side up, remove the boilts fastening the clutch housing cover and move it;

Remove of a boilts fastening the oil pan, remove it together with its gasker.
Repareting it with a seru-driver or knife;

To reserve the two-section oil pump; it is necessary to waserwe the bolts fastening that two oil lines (Plate 3-45) and the bolts fastening to oil pump body, and resove the pump with the gaskets;

Fo remove the case goer cover, drive down the retchet washer, magazew the retchet, remove the washer; remove the crankshaft pulley and the front motor sount bracket; the pulley is removed with the two balts (Plate 3-46, a) intended for fastening the caseshaft gear cover, or with a guller (Plate 3-46, b), or with a model 2492 puller, shown in Plate 3-47.

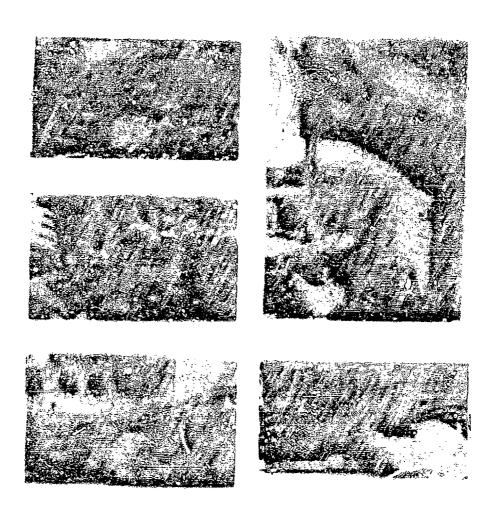
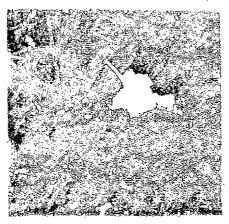


Plate 3-44. Valve removal: a) removal of valve cover fastening bolts;
b) removal of tappet guide fastening bolts; c) removal of tappet guide section; d) compression of valve springs e) removal of valve keys, plate, and opring



Place 1-45. Reserval of the oll pump

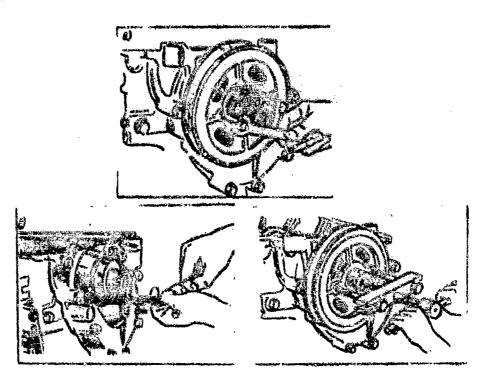


Plate 3-46. Removal of the timing gear cover: a) removal of the crankshaft pulley with pulling bolts; b) removal of the pulley with a puller c) unscrewing the cover fastening bolts

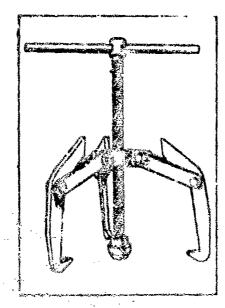


Plate 3-47. Puller for engine crankshaft puller



Plate 3-48. Withdrawing the piston and connecting rod from the engine criticist

Mascrew the boits (see Fiate 3-46, c) fastening the sem goar cover, remove the bracket of the engine fastening brace together with the two bolts, remove the camebant goar cover, trying not to damage the gasket, drive out the creakshaft pulley key, and remove the cover gasket and beffle washer:

Unpin connecting rod note with pliers and a screwdriver;

Unsersy the connecting sod cap whis, remove the caps together with the inserts and gaskets; before resoving the caps, it is necessary to check the presence of marks on them indicating the massively order of their cylinders, and if the massivers absent, mark the cylinder numbers on the caps:

Drive the piston and connecting rod from the cylinder as an assembly; the piston and rod cust be driven from the cylinder carefully, observing that the cylinder wall finish is not damaged by the edges of the big and of the connecting rod. A mathod of drawing the pistons from the cylinders is shown in Place 3-49;

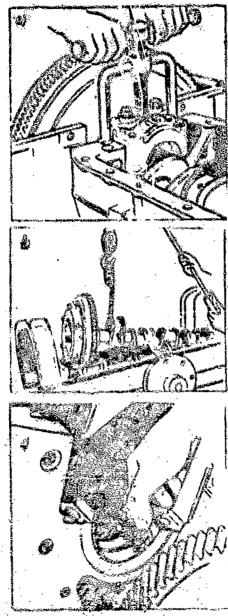
Before removing the main bearing caps, check for presence of numbers on them, unscrew the cap fastening bolts, and remove the caps and their caskets:

While removing the rear suin bearing cap, it is necessary to use the COP-1492 puller as shown in Flate 3-49, a. When all sain bearing caps have been removed, the number six connecting rod bearing journal is grasped by a special grapple, the hook of the hoist is raised and the shaft is raised (Plate 3-49, b) in assembly with the flywheel and clutch. During removal of the crankshaft, it is necessary to support and guide its free and so as to prevent misalignment. The weight of this assembly is not great, and in the absence of a hoist mechanism, the shaft can be removed by the efforts of two workers. For removal of the inserts from the cylinder block bed, it is necessary to prove the insert face from the side opposite its lock (as shown in Piete 3-49, c);

Through the holes in the face of the cashaft gear, unscrew the bolts fastening the support flange to the cylinder block with a mocket wrench (Plate 5-50, a) and drive out the cashaft in assembly with its goar (Plate 5-50, b). It is necessary to support the rear and of the can-haft and, besides this, carefully turn it so that the can lobes do not strike its bearings and the passages in the cylinder block;

The cambaft is driven out is assessly with the cambaft gear and the support flange. The cambaft gear is fitted on the face of the shaft with a maximum clearance of 0.000 mm or a roll claarance of 0.000 mm, and the diameter of the shaft journal at the goar fitting point is 10.015-16.036 mm. Gear rotation on the shaft is prevented by a key, and with of the shaft key may is 5.66525.080 mm with an allowable increase of key way width to a diameten of 6.445-6.880 mm for installation of overhaul diameter key;

For removal of the gran from the complete, it is necessary to bend down the lock washer, unusual the goar fastening not (Plate 3-51,0) and receive the locking washer;



Pints 3-49. Crankshaft removed:
a) executing the over usin bearing
cap b) recoving the crankshaft
c) removing the bearing insert





Place 3-20. Resoval of the comshaft: a) unacrewing the support flange featening bolts b) resoving the casshaft

fasten down the demander, install puller 10P-7968 on the goar, and pulling the gest off (Plate 3-51, b). The gest may be pulled using the attachment shows in Plate 3-51, c, for which the camebaft should be installed in the stackment, fastened in a vise, and the gest pulled off. The flange (Plate 3-51, d) and the teacing ring (Plate 3-51, e) are then re-waved. The "techness for pulling and pressing the cambaft gest is

shown in Plate 3-52:

The hole in the clutch housing is final bored in assembly with the cylinder block, and the clutch housing should therefore not be disconnected from the cylinder block unless necessary. To remove the bousing, it is necessary to remove the cylinder block from the stand, free the support clamps, and set it on benches or on a special stand. Therewe the bolts fastening the housing to the cylinder block with an angular socket wrench and remove the housing.

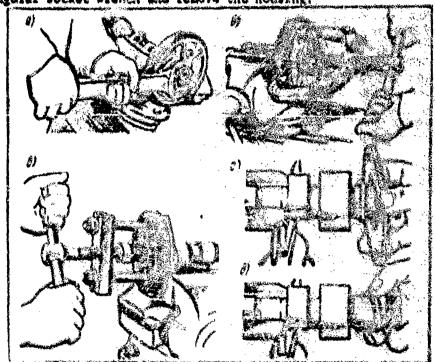


Plate 3-51. Disassembling the camehaft: a) uns. The ing the gear fastening nut b) pulling the gear with a puller c) pulling the gear with an attachment d) removing the support flunge e) removing the spacing ring

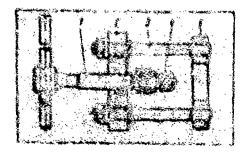


Plate 3-52. Attachment for pulling and pressing the cambaft gear:
1) screw 2) crossbar 3) stud
4) support bushing 5) ris flance

Washing of parts. All parts of the disassembled engine are subjected to classing, degreesing, washing, and subsequent checking. Steel and iron engine parts should be wathed in a water solution with a concentration of 1.5-28 sods and an additive of 0.2-0.39 sodium nitrate. For washing aluminum parts, a water solution of 18 triethonolaxine or pure hot water is used.

After weshing, the parts should be dried by blowing them off with compressed air. In that compressed air usually contains water particles, it is recommended that a moisture apparator be installed in the compressed air system. Linen cloths are recommended for use in rabbing the parts dry. Use of textile ends is not recommended, in that during their use for parts drying, lint and threads will remain on the parts and will move into the oil passages, clogging them.

The passages should be blown out with compressed air. If the passages are blocked they but be cleaned out with a metal rod or shaft.

Disabsumbly and Assumbly of Engine Components

The piston and connecting rod. For disassembly, it is recommended that the connecting rod in assembly with the piston be held in a vise and, using attachment 269-7975 (Pisto 3-53, a) remove the piston rings, draw out the piston wrist pin, took rings with smooth-jaw pliers (Pisto 3-53, b), press out the wrist pin and remove the piston from the connecting rod. Check the condition of the connecting rod small and bushing.

Before essembly with the piston, the connecting rod and its insert must be fitted to the crankshaft journal, the piston to the cylinder, the rings to the piston groves and the cylinder, and the wrist pin to the connecting rod small end and the piston holes.

The pistons must be assembled in a cylinder block at a temperature of 10-50°C so that the clearance between the cylinder walls and the piston skirt is within the limits of 0.08-0.10 mm. The size of the clearance is determined with a leaf gauge (Plate 3-54) 0.10 mm thick, 13 mm wide, and no less than 200 mm long. The leaf gauge is drawn into the clearance between the piston and the cylinder with a force of 2.25-3.65 kg. During assembly it is recommended that the piston be installed in the cylinder with its head down, and the leaf gauge must be located on the side opposite the notches in the piston skirt.

After assembling the piston in the cylinder, it is necessary to stomp its cylinder number on the head.

For messably with the connecting red, the piston is heated in a water bath or in an alectric heating device (Plate 3-55) to a temperature of 75°C. The wrist pin must go into the hole in the face plate of a heated piston smoothly, with the force of a thusb, and the same is true of the hole in the small end of the connecting red (Plate 3-56).



Plate 3-53. Assessmbly of a piston and connecting rod:
a) removal of the piston rings b) removal of wrist pin stop rings

Match the cylinder number of the piston and connecting rod.

The connecting rod is grasped in a vise, the piston is mounted on it, and they are connected by insertion of the wrist pin.

The piston must be assembled with the connecting red in a position so that the arrow stamp on the piston head is simed toward the stamped boss (mark) on the connecting rod. In this way, the oil-throwing holes in the hig end of the connecting rod are directed to the side opposite the grooves in the piston.

After assembling and checking the piston with the connecting rod, it is necessary to install the stop rings in the piston bosses.

Carefully struck the piston rings, selected according to groove and fitted to the cylinders, and install them on the pistons with a device.

Cleaning coke from the grooves of a piston which has been used is done with a device (Plate 3-57). Coke suit he resoved precisely and carefully, so as not to design the groove surface. Coke is removed from the oil exhaust holes with a drill (3 mm in diameter).



Plate 3-54. Fitting platens according to cylinders with a leaf gauge and dynamometer



Plate 3-56. Fitting a wrist pin to the disseter of the connecting rod humbing

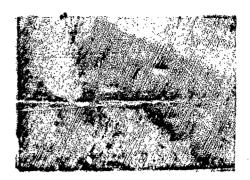
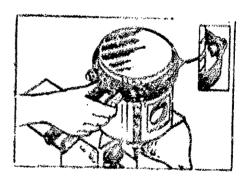


Plate 3-55. Heating pistons in an electric heating device



Plute 3-57. Cleaning coke from the piston grooves

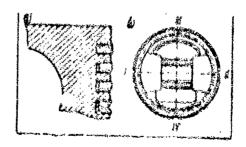
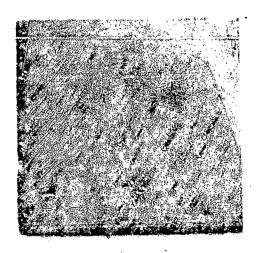


Plate 1-59. Piston ring instal.ation on the piston s) piston ring b) ring gap placement

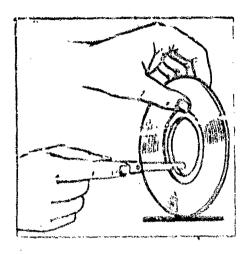
The schematic of piston ring installation and position of the ring spaces on the piston is cheen in Plate 3-58. Clearances in the ring looks after installation in the cylinder for new rings must be: for the top ring, 0.25-0.60 km; for the bettom ring, 0.25-0.45 km; for the oil ring, 0.15-0.5 km.

Clearance in the piston ring lock is adjusted with a small-grained file.

Clearance is checked with a loaf gauge when the ring is installed in the cylinder (Plate 3-59) or with a calibrating ring (Plate 3-60).



Place 3-59. Checking piston ring lock clearance in cylinder block



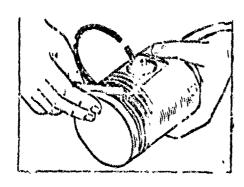
Place 3-60. Checking piston ring lock clearance with a gauge

Clearance and piston ring height between the ring and the groove of a new piston must be 0.035-0.072 mm for the compression rings, and 0.035-0.080 mm for the oil rings. The clearance is checked with a gauge (Plate 3 ol). The rings are fitted to the piston grooves in the process of rubbing, using small-grained emery paper. Rings installed in the piston grooves must move freely.

During removal and installation at the rings, it is convenient to use the ZOP-7985 device (see Place 3-53, a).

Ring elasticity is checked on a device (Place 3-62) using an elastic band. The execut of coepression force for new compression and oil rings must be no less than $2.15 \, kg$.

The connecting rod bottom end is machined in assembly with its cap, and therefore during disassembly, checking, and assembly, the rod and cap should be kept as a unit. Connecting rod bearing caps as a centered along ground surfaces of tension bolts. It is also not recommended to switch connecting rod



Plats 3-61. Checking clearance between ring and ston groove

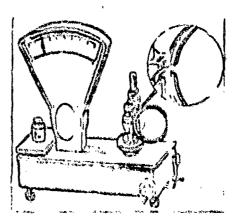


Plate 3-62. Checking piston ring elasticity on a device

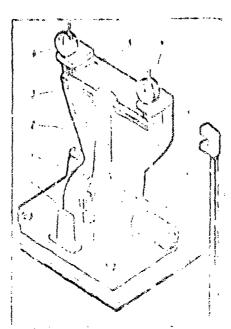


Plate 3-e3. Device for checking alignment of top and bottom connecting rod ends and straightening the rod: 1) body 2) connecting rod 3) mendrel for rod top end 4) indicators 5) index projections 6) wrench 7) mandrel for rod bottom end 3° support

manufacturing plant according to weight within the limits of 1440-1560 grams. In selection of new rods for assembly, they should also be chosen according to weight. Weight adjustment is performed by means of removing metal from the tail portion of the rod cap with a special tool.

During operation of the engine, the connecting rod is subjected to bending and twisting. Non-parallelness of the axes of the top and bottom connecting rod ends is not allowed to be greater than 0.04 mm, and deviation from their position in one plane (twisting) must be no greater than 0.06 mm on a length of 100 mm.

Checking for bending and twisting takes place on a device (Plate 3-63).
When checking, the mandrel 3 is inserted in the bushing of the top end of the checked connecting rod, and in the bottom end of the rod is installed mandrel 7 (without inserts) with the simultaneous installation of the rod and mandrel in the attachment. After this, lotating the rod on mandrel 7, it, together with mandrel 3, is pressed against the projections 5. The rod it considered upuble if both ends of mandrel 3 and the top end of the rod are pressed against the reference projections 5 and the indicators do not show deviation. Connecting rods having a deviation in exial parallelness no greater than 0.10 mm and deviation in exial twist no greater than 0.20 mm are allowed to be corrected.

Connecting rod correction takes place, without removing it from the device, with wrench 6, or grasping the condecting rod in a device (Plate 3-64). It is recommended that rod twist be corrected by first twisting it somewhat more than required to eliminate the deformation, and then twisting it in the opposite direction until the axes of the rod holes become parallel. This method of correction increases connecting rod resistance to deformation during its future use in an engine. Correction of a bent connecting rod may be performed on a hand press.

Disassembly of the crankshaft, flywheel, and clutch. The crankshaft is balanced in assembly with the flywheel and clutch. The allowable imbalance is no more than 150 gram cm. Disbalance of the flywheel and clutch may be eliminated by drilling holes 15 mm in diameter and no more than 25 mm in depth on the interior side of the flywheel at a radius of 184 mm.

Distance between the holes must be no less than 20 mm.

In order to maintain the balance of the crankshaft, flywheel, and clutch in assembly, it is recommended that marks be placed on the assembled parts before removal of the clutch from the flywheel, to be used as reference when reassembling the unit.

Removal of the clutch from the flywheel. Mark the relative position of the clutch jacket on the flywheel, note the installation position of the

halancing washers on the clutch cover, unscrew the clutch cover fastening bolts with a socket wrench, remove the pressure plate in assembly with the cover and clutch disengaging levers, and remove the clutch disk in assembly.

Elywheel removal. Unpin the flywheel fastening nuts, unscrew them with an angular wocket wrench (Plate 3-65), remove the Lywheel, and drive the bolts out of the crankshaft Plange. The flywheel diameter under the ring is 395.055-395.067 mm. The internal dimension of the flywheel ring is 394.700-395.025 mm. The ring can be removed from the flywheel only with a press. To fit a new ring, it must be heated to a temperature of 300-400°C, after which the ring is installed on the flywheel.

The flywheel is statically balenced in assembly with the ring. Allowable imbalance is no more than 100 gram cm.

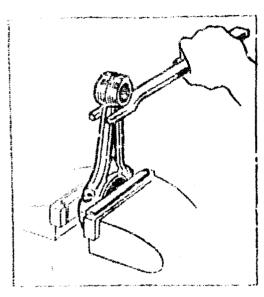


Plate 3-64. Connecting rod connection



Plate 3-65. Pemoval of flywheel from crankshaft

The surface of the flywheel which is assembled with the clutch disk is ground and polished. If marks or scoring appear on the working surface of the flywheel, grinding or turning of the flywheel surface is allowed to a dimension of 47 mm. The flywheel is fitted onto the crankshaft flange on six non-symetrically positioned bolts. If the fastening bolt holes are worn to more than the allowable dimensions, the flywheel must be replaced with a new one.

If the threads in the holes for fastening the clutch pressure plate are worn or damaged, now holes may be drilled between the old ones and tapped with a thread M 10 X 1.5. The diameter of the circumference on which these holes are drilled is 381 mm.

in the process of the engine's operation, the flywheel ring teeth are worn from the face in the places where they are engaged by the starter gear. If wear is present along the length of the teeth within the limits of up to 5 mm, the ring teeth should be accurately rounded off with a file. For wear over 5 mm, the ring should be removed and pressed on in a reversed position.

If the front bearing of the transmission drive shaft must be changed, it should be pulled out before removal of the flywheel, using puller 2-K-109 (Plate 3-66) or a crank puller (Plate 3-67).

Pulling the gear from the crankshaft journal is done with puller 1P-21305 (Plate 3-68).

A crunkshaft going into repair must be checked for absence of bending. The amount of bend must not exceed 0.05 mm. Checking of the shaft for bend is done with an indicator, with the shaft set on supports on its end main bearing faces (Plate 3-69). If the shaft is bent, it may be corrected on a hand press. For correcting the crankshaft, it must be installed or supporte by the end main bearing faces (Plate 3-70) and corrected with the hand press entil bend is eliminated, checking this with an indicator.

All cil passages in the shaft must be carefully cleaned of oil coking products and other contamination. It is recommended that passage cleaning be done with a metal jag wire followed by blowing out with air.

Assembly of the crankshaft, flywhool, and clutch. For assembly of the crankshaft, it is necessary to fit two supporting collars on the first main bearing surface, insert the key into the keyway, and press on the crankshaft gear.



Plate 3-66. Pulling the transmission dive shaft boaring

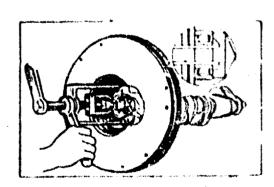


Plate 3-67. Pulling the transmission drive shaft hearing with a crank puller



Pulte 3-68. Pulling the gear from the crankshaft

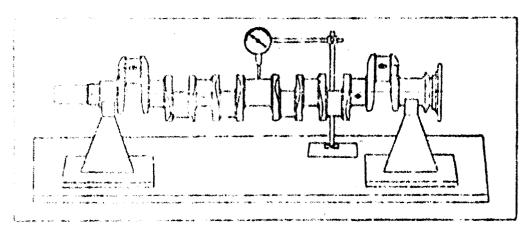


Plate 3-69. Checking the crankshaft for bend

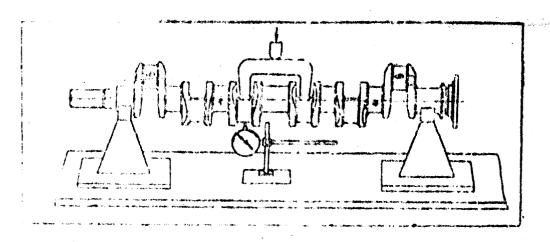


Plate 3-70. Correcting a bent crankshaft

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The shaft with the flywheel is set on ligs (Plate 3-71) and the working surface of the flywheel is checked for oscillation with an indicator. No more than 0.15 mm oscillation is allowed on a radius of 150 mm. Cotter keys are inserted in the flywheel fastening nuts. The cotter keys of each bolt must lie eightly against the bolt face.

Aubricate the bearing cavity in the crankshaft flange with i-13s grease and press the bearing for the front end of the transmission drive shaft into it. Screw in the lubricator for bearing lubrication. Check to see that grease from the lubricator reaches the bearing.

Using the transmission drive shaft for a mandrel, install a new clutch disk in its place. Install the clutch cover assembly on the flywheel and faster it with the bolts. Torque moment on the bolts must be 3-4 kg meters (assembly and adjustment of the clutch is presented in Chapter 6, "The Clutch").

During installation of the clutch on the flywheel, the markings made during disassembly of the clutch must be adhered to, so that the crankshaft balance temains as before. If this condition is violated, it is necessary to balance the crankshaft in assembly with the flywheel and clutch.

Dynamic balancing takes place on a special machine. Static balancing of the flywheel in assembly may be performed on balancing knives. When installed on the knives, the shaft must not spontaneously rotate when set in any position. The method of eliminating imbalance was presented above.

It is recommended that disassembly of the oil pump be conducted in the following order.

Wash the assembled pump in a degressing solution, pull out the pin holding the oil pickup with pliers, and remove it from the pump line. Unscrew the bolts fastening the oil exhaust pipe, disconnect it, and remove the gasket. Unscrew the reduction valve plug and pull out the spring and plunger.

For two-sectioned pumps: unscrew the bolts fastening the pickup line of the top and bottom sections and disconnect them with the gaskets. Unscrew the by-pass valve plug, and remove the spring and ball. Unscrew the bolts fastening the body of the bottom section and remove it from the top body in assembly with the axle and driven gear of the bottom section, and also carefully remove the regulating gasket.

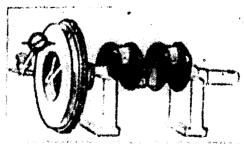


Plate 3-71. Clecking oscillation of flywheel working surface

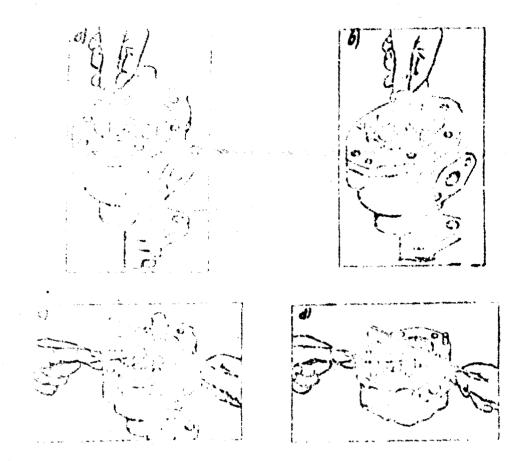


Plate 3-72. Checking clearances in an oil pump with the gauge and straightedge:

- a) checking clearance between gear teeth and body walls
- b) checking clearance in gear teeth engagement
- c) checking clearance between top section gear faces and intermediate cover d) checking clearance between bottom section gear faces and intermediate cover

To draw the drive shaft with its gear from the body, it is necessary to for a single-section pump, knock out the pin, pull the pump drive gear, and withdraw the shaft in assembly with the gear; for a two-section pump, having removed this drive gear, draw out the drive gear and intermediate cover together with the shaft.

To press off the shaft of the driven gear, it is necessary to stand the top body of a one-section or two-section pump, and also the body of the bottom section of a two-section pump on the gaskets and press out the shafts.

For removal of the drive gear, it is necessary to: for a one-section pump,

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install the shaft in the device or a vise and pry up the lock ring with a screwdriver, press the drive gear from the shaft, and pry the key from the key way; for a two-section pump, besides this, move the top section drive gear upward along the shaft, remove the lock ring and press off the bottom section gear, pry the key from the shaft key way, remove the intermediate cover, and press off the top section gear and pry out the second key.

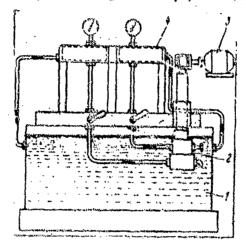


Plate 3-73. Schematic of stand for testing oil pumps:
1) oil bath 2) tested pump 3) electric motor 4) stand chamber

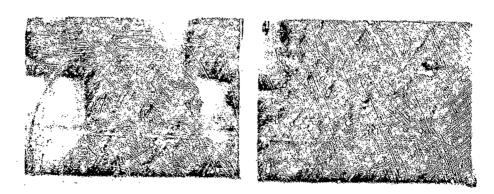


Plate 3.74. Disarrembly of oil filters: a) removal of fine cleaning filter element b) removal of coarse cleaning filter

The parts, cleaned of oil residue and washed out in kerosene, must freely save in the body of the reduction valve.

The reduction valve spring must have the following dimensions: length in

free state, 72 mg; under load of 3.2-3.5 kg, 57 mg. The spring of the bottom section by-pass velve of the pump must have the following dimensions: length in the free state, 35 mg; under load of 1.7-2.1 kg, .2 mg. Working pressure of the by-pass valve is 1.2-1.5 kg/cm².

Assembly of the pump takes place in the opposite sequence to its disassembly. The parts going for assembly must have been exceedilly mashed out. It is desirable that all paper gaskets be replaced with new ones. Oil pump parts must be washed in a degressing solution, and their usubility must be checked.

During assembly of the pump, it is necessary to pay attention to the following: the shaft of the driven gear must sit in the body with a roll clearance of 0.10-0.052 mm. The pump drive gear must be fitt' I on the drive shaft with a clearance of 0.014 mm or a roll clearance of 0.025 mm. The pump drive gear pin must be exactily flattened on both ends. Clearance between the body face and the drive gear must be 0.3-0.5 mm.

During installation of the gear in the pump body, it is necessary to measure the clearance between the gear tooth and the walls of the pump receptable with a gauge. This clearance must be within the limits of 0.025-0.275 am (Plate 5-72, a). The clearance in gear engagement must be within the limits of 0.150 0.550 am (Plate 3-72, b). The clearance between the gear faces and the intermediate cover of the body must be within the limits of 0.10-0.25 mm (Plate 3-72, c and d).

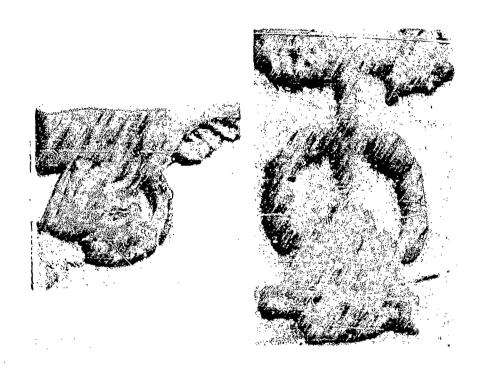
The pump drive shaft, installed in the body, must rotate freely by hend without binding after the bolts are tightened. Clearance between the pump gear faces and the cover is adjusted with the gaskets. In case of binding, add gaskets

The oil pickup, hanging on the pipe, must freely roll on its shaft, and the pin must be spread so that it cannot fall out. It is recommended that the associated pump be checked. The schematic of a stand for checking pumps is shown in Plate 3-75.

Checking of the pressure developed by a pump takes piace in liquid potrelatus T (COST 1240-51) with the latter at a temperature of 18-20°C. Pressure at 675 pump revolutions per minute must be no less than 2.5 kg/cm² ror the upper section and no less than 0.9 kg/cm² for the lower section. The reduction valve must open at a pressure of 3-4 kg/cm², and the by-passed valve in the lower section must open at a pressure of 1.2-1.5 kg/cm².

Disassembly of the oil filter body. For disassembly, it is necessary to install the filter body in a device or a vise, unscrew the bolts fastening the cover, and comove the cover and gasket. Remove the top spring compressing the changeable filter element. Pull the fine cleaning filter element from the

body (Plate 3-74, a), and remove the bottom compressing spring.



Plute 3-75. Pulley removal:
a) unscrewing the nut b) pressing off the pulley with a puller

Unscrew the boits fastening the coarse cleaning filter element, pull out the sleash in assembly (Plate 3-74; b), and remove the gasks: Unscrew plug 3 (Plate 3-21) of the by-pass valve together with the backing ring, and draw out spring 5 and bolt 6.

Disassembly of the coarse cleaning filter element is performed in case of damage to the blades or heavy dirtying.

Assembly of the oil filter body takes place in the reverse sequence. The parts are carefully cleaned and the fine cleaning element and paper gaskets are changed. The coarse handle must be easily turnable by hand. The moment of rotation must be no more than 0.4 kg meters. The hy-pass valve has a length in free state of 52 mm, and under a load of 0.9-1.1 kg, its length is 44 mm.

The body cover bolts must be tightened (tightening torque 9-12 kg meters) sequentially, so as not to damage the cover flange. The assembled filter is checked for tightness under pressure of 6 kg/cm² for a period of one minute.

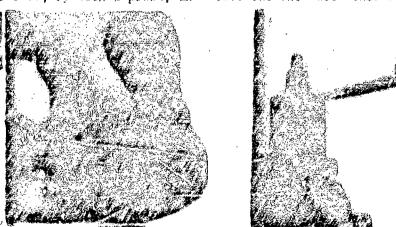
Check operation of the by-pass valve, which must open under pressure of 1.0 kg/cm².

It is recommended that the water pump be disassembled in the following order.

Unscrew the bolts fastening the cap and remove the cap and gask : Unscrew the lubrication fitting from the body. Unscrew the bolts fastening the pump cover and remove the cover and gasket.

Unpin the nut fastening the pulley and unscrew it, holding the shaft by its blade to prevent rotation. Plate 3-75, a, shows how to hold the shaft to prevent rotation. Remove the pump shaft pulley with a press or with a 20P-7968 puller with a 20K-97-1 cap (Plate 3-75, b). Unscrew the water pump cap.

Remove the bearing lock ring with pliers (Plate 3-76, a). Remove the conic bushing (Plate 3-76, b) and key. Press off the water pump shaft in assembly with the vence and packing (Plate 3-77, a). Press the bearing out of the pump body (Plate 3-77, b) with a press, and drive out the water-throwing washer.



Place 3-76. Removal of bearing lock ring and conic bushing a) removal of ting b) removal of conic bushing

To disassomble the seal from the vanes, it is necessary to remove the spring ring of the water-throwing washer and the lock ring of the seal from the shaft, then remove the textolite support washer, the rubber collar (gland), the gland compression ring, the compression spring, and the gland support ring.

When changing the vanes, drive out the vane fastening pin and press it from the shaft. If the bearings and parts of the seal assembly (support washer and collar) are worn, they should be replaced with new ones. The support washer is manufactured of graphitized textolite.

When changing the parts of the packing unit, it is necessary to remove the pump cover, press shaft 1 (see Plate 3-29) in assembly with vanes 15 and the glands out of the body, replace the worm parts of the packing unit, and assemble the pump.

Assembly of the water pump is conducted in the following sequence: assemble the seal and vanes on the shaft, for which the vanes should be pressed on and fastened with a pin; fit the support rim, compressing spring, compressing rim, rubber collar, and textelite support washer on the shaft in order; fasten the soal with the lock ring and fit the spring ring for the water-throwing washer on the shaft, setting it the ring groove of the shaft.

Insert the shaft in the pump body, fit the water-throwing washer on the shaft, and press on the rear bearing; screw the grease fitting into the body and fill the pump body hollow with 1-13c grease, install the spacing bushing, press on the front bearing the same as the rear one, fasten the bearing with the lock ring (see Plate 3-76, a), after which the shaft must rotate freely in

Install the cover and gasket on the pump body and fasten it with bolts, set the key in the shaft key way, install the conic bushing, install two more bolts for fastening the pump to the engine in holes in the body, mount the generator rensioning bar on one of the bolts, install the pulley and set it in its place, screwing on the pulley fastening nut; If a stamped pulley is used, the boss is fastened onto the conic bushing; pin the pulley nut, install the cap on the body with a gasket and fasten it with bolts.

For disassembling the radiator from its housing, it is necessary to unscrew the nuts fastening the radiator housing to the sides of the diffuser and remove

theorem the bolts and nuts fastening the diffuser, sides, and louvres, and then disconnect the parts.

During disassembly of a radiator on which an oil radiator is installed, it

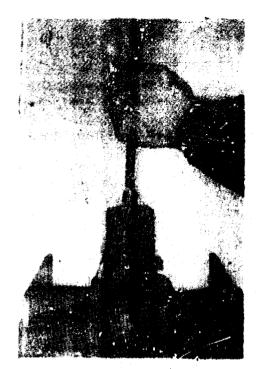




Plate 3-77. Pressing out water pump parts: a) shaft b) bearings

is necessary to unscrew the bolts fastening the oil radiator to the two brackets which are welded to the louvre frame and disconnect the oil radiator.

Assembly of the unit takes place in the reverse order.

Assembly of the engine

It is recommended that engine assembly take place on a rotating stand without the moving installation or on a model 2164 GARO stand with a moving installation (see Plate 3-40).

All parts and components going into assembly are carefully washed and checked for usability in assembly. Assembled parts must be selected and fitted, and if necessary, assembled with specific parts. Methods of fitting assembled parts are presented in corresponding sections touching on each part or component.

The cylinder block, either new or rebuilt, goes into assembly complete with camshaft bushings, valve guides, and clutch housing. All oil passages in the engine must be cleaned out and blown out with compressed air.

Before assembly, the cylinder block should be fastened on the stand, turning its crankcase separation plane upward. The main bearing caps are bored together with the cylinder block, and are therefore not interchangeable. Boring

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takes place with gaskets, 0.05 mm thick, installed in the cap butt joints. The caps of the middle and rear brarings are fastened with four bolts, and the caps of the remaining bearings are fastened with two bolts each. The holes for fastening the main bearing caps are symmetrical in relation to the crankshaft axis.

The main bearing caps are centered in slots in the block along the sides. These slots are positioned non-symmetrically, eliminating possiblity of incorrect installation. The nominal dimension of the main bearing insert beds is 70.50-70.53 mm. Total difference in hole axiality must not exceed 0.04 mm and deviation between the axes of two adjoining holes must not exceed 0.0 mm.

Crankshaft installation. Remove the main bearing caps, rub the beds in the cylinder block and in the caps under the inserts with a cloth, and blow the cylinder block out with compressed air. Install the selected inserts in the main bearing beds. Check coincidence of the oil passages.

insert the rim with the 7th bearing packing glands in the slot in the block and in the slot in the cap (Plate 3-78), and also insert the rubber seals of the rear bearing face in their receptacles (Plate 3-79). Install inserts in heds in the main bearing caps. Check the crankshaft in assembly with the flywheel, clutch, camshaft goar, and support collars, set it in a convenient position, blow out the oil passages with compressed air and rub the main faces of the shaft with a cloth.

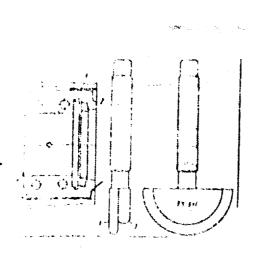


Plate 3-78. Installation of the rear main bearing seal in a cylinder clock:
1) seal rim 2) graphite-asbestos seal
3) small projection of semi-circular mandrel 4) large projection of semi-circular mandrel 5) cylinder block

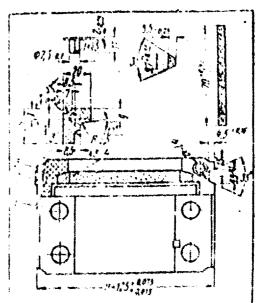


Plate 3-79 Rear main bearing seal:
1) rear hearing cap 2) wooden seal
3) rubber seal 4) graphite-ashestos gland

Lubricate the surfaces of the upper inserts with clean engine oil and lay in the crankshaft (see Plate 3-49, b). Lay the 0.05 mm thick brass inserts in the cap butt joints. Lubricate the surfaces of the bottom inserts and wain faces of the shaft with oil. Install the main bearing caps in their places. The side surfaces of the caps which have the numbers must be directed toward the camehaft side of the engine.

Install the bolts with spring washers, and, screwing them in at first by hand, finally tighten them with an angular socket whench. It is recommended that the middle and rear caps be tightened diagonally.

Theck main bearing bolt tightness with a torque wrench. Tightening torque must be 18-10 kg meters for the middle and rear bearings, and 11-13 kg meters for the remaining bearings.

The front crankshaft bearing has support rings (Plate 3-80) made of a bimetallic band on each of its sides to absorb axial stresses arising during operation of the shaft. The support rings, which have sides cast of an antification alloy, are for the front support ring on the side of the camshaft gear, and the mear one on the side of the crankshaft. The total clearance between the support ring and the crankshaft journal, and also between the support ring and the camshaft gear is set within the limits of 0.05-0.23 mm. The means of measuring sxial clearance is shown in Plate 3-81. Clearance between jig faces and the faces of the remaining main bearings must be no less than 0.75 mm.

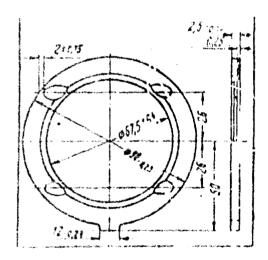


Plate 3-80. Crankshaft support

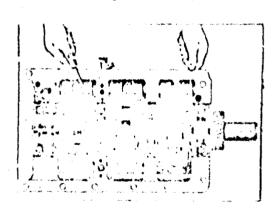


Plate 3-81. Checking crankshaft axial clearance

Support rings (front and rear) are produced with a thickness within the limits of 2.46-2.50 mm. The rear support ring is produced with a repair thickness dimension within the limits of 2.66-2.70 mm, which is set with ring wew.

when crankshaft slack is greater than 0.25 mm.

Check ease of rotation of the crankshaft. The moment of shaft rotation must be no greater than 7.0 kg meters.

Wet the wooden seals in oil, insert them in the vertical slots of the rear main bearing cap, press them to the end with a mallet, and then smooth off the projecting faces of the seal flush with the separation plane of the cylinder block.

Sealing the crankshaft. To eliminate oil leakage from the front end of the crankshaft, a rubber casing type gland is installed on the front end of the crankshaft.

A spiral oil-moving passage is located near the rear main bearing gland on the crankshaft base.

Before installation of the crankshaft, the rear main bearing rims with asbestos packing must be tightly fitted into their nests in the bearing c and cylinder block. Gland packing must not fall between the surfaces of the cap and the cylinder block after installation of the shaft and tightening of the bearing caps.

Thin-walled bearing irserts are manufactured to a high degree of precision, and therefore their repair or any sort of fitting with filing or scraping is not allowable. The only method of eliminating insert deficiencies is their exchange.

There must be a clearance between the crankshaft cheek and the bearing insert within the limits of: for main bearings, 0.026-0.100 mm, and for connecting rod bearings, 0.026-0.083 mm. Checking the amount of radial clearance may be done with a set of control gauges made of copper foil, 6 025, 0.05, 0.075, and 0.1 mm in thickness, cut in the form of strips 6-7 mm wide and somewhat smaller in length than the width of the insert. Edges of the gauges must be smoothed with an abrasive whetstone to prevent damage to the insert surface.

The radial clearance checking operation takes place in this way: remove the cap and insert from the bearing being checked and lay the previously lubricated minimum thickness (0.025 mm) control gauge on the insert surface. After installation of the cap and insert in their place and tightening of the bolts, rotate the shaft by hand. During this, the bolts of the remaining bearing caps must be loosened. If the shaft is rotated too easily, the clearance is greater than 0.025 mm. After this, the gauge is replaced with the sequential thickness sizes until such time as the shaft is impossible to turn. The thickness of the gauge with which the shaft can be rotated with noticeable effort is taken as equal to the actual amount of clearance in the bearing.

During checking of the clearances with control gauges, it is recommended that the bearing bolts be tightened with a torque wrench to attain cightness which is equal and constant in amount. To avoid damaging the insert surface, the shaft should not be rotated more than 60-90°.

A simpler and sufficiently reliable method of checking, for an experienced mechanic, is checking clearances in bearings which are lubricated with oil 'oy feel." In this way, it is considered that with normal clearances, the connecting rod (without the piston) assembled on the shart journal with a fully tightened cap, must freely fall under its own weight from the horizontal position down to a vertical one. With normal clearances in the main bearings, the crankshaft, with fully tightened caps and without connecting rods, must be able to be rotated manually with a starting crank and without noticeable effort.

Exchange of crankshaft bearing inserts. The inserts are exchanged as a pair-supper and lower halves simultaneously.

In exchanging inserts without repair of the shaft, the exchange operations may be performed on the engine without removing it from the chassis, just as on an engine mounted on a repair stand. In this instance, for exchange of connecting rod inserts, it is necessary to remove the oil pan and oil pump pipe with a pickup. Then, sequentially rotating the crankshaft 120° at a time, it is set in a position for removal of the first and sixth, second and fifth, and third and fourth connecting rods.

Having set the crankshaft in the required position, it is necessary to; unpin and unscrew the connecting rod bolt nuts, remove the rod cap, move the rod and piston slightly upwards along the cylinder, extract the insert from the rod and cap, wipe down the insert beds with a cloth, and install the new inserts; wipe down the connecting rod journal on the crankshaft, lubricate it with engine oil, pull the rod down to the face, install the rod cap in its place so that the number on the cap and or the rod are on the same side, screw on the connecting rod bolt nuts, place one gasket 0.05 mm thick in the butt joint under the cap, tighten the nuts with a wrench to a torque moment of 8-10 kg meters and pin them.

The same operation is conducted for removal of the next pair of inserts.

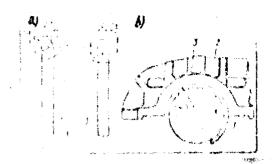


Plate 3-82. Exchange of crankshaft upper inserts: a) insert extractor b) method of extracting upper insert; 1) upper insert 2) cylinder block rib 3) insert extractor

After exchanging the connecting rod bearing inserts, it is necessary to install the oil pump pickup and delivery tube with the oil pickup, which have previously team cleaned and washed in kerosene, had their gaskets checked and replaced if necessary, and them been installed on the engine, making sure that the oil pickup does not touch the walls of the oil pan, after which the oil pan is fastened into place and filled with oil.

For changing main bearing inserts, it is necessary to unscrew the main bearing bolts, remove the caps, and change the inserts.

For changing inserts without removing the crankshaft, the special extractor 3 (Plate 3-82) is used, easing removal of the upper half of the insert. For this; the bearing cap is removed; the crankshaft is set so as to expose the oil passage holes in the main bearing face; the extractor 3 is inserted into the oil passage hole; the crankshaft is turned until the extractor dog lies against the face of the insert and its head is set parallel to the formed exterior surface of the insert; the crankshaft is rotated 180°, and the worn out bearing 1 is extracted. The new insert is installed in the reverse sequence. The shaft face must be carefully dried, and the insert lubricated with liquid oil.

After changing the insert, is is necessary to install the cap in its place, placing a gasket on each side of it and tightening the bolts. Tightening torque for the front and intermediate bearings is 11-13 kg meters, and for the cap of the middle and rear bearing, it is 8-10 kg meters. Lock washers in good condition are installed beneath the bolt heads.

After tightening only the main bearings, the torque applied to rotate the engine crankshaft must be no greater than 7 kg meters, and after tightening the main and connecting rod bearings, it must be no greater than 10 kg meters.

The dimensions of the crankshaft bearing inserts are selected according to the diameter of the shaft journals of the assembled engine. The connecting rod journals may be measured without removing the shaft from the cylinder block. For measuring the main bearing faces, the shaft must be removed. After any exchange of inserts, it is necessary to check the clearance in each of the bearings, so as to insure that shaft repair and selection of repair insert dimensions were done properly.

If the crankshaft is changed in an engine, it is also necessary to change all the inserts. For such enceschange, the plant produces set No. 120-1000107-B -crankshaft with normal dimension connecting rod and main bearing inserts. The set includes: a new crankshaft, seven pairs of main bearing inserts, six pairs of connecting rod inserts, and two thrust rings.

During the process of the engine's operation, appearance of small localized breaks in the anti-friction layer of main or connecting rod bearing inserts,

of insert failure.

When installing pistons with connecting rods, the cylinder block is turned so that its cylinders are up. Laterally, one after the other, take the piston and connecting rod in assembly. Carefully wipe the insert bed in the big end of the connecting rod with a cloth, unscrew the nuts and remove the connecting rod cap and inserts which are installed between the connecting rod and the cap. Place brass or copper ends on the connecting rod holts to protect the cylinder wall from damage during installation of the connecting rod and piston.

Check and blow out the holes in the bottom end of the connecting rod serving to splash oil on the cylinder holes and the camshaft lobes, place the inverte in the rod and the cap and check coincidence of the oil passages. Dry oif the upper connecting rod insert and piston with a cloth, instail the rings on the piston, and place the ring but? joints on the piston in the proper position (see Plate 3-58). Wipe down the cylinder block and the connecting rod journal of the shaft with a cloth.

imbricate the surfaces of the connecting rod insert, piston, piston rings, and cylinders with clean engine oil.

Mount device K-1288 (Plate 3-83) on the piston from the skirt side and install the piston together with the connecting rod in the cylinder (Plate 3-84). The "forward" mark on the piston head must be directed toward the front part of the engine. The piston rings must be freely compressed in the device. Drive the piston along the cylinder with the wooden mandrel (Plate 3-85) and lead the connecting rod bearing to the crankshaft journal. Lubricate the connecting rod journal of the shaft and pull the bottom end of the connecting rod to the connecting rod journal. Remove the protective caps from the connecting rod bolts, set the insert and connecting rod cap in place, and tighten it. The side of the connecting rod cap having the stamped connecting rod order number must be directed toward the valve chamber side of the block. Ensure that the diametric clearance in the connecting rod bearings was selected normally.



Plate 3-d3. Device K-1288 for piston installation



Plate 3-84. Installation of piston and rings in cylinder with a device



Plate 3-85. Moving piston and connecting rod along cylinder with wooden mandrel

Check the total clearance between the connecting rod bearing faces and crankshaft journals with a gauge. The clearance must be 0.075-0.260 mm.

It is expedient to install the picton and connecting rod assembly in the cylinders in the following sequence: first and sixth; second and fifth, third and fourth.

Finally, tighten the connecting rod bolt nuts and check their tightness with a torque wrench. Torque moment on the nuts must be within the limits of 5.5-8.9 kg meters. In tightening the nuts, it is necessary to bring their close into position for pinning. Bringing the nuts to coincidence between their closest slots and the pinning hole must be done only in the direction of increasing tightness.

Check the tightness of main and connecting rod bearings by means of rotating the crankshaft. The moment of sheft rotation must be no greater than 10 kg meters. Having finished checking the tightness of the connecting rod bearings, it is necessary to pin the rod belt nuts.

Assembly of the commshaft includes installation of the spacing ring 6 (see Pluts 3-13), support flange 5, key 4, and gear 1.

The gear must be pressed onto the shaft until it rests against the spacing ring. After pressing on the gear, the lock washer is installed, the nut is screwed on, tightened until it refuses to move, and a washer is driven up against one of the flats of the nut. The support flange must move freely after this, and clearance between the flange and the face of the support check must

be 0.08-0.21 mm.

Journal oscillation of the large camshaft gear hub on the side lying against the support flange is not allowed to be greater than 0.04 mm. Oscillation of the journal on its rim is not allowed to be greater than 0.16 mm. Gear oscillation is checked with an indicator (Plate 3-86).

For pressing on the gear, the shaft must be mounted on a device (Plate 3-87) and fastened in a vise. Then press on the gear.

In the process of engine operation, the support flange also wears out. Increased axial clearance causes longitudinal stack in the shaft and a knock in the engine. The amount of clearance may be decreased by decreasing the height of the spacing ring.

Axial clearance in the camshaft may be checked without removing the engine from the truck, or with an engine already removed, with an indicator, for which it is necessary to remove the camshaft gear cover, mount the indicator (Plate 3-88) against the journal of the camshaft gear rim, and measure the axial clearance, shaking the gear slightly with a tap wrench.

If the camshaft bushings are worn more than the allowable limit, it is necessary to press ther out of their nests in the cylinder block with a device (Plate 3-89) and press in new bushings using the same device.

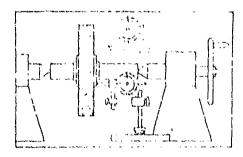


Plate 3-85. Checking journal cacillation of the hub and rim of a cranksneft gear



Plate 3-87. Procsing on a camshaft gear with a device

When pressing in rebuilt or new bushings, the holes for lubrication in the bushing must exactly coincide with the passages in the cylinder block body. Pressed-in bushings must be fitted by development to the diameter of the support journals of the camshaft to assure a normal clearance in the bearings within the limits of 0.05 0.10 nm.

Installation of the camshaft and the cam gears. Wipe out the camshaft supports in the cylinder block with a cloth, check coincidence of the oil passages and lubricate the shaft journals and lobes with engine oil.

Install the camshaft in the cylinder block with the gear and flange in assembly (see Plate 3-50, b), connecting the crankshaft and camshaft gears so that the tooth noted with a dot on the crankshaft gear goes into the cut noted with a dot on the camshaft gear (Plate 3-90). Check the amount of clearance between the teeth of the camshaft gears.

For checking clearance in the camshaft gear teeth, use of a device which fastens on the front face of the cylinder block with a screw (Plate 3-91) is recommended. The end of the lever should rest against the lateral surface of the camshaft gear. With the crankshaft remaining stationary, rotate (by the amount of clearance) the camshaft gear, taking up the clearance between the lear teeth, and determine the amount of clearance according to the hand on the indicator. For used gears, the clearance is allowed in the limits of 0.04-0.25 mm, and for new gears, the allowable clearance is 0.04-0.12 mm. Clearance should be checked in three points at an angle of 120°, and deviation in the clearance for used gears must be no greater than 0.10 mm, and for new years, it must be no greater than 0.06 mm. Having checked the clearance, it is necessary to colocate the holes of the support flange with the threaded holes in the cylinder block and fasten the camshaft with bolts and lock washers, using a socket wrench (see Plate 3-50, a), inserting it in the gear holes.

The tightening moment of the flange fasteding holts must be 2.3-2.8 kg meters, after which the axial clearance must be maintained within the limits of 0.08-0.21 mm. Lubricate the gears, fit the oil deflector on the end of the camshaft, install the screen and camshaft gear cover with gaskets and faster them, installing the bracket for the engine suspension swaybar beneath the first and second bolts on the right side. The bolts are tightened in two peases. Torque moment must be 7-8 kg meters.

Installation of the oil pump and engine oil pan. Turn the block crankcase upward. Set the oil pump on the cylinder block, connect its drive gear with the gear formed on the camshaft, and fasten the body and pipe leading oil to the engine mair oil line to the engine block with bolts. Install gaskets beneath the pipe flange. With installation of a two-section oil pump, besides this, fasten the pipe conducting oil to the oil radiator, also installing gaskets beneath the flanges.

Before installing the oil pan, it is necessary to make sure that there are no foreign objects inside the engine. After that, liberally lubricate the bottom part of the cylinders with oil, and also lubricate the external side of the piston wrist pins, and the main and connecting rod bearings.

Lay a gasket on the cylinder block plane, blow out the oil pan with compressed air and install ton the cylinder block. Scrow in the bolts with lock

washers by hand, and tighten the oil pan using a socket wrench. Tighten the bolts in two passes.

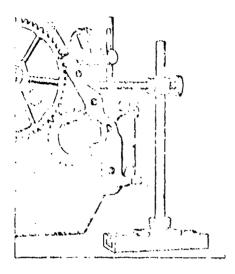
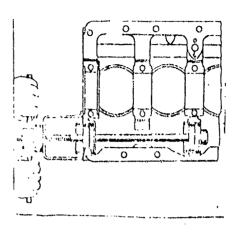


Plate 3-88. Measuring axial camshaft clearance with an indicator



Piate 3-89. Pressing out and press fitting camshaft bushings

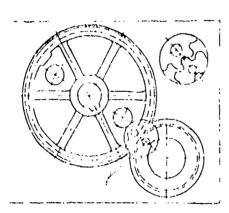


Plate 3-90. Position of marks on gears during installation of gas distribution system



Plate 3-91. Checking clearance between camshaft gear teeth

Installation of the clutch housing cover and disengagement fork. Install the clutch disengagement fork in the housing and fasten the bushing flange with bolts. Install the clutch housing cover and housing plate and fasten them with bolts.

Installation of valves and tappet sections. Rotate the engine on the stand, setting the cylinders upward. Blow out the valve chamber space with compressed air.

Tightness of valves is renewed by lapping the working faces of the valves against their seats. If there are pits or marks on the working face of the valve which are impossible to eliminate by lapping, the face is subjected to grinding, with consequent lapping against the seat. Rotation of the valve during the process of manual lapping is accomplished with a drill which rotates the valve across its section, first to the right and then to the left.

If the valve has a slot in its head, it is held by mandrel using this slot, and if there is no slot, it is held by a rubber suction cup.

During lapping, it is recommended that a slightly elastic spring be installed beneath the valve. Lapping paste or light abrasive powder mixed with engine oil is used to accelerate lapping.

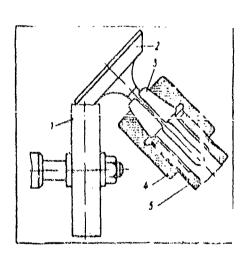


Plate 3-92. Grinding a valve face:

- 1) grinding wheel 2) valve
- 3) jaw chuck 4) nut 5) body

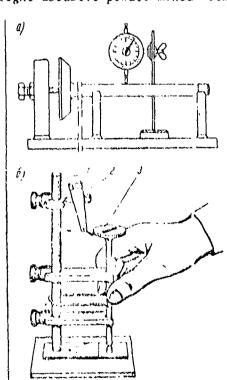


Plate 3-93. Checking a valve:

- a) checking stem straightness
- b) checking working face 1) device upright 2) indicator 3) valve

In a case where the working surface of the valve is worked out (worn), it undergoes grinding. Valve working faces may be ground on a circular grinding machine or on a model 2178 table grinder with the valve fastened in a jaw chuck (Plate 3-92). Construction of the machine allows installation of the valve at the required angle relative to the grinding wheel. The face of an intake valve is ground at an angle of 30°, and that of an exhaust valve is ground at an angle of 45°. The grinding machine also allows the valve stem face to be ground if it is worn.

The working face of a valve may be ground if the height of the cylindrical belt on the valve head exceeds 0.3 mm. Valves whose belt is less than 0.3 mm in height are replaced.

The valve stem must be straight. Straightness is checked with an indicator on jigs (Plate 3-93, a). Valve stem curvature must not exceed 0.015 mm on 100 millimeters of length. Clearence between the valve stem and guide bushing must be within the limits of 0.02-0.08 mm. Working surface oscillation in a valve relative to the axis of its stem is checked on a device Plate 3-93, b). The amount of oscillation must not exceed 0.03 mm. Valve st wear along the diameter must not exceed 0.05 mm. If the wear present is greater than that indicated, the valve is

Testing valves for tighthess may take place with a model NIIAT instrument. For this, the instrument is tightly set on top of the lapped-in valve, as shown in Plate 3-94, and air is forced into the space in the cylinder with a squeeze bulb. In this, if the mir pressure of 0.7 kg/cm² does not fall in the course of half a minute, the valve is well lapped in.

Valve seating tightness may also be checked by sending air under the valve through the exhaust or intake passage of the cylinder block (Plate 3-95) and through a tube with a rubber washer which is tightly pressed against the passage. To determine the location of air leakage, kerosene or liquid oil is poured on the valve. The location of air leakage is revealed by the appearance of bubbles.

After lapping and checking valve tightness, the cylinder block and valves should be carefully washed and blown off with compre seu air.

The maximum allowable increase in valve guide diameter due to the effect of wear is 0.08 mm, and with a greater increase in guide diameter, it should be exchanged. The valve guides must be pressed out with a device (Plate 3-96,a).

The guide is pressed into the cylinder block with an interference of 0.013-0.075 mm with a mandrel 7 (Plate 3-96. " After pressing the guide into the block, its dimension should be brought to significations by resping (Plate 3-96. c).

If the valve guides are changed in the engine, this operation should be performed before the valve seats are corrected by milling.



Plate 3-94. Method of checking valve tightness with NIIAT instrument

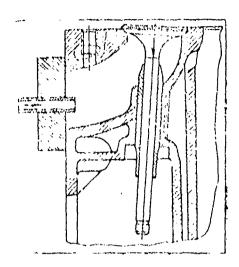


Plate 3-95. Checking valve tightness by sending air under the valve

The valve scats are formed in the cylinder block. Wear on the seat face leads to improper valve scating, which causes penetrating gases to form pits on the working surface of the valve scat. Small pits in the seat may be climinated by lapping, and deeper ones by milling or grinding with consequent lapping of the valve to the working face of the seat. For an intake valve seat, a cutter (miller) whose teeth are positioned at an angle of 30° is used, and for exhaust seats, this angle is 45°.

Width of the working face of the valve seats must be 2.5-3.0 mm. With r width of seat working face greater than 3.0 mm, it is necessary to decrease the face by milling the seat at angles of 75° and 15° to the axis of the valve guide.

Valve seat faces are repaired in the following order: machine the working surface of the valve seat with a millor at an angle of 45°, as shown in Plate 3-97, a, and b, and remove the face at the lottom part of the valve seat with a millor at an angle of 75° (Plate 3-97, c); remove the face of the upper part of the seat with a millor at an angle of 15° (Plate 3-97, d) and grind the working surface of the valve seat with a grindstone (Plate 3-97, e). These same operations are performed for a seat with a 30° seat face.

A working surface of the seat is ground using an electric drill with a special mandrel (Plate 3-98, a), and the guide rod 1 is selected according to the diameter of the valve guide. Before grinding the valve sert, the stone on the grinding device should be trued with a diamond (Plate 3-98, b).

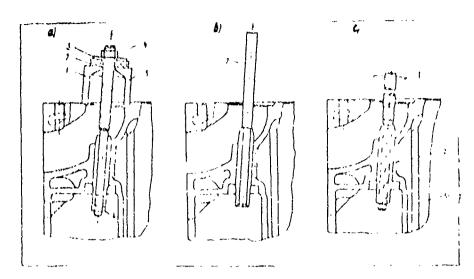


Plate 3-96. Changing valve guides: a) pressing guide out b) pressing guide in c) reaming guide 1) puller body 2) support ball bearing 3) washer 4) nut (drawing) 5) puller shaft 6) nut (backing) 7) mandrel 8) handle 9) counter bore reaming 10) cylinder block

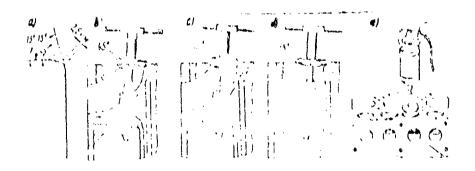


Plate 3-97. Valve seat correction: a) machining singles and dimensions of valve seat b) machining seat at 45° angle c) removing seat face at 75° ingle d) removing seat face at 15° angle e) grinding working face of seat with abrasive stone

After grinding the valve seat, it is necessary to check the accuracy of its machining with a device (Plate 3-99). Oscillation of the working surface of the valve seat relative to the axis of the valve guide hole is not allowed

to be greater than 0.03 mm.

The tappet. Wear on the spherical surface of he tappet place must not exceed 0.10 mm. Wear on the tappet shaft diameter must not exceed 0.04 mm. Worn out tappets and tappet guide sections must be replaced or repaired.

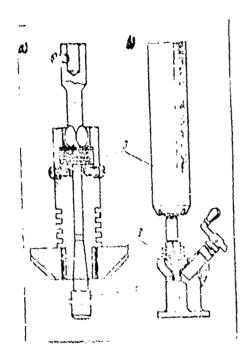




Plate 3-99. Checking valve seat oscillation

Plate 3-98. Universal device for grinding valve seats: a) device for grinding b) device for truing grindstene 1) guide rod 2 grind stone 3) device

Worn out tappet guide holes may be requilt to repair dimensions.

Tappets which are correctly selected according to the dimensions of the guide holes and lubricated with oil must freely fall through the guide holes under their own weight.

indiricate the valve stems with engine oil and install the valves in the cylinder block receptacle. Next, mount the spring and plate on the valve stem (see Plate 3-34, e), and then, compressing the spring with device 20P-7992

(see Plate 3-44, d), install the keys and remove the device.

Install the rear tappet section in assembly with the tappets, for which the crankshaft must be turned to a position in which the fifth lobe of the camshaft is directed upward, and after this, rotate the crankshaft by 120° to the position in which the eighth lobe of the camshaft is directed straight upward, and then install the front tappet section. Tighten the tappet sections with bolts (see Plate 3-44, b). Torque moment is 7.0-9.0 kg meters.

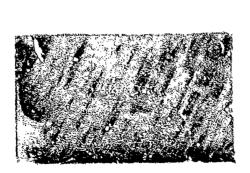
Adjust clearance in the valves. Then lubricate the cam lobes with oil, install the valve chamber covers with gaskets and fasten them with bolts (see Plate 3-44, a).

Installation of the cylinder head. Check, and if nocessary, carefully wipe the cylinders, piston heads, and cylinder head with a cloth, and then blow them out with compressed air. Lay the cylinder head gasket with its smooth side toward the block. Screw in the seven sauds at first by hand, and then tighten them with a stud tightener.

Install the cylinder head, insert the bolts, and tighten them with an angular socket wrench in two passes. Cylinder head bolt torque should be checked with a torque wrench. The torque moment for bolts and nuts must be within the limits of 10-12 kg meters. The head fastening bolts should be tightened in the order shown in Plate 3-31.

Installation of the front motor mount bracket, the crankshaft rulley, and the ratchet. Install the front motor mount bracket on the projection of the camshaft gear cover as shown in Plate 3-100, a, so that the depression in the bracket is directed toward the side of the camshaft gear cover.

Install the key in the key way in the end of the crankshaft and press the pulley on the shaft (Plate 3-100, b). Install the locking washer on the end of the shaft and screw the ratchet into the threaded hole in the crankshaft. Tighten the ratchet with a wrench and crimp the locking unaber.





Place 5 100. Installation of the front motor mount bracket and pressing the crankshaft pulley: a) bracket installation h) pulley pressing

Installation of exterior parts and assemblies on the engine. install the intake and exhaust manifolds with the gasket and fasten them with bolts (see Plate 3-42). For convenience in performance of this operation, two helping stude can be screwed into the block and the manifolds mounted on them. Later, after having fastened the manifolds with bolts, the stude are unscrewed and the final two bolts are screwed into their places. Torque moment on the manifold fastening bolts must be 4-5 kg meters.

Curvature of the intake and exhaust manifold contact surface must be less than 0.7 mm on its entire length, and no greater than 0.4 mm for a row of continuous flanges. Checking of this is done with a leaf gauge and straightedge gauge.

If the straightness of the contact plane does not fall within the assigned limits of tolerance, its correction must be conducted by milling or manual fitting with a file. The presence of small cracks on the internal part of the manifold need not serve as an indication of failure.

During repair, the walls of the manifolds should be checked and cleaned of formations of deposits on them, since a significant quantity of these deposits noticeably constricts the passage section of the manifolds, decreasing its power and economy. Cleaning is done with a metal brush and jag wire with subsequent washing in kerosene and blowing out with compressed air. After cleaning, the manifolds should be checked for tightness under pressure of 3-4 kg/cm².

Screw in the two study for fastening the fuel pump, install the fuel pump with the gasket beneath it, and tighten the nuts.

Check the cylinder block for presence of the water distributing pipe. Install the water pump with its gasket on the front part of the block and fasten it with bolts. Mount the compressor drive belt and the fan belt on the pulley, including the crantshaft pulley in them.

Install the compressor on the cylinder head and fasten it, tightening the nuts on the stude to a preliminary position. Mount the drive belt on the pulley, tighten the belt and final tighten the compressor nuts.

Install the starter and fastan it with holts.

Install the oil filler pipe in assembly with the air filter of the crank-case ventilation system and fasten the pipe with bolts. The bolts must be tightened evenly to prevent breakage of the flanges on the tube.

Install the oil filter body in assembly with its gasket on the cylinder block area for it, and fasten it with bolts.

Screw the cooling liquid temperature indicator switch to its receptacle in the cylinder head. Screw the oil pressure indicator switch into its receptacle



in the cylinder block main oil line.

Install the ignition coll on the cylinder head and fasten it with belts.

After having inserted the thermostat in the water pipe, install it with its gasket on the cylinder head and fasten it with bolts. The bolts must be tightened evenly to protect the pipe flanges from damage.

Install the generator brackets on the cylinder block and fasten them with bolts. Install the generator on the brackets and fasten it. Connect the tensioning arm, mount the generator drive belt on its pulley, and tighten the belt.

Install the heat insulation gasket on the upper flange of the intake and exhaust manifolds, install the engine revolution governor, and then install the carburetor with its gasket and fasten it with nuts. Connect the fuel line from the fuel pump to the carburetor and fasten it.

Install the engine cir filter on the carburetor and fasten it. Connect the pir separation tube to the compressor and fasten it on the filter and on the compressor.

Connect the cooling system hoses to the compressor, to the cylinder head sleeve, and to he water pump cap sleeve and fasten them. Connect the inlet and outlet oil hes for lubrication of the compressor and fasten them.

Bring the transmission up on a hydraulic jack (type 32P+1270), raise the transmission, and, having connected it to the clutch housing, fasten it with bolts, tightening them with an angular socket wrench until they refuse to torn.

Installation of the distributor. Since not only the distributor was removed from the engine but also the intermediate shaft for its drive, it is necessary to install the drive shaft before installing the ignition. For this, the piston in the first cylinder must be set at TDC on its compression stroke, according to the mark on the flywheel or according to the setting rod on the camshait gear cover.

Install the intermediate distributor drive shaft with the body as an assembly in the cylinder block receptable and rotate the shaft so that the slot in its sleeve, which is displaced by 0.5 mm relative to the shaft axis, is directed toward the side of the cylinder block. Then, turning the shaft slightly in a counter-clockwise direction, drop it with the body into the receptable in the block so that the drive gear teeth are engaged with the gear on the camshaft. The intermediate drive shaft of the distributor must rotate and sit in a position so that the slot in its sleeve is parallel to the camshaft axis with the slot displaced toward the cylinder block, after which the stop bolt is tightened and clenched on the engine.



Install the plates of the manual timing adjuster on the cylinder block space for them, and fasten them with bolts. Loosen the upper plate tension bolt of the octane corrector and install the distributor on the engine, having previously turned the shaft so that the projection on the distributor connecting sleeve, having a displacement of 0.5 mm relative to the axis of the shaft, is directed to the side of the vacuum regulator, which must be directed upward toward the ignition coil. In this, the rotor electrode must be located apposite the terminal of the first cylinder on the cap. After this, tighten the distributor fastening tension bolt on the cylinder block. Install the high tension wires and connect them with the spark plugs.

For checking ignition timing, it is necessary to install the wires in place, fuston them on their corresponding terminals of the equipment, and connect the wire of the primary circuit to an auxiliary battery.

Rotating the adjusting nut, co-locate the indicating arrow of the upper plate of the octane corrector with the zero mark on the lewer plate. Turn on the ignition and rotate the distributor body counter-clockwise with the adjusting nuts until the appearance of a spark between the end of the middle wire from the ignition coil and ground (by a distance of 2-3 mm). Initial contact point breaking may be checked with a timing light connected to the engine ground and to the low tension termina; of the distributor. Tighten the adjusting nuts of the octane corrector in this position. Then, check for the correct installation of wires in the distributor cap, corresponding with the ignition firing order (1-5-3-6-2-4).

Running the engine in

To increase the service period of an engine, it is run in after assembly. The ongine running-in process allows checking of the quality of repair work performed, presence of local over-runs, extraneous noises or knocks, and leaks or lack of tightness. It also allows fine adjustment of clearance between valves and tappets on a werm engine, setting of ignition timing, adjustment of the carbureter for engine idle, as well as checking the level of fuel in the carbureter float chamber, and pressure and temperature in the engine lubricating and cooling systems.

After a short running-in period, a short-time load can be applied to the engine with a partially closed throttle, and one or two power control points can be taken during its operation. After overhaul, the engine should be run in according to the schedule shown in Table 3-2.

The engine in considered unable if it can be started with a starter or with a handcreek, works at any speed without missing, runs smoothly at idle (400-600 rpm), goes not leak oil, water, or fuel, and does not have extranogus noises and brocks. Oil pressure at 1000 rpm must be no less than 2.5 kg/cm². If a defect is uncovered in an engine during the process of its running in, the respon the parts are exchanged and the engine undergoes a second running

in, using either the full schedule or a partial one

kunning in and testing of engines takes place on stands. Hydraulic brakes, electrodynamometers on direct current or specially equipped normal desynchronous alternating current motors can be used to lead the engine. Plate 3-101 presents an engine stand equipped with an alternating current electric motor.

Installation of the power unit in the truck

Install the power unit on the special carriage and bring it to the truck, disconnect the hand brake drive lever, remove the cover and lever from the transmission, and cover the transmission with a piece of cardboard which has been specially prepared for it. Fasten the mechanism book to the engine hanger and set the engine on the truck frame, simultaneously placing the top suspension cushions beneath the front motor mount. Install the front suspension bolts with the bottom cushions and fasten the front engine suspension. Install the bolts on the rear engine suspension and fasten them. Install the transmission cover and fasten it with bolts. Connect the exhaust pipe with its gasket and fasten it to the flange of the exhaust manifold with bolts. Install the handbrake drive lever, fasten it and connect it with the brake. Connect the clutch disengagement mechanism and install the pedal return spring. Connect the propollor shafts and fasten them with bolts. Connect and fasten the speedometer cable.

Connect the transfer case drive and fasten it. If the truck has a winch, it is necessary to install and fasten its drive.

Install and arten the inspection plate in the cab floor with bolts. Connect and tights he ompressor line and fuel line. Install the throttle control bracket and fasten it. Fasten the throttle control pedal vod to the bracket and fasten it. Install and connect the rod with the throttle jever and with the throttle control bracket, and install the carburetor leakage return spring. Fasten the manual choke and throttle cables to their brackets and fasten them with screws.

Install the radiator in assembly with its jacket on the frame with rubber cushions and fasten it. Connect the drawbar to the louvre lever, and pin and fasten the drawbar bracket of the dashboard. Install the bottom radiator pipe with a gasket and fasten it with bolts. Then connect the hose with the water pump and the hose with the cylinder head pipe, and fasten the champs with screws. Install the hood spacing rod and preliminarily fasten it.

Connect the wires for the generator, starter, ignition coll, distributor, and sending switches for the indicators of cooling liquid temperature and oil pressure and fasten them on their poles. Fasten the multiwire conductors on poles of the connecting blocks, connect the "ground" crosspiece and fasten it

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Table 3-2. Schedule of engine running-in

Key: a) running-in

b) load, hp

el number of crankshaft revolutions, i pa

d) run-in time, minutes

1) cold

2) samo

3) her, without load

4) same

i) hot, under load

eque (d

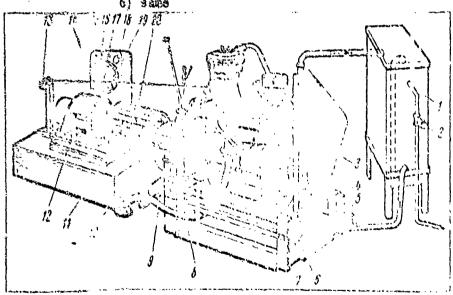


Plate 3-101. Stand for running in and testing enging:
1) tank with water 2) valve shutting off water from water line 3) protective grating 4) and 10) nuts fastening engine on stand 5) water shutoff valve 6) engine 7) stand frame 8) fuel shutoff valve 9) exhaust gas collector pipe 11) universal drive 12) electric motor 13) throttle control drive 14) electric motor control buttons 15) manometer for oil pressure in engine lubrication system 16) water thermometer 17) oil thermometer 18; tachometer for number of engine crankshaft revolutions 19) dual for weights 20) protective grating

to the cylinder head with a bo't, and fasten the "ground" wire and starter wire to the poles of the storage battery and tighten them.

Install the engine hood and fasten the hood bar.

Dimensions of parts

Engine cylinders are measured in two directions which are perpendicular to each other, along the axis of the crankshaft and perpendicular to it, and also in two belts at distances of 10-15 and 65-70 mm from the upper plane of the cylinder block.

Maximum allowable cylinder wear should be considered to be 0.4 mm. Planar irregularities on the surface of the block where it is assembled with the cylinder head are not allowed to be greater than 0.2 mm on the entire length of the block, and no greater than 0.05 mm on the length of 50 mm, along the surface lying against the oil pan, no greater than 0.2 mm on the entire length, and no greater than 0.05 mm on the length of 50 mm; on the surface lying against the intake and the exhaust manifolds, no greater than 0.4 mm. If planar irregularities in the surfaces noted above exceed those allowable, it is necessary to true these surfaces by scraping or fine milling.

Before the cylinders go in for repair, it is necessary to determine the degree of wear on their valls. Wall wear is measured by an indicating plug gauge of dimensic 100-150 mm, set at the nominal cylinder diameter. To maintain stable pasurements, it is desirable that all measurements be taken at a constant temperature of the surrounding medium of 10-30°C.

Cylinders are overhauled by boring and subsequent honing. It is recommended that the fortable machine mod 1 2407 be used for boring cylinders. The cylinders should be bored leaving a margin of 0.02-0.08 mm for honing. Honing is accomplished with ab asive blocks or drilling machines or on model 2291 finishing machines.

During boring, deviation of the perpendicularity between the cylinder axis and the crankshaft sxis must not exceed 0.05 mm on a length of 100 mm. The nominal and repair dimensions of cylinders are given in Table 3-3. Dimension groups are given for individual colection of pistons.

All cylinders of a single block are repaired to a single repair dimension. The maximum conicity and evality of an everhauled cylinder is not allowed to be greater than 0.025 mm. Some cylinders, whose diameters for some reason full outside the limits of the maximum dimension 103 or 120 mm, may be repaired by the method of sleeving. The number of sleeves in a single block may not exceed three. Sleeves are manufactured of the cast iron used in cylinder blocks.

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i ionnumental	191 2 4	101,55	101,38 101,58	101,60	101,60
9 la penourant	0.8	103,00	107,06	102,00	102,10
hase .	1.0	102,62	102,50	102,60	102,60 102,63
34,	1,5	103,00	102'00	103,08	103,12
	! .} '.4")	1 ? f	,	٠,

Table 3-3. Nominal and repair dimensions for cylinders, mm

Key: a) dimension

- b) cylinder diameter increase
- c) cylinder dimensions
- d) nominal and repair
- e) groups
 f) nominal
- g) first overhaul
- h) second overhaul
- i) third overhaul

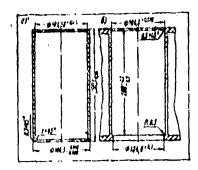


Plate 3-102. Dimensions a) sleeve b) sleeve cavity

Dimensions of the sleeve and sleeve cavity in the cylinder block are presonted in Plate 3-102. For pressing the sleeve into the cylinder block, hot

water should be poured into the water jacket, and the sleeve should be cooled as much as possible and lubricated with oil. Sleeves are pressed in by a press with an interference of 0,05-0.10 mm. The face of the pressed-in sleeve must be flush with the upper plane of the cylinder block.

The clutch housing. On the clutch housing assembly surfaces with the cylinder block and with the transmission, planar irregularity is not allowed to be greater than 0.4 mm, and non-parallelness of these planes relative to except other is not allowed to be greater than 0.35 mm.

Height of the housing support lugs must be within the limits of 76.25-69.75 mm. Wear of the support lugs along height is allowed to 64 mm. The diameter of the holes for the rear motor mount bolts must be within the limits of 19.75-21.0 mm. If the holes are greatly worn, it is permissible to ream them and install bushings. The internal diameter of the bushing for the clutch disengagement fork shaft must be within the limits of 25.06-25.17 mm.

Holos for the clutch disengagement fork shaft may be reamed to the overall dimensions shown in Table 3-4.

In reaming the holes, bushings are pressed in with an interference of no greater than 0.10 mm. After pressing, both bushings are bored simultaneously to ensure their coaxiality. Nonalignment of the bushings is allowed to be no greater than 0.025 mm and nonparallelness relative to the surface lying against the cylinder block is allowed to be no greater than 0.1 mm on a length of 100 mm.

The clutch housing is centered on the cylinder block with two installation rings. When the clutch housing is exchanged, it is installed on the rings, which are pressed in the face of the cylinder block, and it is fastened with bolts. The balt torque moment must be equal to 8-10 kg meters. After tightening, alignment of the holes centering the transmission with the axis of the crankshaft should be checked, along with the perpendicularity of the rear face of the housing relative to the axle of the crankshaft.

This checking is performed with device IV-2376, fastened on the crankshaft flange (Plate 3-103). The amount of oscillation of the internal surface of the hole and the face of the clutch housing relative to the axis of the crankshaft must not exceed 0.2 mm.

The cylinder head. Planar irregularity of the cylinder head must not exceed 0.3 mm on its entire length or 0.1 mm on a length of 100 mm. If curvature is present which exceeds the mentioned amounts, the cylinder head surface must be milled or scraped, keeping in mind that the volume of the combustion chamber may not be decreased by more than 2 cm³. Control of the assembly surface of the cylinder head is done with a set of gauges on a control plate or with a straightouge gauge.

Testing the cylinder head for tightness should be done with water or emulsion at a pressure of 3-4 kg/cm^2 over the course of three minutes.





Plate 3-103. Checking alignment and perpendicularity of the clutch housing relative to the crankshaft axis:

a) device installation b) checking alignment and perpendicularity with two indicators simultaneously 1) cylinder block 2) crankshaft flange 3) wing nut fastening the device to the crankshaft flange 4) device shaft 5) clutch housing 6) indicator for checking flanged clutch housing hole 7) indicator for checking plane lying against transmission

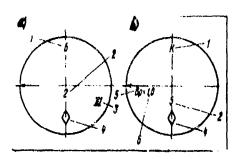


Plate 3-104. Piston marking: a) nominal dimension b) overhaul dimension 1) dimensional group according to skirt diameter 2) dimensional group according to weight 3) dimensional group according to wrist pin hole diameter 4) location of DTC stamp 5) designation of piston overhaul group 6) overhaul dimension of piston

Pistons. Marking of a piston of nominal dimensions is shown in Plate 3-104, a, and that of a piston of overhaul dimensions is shown in Plate 3-104, b, Repair and nominal piston dimensions are presented in Table 3-5. To previde individue! selection of pistons according to cylinders, each of the presented dimensions is divided into dimensional groups, in which the pistons follow every other 0.02 mm increment, according to skirt diameter.

Q. Размер	В Перапначальный	C Longration Bes private
d Номинальний	30,000 - 30,045 30,250 - 30,295	30,07 30,32

Table 3-4. Dimensions of holes for fork shaft bushings, mm

- Key: a) dimension
 - b) initial
 - c) allowable without repair
 - d) nominal
 - e) first repair

<u> </u>			C. Passe	С. Размеры юбки (в плоскости оси пальца)							
0 -	•). Упеличение	d	e	e rpynnu						
а. Резнер		THEMETPE	н минадьный н ти ремонтный	ı	11	111					
1.оминальный			101,48	101,48	101,50	101,52 101,54					
1 й ремонтный	·	0,5	101,98	102.00	102,00	102,02					
26 >		1,0	102,48	$\frac{102,48}{102,50}$	$\frac{102,50}{102,52}$	102,5					
i s.a »		1,5	103,98 104,04	$\frac{102,98}{103,00}$	103,00	103,04					

Table 3-5. Dimensions of pistons, mm

Key: a) dimension b) cylinder diameter increase c) skirt dimension (in wrist pin axis plane) d) nominal and repair e) groups f) nominal g) first overhaul h) second overhaul i) third overhaul

	<u> </u>	Обозначен	ие группы	·
u. Pasuep	ŧ	u	10	IV
• Номинальный (27,985)	27,9925	27,9900	27,9873	27,9830
(27,995)	27,9950 Голубой	27,0935 Красный	27,9900 Beauth	27,9875 Черный
• 1-й ремоняный (+0,12) • 2-й » (+0,20)	r.	28,103- 28,183-	-28,115 h. -28,195	· i.
92				

Table 3-6. Dimensions of piston wrist pin hole,mm

Key: a) dimonsion

b) group designation

c) nominal

d) first repair
e) second repair

f) blue

g) red h) white i) black

a.	b.	U PENCOOU	на значетр	d.	-		
Размер	Увсянченне Анам тра		31	!11	IV	Обозначены ремонтилго резмире	
с. Номинальный 28 ^{-0 01}		27,9973 28,0000	27,0050 27,0075	27.9925 27,9950	27,9900	_	t
f. I-й ремонтный	0,12	$\frac{28,1173}{28,1200}$	28,1150 28,1173	28,1125 28,1130	28,1100 28,1125	БР или АРГ	1.
g - 2-A	0,20	28,1973	28,1950 23,1975	28,1925 28,1930	28,1900 28,1925	БР вая АР2	m.
		l'oay toff	Красный	Белий	Черный к.		

Table 3-7. Piston wrist pin dimensions, mm

Key:	a) dimension	e) nominal	j) white
	b) diameter increase	f) first repair	k) black
	c) designation of wrist pin	g) second repair	1) BR or ARI
	diameter according to group	h) blue	m) BR or AR2
	d) designation of repair dimension	on i) red	

With perpendicular measurements, ovality in a new piston skirt is allowed to be no greater than 0.15 mm, and piston skirt conicity must be within the limits of 0.04-0.06 mm.

Piston weight must be within the limits of:
For a piston of nominal dimensions, 782-822 grams;
For a piston of +C.5 overhaul dimensions, 782-836 grams;
For a piston of +1.0 n overhaul dimensions, 790-846 grams;
For a piston of +1.5 mm overhaul dimensions, 814-554 grams.

In a set of pistons for one engine, variations in piston weights are allowed to be no greater than 8 grams. Fitting the pistons by weight is done through boring the internal diameter of the piston skirt belt.

To facilitate individual selection of piston wrist pins, the pistons are broken down into four various groups, according to the diameter of their wrist pin holes, in correspondence with Table 3-6. Marking of the different groups according to nominal wrist pin hole diameter is done by either marking komen numerals on the piston head (see Plate 3-104) or with paint on the face of the wrist pin hole. Ovality and conicity of the piston wrist pin hole is not allowed to be greater than 0.0025 mm.

Piston wrist pins and rings. Nominal and repair dimensions of piston wrist pins are presented in Table 3-7. The wrist pin is fitted into the piston hole with an interference of 0.0025-0.0075 mm.

The piston wrist pin stop rings must sit in their grooves in the piston with some interference, and must not be able to be rotated by hand. Rings which have lost their elasticity are replaced.

Nominal and repair dimensions of the compression and oil rings are presented in Table 3-8.

Connecting rods which go into repair with deficiencies in the correct cylindrical form of their holes by more than 0.01 mm or which do not fall in the limits of the directed dimension are discarded.

The diameter of the connecting rod big end hole with the nuts torqued must be within the limits of 65.500-65.518 mm (see Plate 3-9). Repair of a connecting red small end usually includes machining the old bushing for a repair dimension piston wrist pin (when the piston is capped) or exchanging the small end bushing with its subsequent machining for a wrist pin of nominal dimensions (when the piston is exchanged).

During repair of the connecting rod small end hole, the dimensions for the bushing and for the wrist pin in the bushing must correspond to the dimensions shown in Table 3-9.

The wrist pin bushing is pressed into the hole with an interference of 0.147-0.220 mm.

While pressing in the bushing, and also while boring it, it is necessary to ensure that a clearance of 2-3 mm is maintained I tween the internal faces of the bushing pressed into the connecting rod small end which must provide normal access of lubrication to the piston wrist pin.

For a better fit in bushings which are newly pressed into the connecting rod small ends, and also to compact the surface layer of metal in the bushings, they should be drawn with a smooth broach, and the broach diameter should be 0.5-9.5 mm smaller than the final diameter of the hole for the wrist pin. After drawing with a broach, the bushing is fitted by drilling to the nominal or repair dimension diameter of the piston wrist pin shown in Table 3-7.

For selection of piston wrist pin-connecting red combinations, the holes in the connecting red small end (along the bushing) are divided into dimensional groups through each 0.0025 mm. Non-cylindricality of the bushing hole is not allowed to be greater than 0.0025 mm.

The final-machined hole for a piston wrist pin of any dimension (standard or repair) has to be such that, with a temperature of +20°C, the piston wrist pin smoothly moves into the bushing hole under the pressure of a man's thumb. Height clearance between the piston wrist pin and the bing hole within the limits of 0.0045-0.0095 mm corresponds to this fit.

The crankshaft. The nominal dimension of a crankshaft main bearing journal is 65.97-66.00 mm, and that of a connecting rod bearing journal is 61.975-62.00 mm. The shaft journals are measured with a micrometer, 50-75 mm in size. The shaft journal should be measured on no less than 2 planes which are perpendicular to each other.

Ovality or conicity in the journals of a new shaft, or a shaft which has undergone regrinding, must not exceed 0.01 mm. Surface smoothness of the main and connecting rod journals is assured by grinding and subsequent polishing.

Loagth of crankshaft journals in mm is:

Connecting	rod							,				,					9		OU	-	3	8	. 10	3
Main:																								
First		٠				,										4	3		55	<u>,</u> -	4	3.	6	ţ
Second				,												1	8		00	۔ (3	8	34	1
Third																			06					
Fourth		,			,										٠	7	Ü		00	۱-	7	O.	. 4()
F1 fth											,			٠	٠	,	8	4	00	٠.	3	3	. 34	į
Sixth										,						3	R	,	00) _	3	8	. 34	\$
Seventh	:																		5 0					

The radii of the connecting rod and main journal fillets are 1.0-3.0 mm. The axes of the connecting rod journals must be parallel to the axes of the main journals. Nenparallelress must not exceed 0.02 mm on the length of each

connecting rod journal. Shaft journal wear (non-cylindricality) for connecting rods over 0.05 mm, and for mains over 0.07 mm, requires their regrinding to repair dimensions.

Repair dimensions of crankshaft journals are presented in Table 3-10.

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Housesautes 1-a penograma 37 8-2	* * *	0.0	101.6 103.1 103.1

Table 3-8. Piston ring dimensions, mm

- Key: a) dimension
 - b) increase
 - c) exterior ring diameter
 - d) nominal
 - e) first reprir
 - f) second repair
 - g) third repair

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۵	ball in the	beauton.		E presented	9 061644	11	111	tV.					
	79,500 79,503	79,600 29,600	79,670	29,820	(20) The (20) The (20)	28,004 28,006 CR. 000	20174 24 (013) 24 (044)	27 0070 27 0070 Hepmin					

Table 3-9. Dimensions of the connecting rod small end and bushing, men

- Key: a) connecting rod small and hole for bushing
 - b) nominal
 - c) repair
 - d) bushing dimensions for wrist pin
- e) exterior diameter
- f) interior nominal dismeter of bushing
- g) designation of bushing diameter according to groups

The small gear of the camshaft drive is pressed onto the crankshaft. Journal diameter beneath the gear is 49.980-50.034 mm. The interior diameter of the gear hole is 50.000-50.027 mm. Oscillation of the journal beneath the gear must not exceed 0.04 mm. Face oscillation of the small gear must be no greater than 0.025 mm, measured at the side directed toward the face of the main bearing. The diameter of the journal under the fan drive pulley is 45.950-45.975 mm. Width of the keyway is 5.945-5.990 mm. Repair of the key way by milling is allowed to a repair dimension of 6.445-6.490 mm. Face oscillation of the shaft flange on which the flywheel is mounted must not exceed 0.06 mm. Flange width is 8.14-8.50 mm. Diameter of the holes for flywheel fastening is 14.00-14.035 mm.

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	ed agent weeks x c	Bojecus waryns
f omariand		60,07 61,07
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,	0.6	65, 87, 61, 375
1	1 , ,	64,97 (0.3) 65,00 (1.603
J	1 4	64, 0 (0, 12
K	2.0	61,00 (0,000

Table 3-10. Repair dimensions for main and connecting rod journals of crankshaft,

Key: a' dimension

- b) diameter decrease
- c) crankshaft journal dimensions
- d) main
- e) connecting rod
- f) nominal
- g) first repair
- a) second repair
- i) third repair
- j) fourth repair
- k) fifth repair

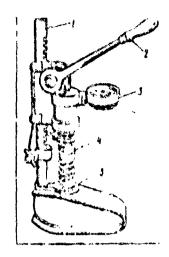


Plate 3-105. Model NITAT device for checking valve springs:

- 1) device stand 2) lever 3) manemater
- 4) spring being checked 5) lower base

Inserts. Nominal and repair insert dimensions are presented in Table 3-11. Marking of the repair dimension inserts (0.3, 0.6, 1.00, 1.50, 2.00) is piaced on the steel surface of the insert near its butt joint. Nominal dimension inserts do not have markings.

The calculate. Diameters of support journals and the amount of their wear allowable without being repaired are presented in Table 3-12.

In grinding the support journals of the shaft to the third and fourth repair dimensions, the oil pump drive gear must be ground along its diameter to the same dimension. Surface smoothness of the lobes and shaft journals is provided by grinding. Oscillation of the front face of the first journal of the shaft is not allowed to be greater than 0.03 mm. After regrinding the journals, it is recommended that shaft straightness be rechecked.

Camphaft lobe profile is identical for intake and exhaust valves. The height of valve lift is 13.1 mm (see Plate 3-10, s). Lobe wear sust not exceed 1.2 mm in height. Lobe wear is measured with an indicator according to the difference between the maximum and minimum diameters of the lobe.

Wear on the fuel pump drive eccentric is allowed to a dimension of 41.0 mm. The nominal dimension of the eccentric is 41.65-42.80 mm (Plate 3-10, b). A caushaft on which the lobes or eccentric are worn greater than the allowance is replaced.

Camshaft bearings are bored in the relinder block parallel to the crank-shaft bearings. The distance between the axes of these bearings is 133.35-153.40 mm, and the hole diameter in the block for the camshaft bearings is equal to 60.00-60.03 mm.

Camshaft bearing inserts are thin-walled, stamped from bimetallic tape, and pressed into their receptacles with an interference of 0.045-0.135 mm. Data on the camshaft bushings is presented in Table 3-15. The allowable misalignment of pressed in buthings must not exceed 0.06 mm. Allowable camshaft bushing wear is no greater than 0.05 mm. Camshaft goar dimensions are presented in Place 5-12, b.

Valve guide incarts. Valve guides, manufactured of type CCh 15-32 (GOST 1412-54) are pressed into the block.

Diameter of the holes in the cylinder block for valve guides is 17.000-17.027 mm. The exterior diameter of the valve guide is 17.040-17.075 mm. Directions of the internal holes of the bushings, in mm, are the following:

Nominal dimension, 9.500-9.530 Repair dimension, 9.250-9.280

Valve springs are formed of wire, 3.75 mm in diameter. There are a total of eleven coils, of which 8.5 are working ones. The internal diameter of a coil is 24.00-24.52 mm. Spring height in a free condition must be within the limits of 90-93 mm, and under load of 21.5-23.75 kg, it must be 70 mm. After freeing the spring from the load, it must not have residual deformation. Springs which do not respond to these requirements are exchanged. Height and elasticity of springs are checked on a device (Plate 3-105). The amount of load on the spring is determined according to the manometer 3.

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Name .	Tonnings erosewood offeres	Echique : Hemanic Hemanic	Gorgen. Heritana Heritana	T ABSTRACT TRACTICAL TRACTICAL ADMITSE	ante mand for anya france	Entrates (substants)
(-1/20) Personana (-1/20) Personana (-1/20) Personana (-1/20) Personana	2,76	2,250 9,237 9,640 5,357 2,750 9,757 1,966 1,967	64,023 64,023 63,786 63,696 63,696 64,026 64,026	1.80	1,730 1,737 1,860 1,030 2,030 2,230 8,237 2,467	61.041 61.041 61.041 61.041 61.041 61.041 61.041
0 M poliostana	A. 011	3,230	64,020 64,035	2,45	9,150	60,041

Table 3-11. Dimensions of main and connecting rod inserts, mm

Key: a) dimension b) main bearings c) connecting rod bearings d) steel band chickness e) overall insert thickness f) diameter of bearing (insert) g) nominal 1; first repair 2) second repair 3) third repair 4) fourth repair 5) fifth repair

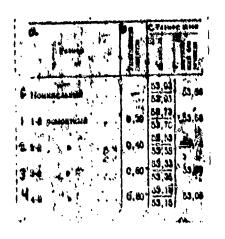


Table 3-12. Diameters of crankshaft bearing journals and their wear allowable without repair, mm

Key: a) dimension

- b) diameter decrease
- c) journal dimension
- d) before wear
- e) allowable without repair
- f) nominal
- 1) first repair
- 2) second repair
- 3) third repair
- 4) fourth repair

The valve seat. If the seat of an intake or an exhaust valve is worn by more than 1.5 mm, a substitute valve seat can be pressed in (Plate 3-105). Dimensions of the cavity in the cylinder block for the replaceable valve seat are presented in Table 3-14. Type CCh 13-36 (GOST 1412-54) iron is used for manufacturing replacement seats. The dimensions of the replacement valve seat are presented in Table 3-15. After pressing, the seat is calked in, and the working surface of its face is ground.

Valve tappets. Tappet dimensions, as well as dimensions of the internal diameter of the holes in the tappet guides, are presented in Tables 3-16 and 3-17.

The two end holes of each tappet guide section have a dimension of 0.016-0.021 mm larger than the middle holes to compensate for linear deviation.

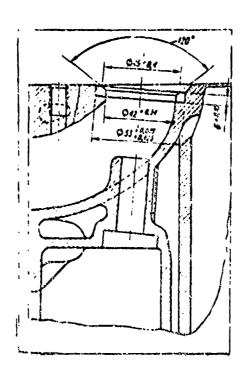


Plate 3-106. Replaceable intake valve seat, installed in cylinder block

2.	Б Визтрени	•		
Наружный шаметр	С коминальный	ремочт. Нії	inenne Ancur	
60,075 — 60,1 3 5	54,000 54,030	53,600 53,830	0,20	
		53,600	0,40	
		53,400 53,430	0,60	
		58,200 53,230	0,80	

Table 3-13. Dimensions of camshaft bushings, mm

Key: a) exterior diameter

- b) interior diameter
- c) nominal
- d) repair
- e) decreuse

NOTE: Length of front and rear journals is 32 mm. Length of middle journals is 22 mm.

6 Казнан	Juamerp Freata	С Раубика тиезта
4	53,0053,05 48,0648,05	6.10

Table 3-14. First repair dimensions of cavities in cylinder block for pressing in valve seats, mm

Key: a) valve

- b) cavity diameter
- c) cavity dopth d) intake
- e) exhaust

6. Клапан	Најужный днаметр, мм	Buchte,	MajanaB pal-nes bacos, ca	Cores, pac-]
Виускной Выпуск- ной	53,075 53,125 48,075 48,125	9 '00 2 '0 0— 9'00 2'00 -	2,5 2,5	30 54	

Table 3-15. First repair dimensions of replacement valve seats

- Key: a) vaive
 - b) exterior diameter, mm
 - c) height, mm
 - d) working face width, mm
 e) angle of working face, °

 - f) intako
 - g) exhaust

The oil pump. The diameter for the hole for the drive shaft in the oil pump body must be within the limits of 15.03-15.06 mm. If the hole diameter is increased to more than 15.12 mm, the body must be exchanged or the hole repaired.

The oil pump drive shaft diameter must be 14.998-15.00 mm. If the shaft

diameter is decreased to 14.970 mm, it should be replaced. Curvature of the shaft is not allowed to be greater than 0.03 mm. Width of the key way must be within the limits of 2.950-2.990 mm. Increase in key way width is allowed to a dimension of 3.040 mm without being repaired.

The nominal dimension of the driven gear shaft must be within the limits of 15.070-15.082 mm. With equal wear, shaft diameter decrease is allowable to 15.030 mm. One-sided shaft wear is not allowable. A worn out shaft should be pressed out and replaced with a new one. The nominal dimension of the hole in the body for the driven gear shaft must be within the limits of 15.03-15.06 mm. If the hole diameter is increased to 15.070 mm, the body is exchanged.

at house	1	Ranga Bar	79 762- 1
A public	Tanks and		hi
House salaman	رسنه (15,087	18,04
1-a paterralia	0.25	15,717 15,734	15,60
1	0,50	15,461 15,484	10.44
3 34	+0,25	10,21	18,19

Table 3-16. Valve tappet dimensions, um

Key: a) dimonsion

- b) decrease or increase in tappet diameter
- c) tappet diameter
- d) initial
- e) allowable without repair
- f) nominal
- 1) first repair
- 2) second repair
- 3) third repair

The nominal dimension of the driven gear hole (Plate 3-107) for the shaft must be within the limits of 15.100-15.127 mm. With an increase in the gear hole to a diameter over 15.170 mm, the gear should be replaced or undergo repair by means of installing a bushing.

	Paramethar and name	Agemba ebenin	us studetted '	el des verber	07 0454760
	Valentaberne und fatzusente evangerne bijapan kancana	memory server.	bergened heart and gen weakle in stand	and beyond Hobb Areyses	Posted the
Hainanind y	-0,55 -0,00 +0,20	18,000 18,619 18,750 10,760 15,650 16,819 16,350	15.62 15.67 16.67	16,016 16,040 16,750 16,750 16,750 16,840 16,860 16,260	10.84 15.89

Table 3-17. Diameter of holes in tappet guide sections, man

Key: a) dimension

- b) decrease or increase in guide hole
- c) for middle holes
- d) to end holes
- e) initial dimension
- f) allewable dimension without repair
- g) nominal
- 1) first repair
- 2) second repair
- S) third repair

The surface of the pump cover which is assembled against the gear faces must be flat. Deviation in flatness and wear are not allowed to be greater than 0.05 mm.

It is necessary to pay attention to the oil pickup hole in the pump inlet sleeve. With a large clearance between the pickup pipe and the sleeve, air leakage occurs and oil pressure decreases. If the pipe wears, it is necessary to replace it or sleeve it.

The water pump. In the water pump, the nominal dimension of the hole for the front boaring is 46.992-47.018 mm, and for the rear bearing, it is 39.980-40.007 mm. With an increase in the diameter of the front hole to more than 47.05 mm, or of the rear one to greater than 40.04 mm, the pump body must be exchanged. If necessary, the pump body may be repaired by means of drilling out the holes in the body and installing bushings with subsequent fitting of the internal diameter of the bushings to the nominal dimension. Dimensions of the water pump body are shown in Plate 3-108.

The water pump shaft has a diameter of 17.012-17.030 mm (Plate 3-109). When the shaft wears to a diameter of less than 17.00 mm, it must be replaced with a new one. Shaft curvature is allowed to be no greater than 0.03 mm. Key way width must be 3.945-3.990 mm, and with an increase in key way width to a dimension greater than 4.02 mm, the shaft must be replaced with a new ore.

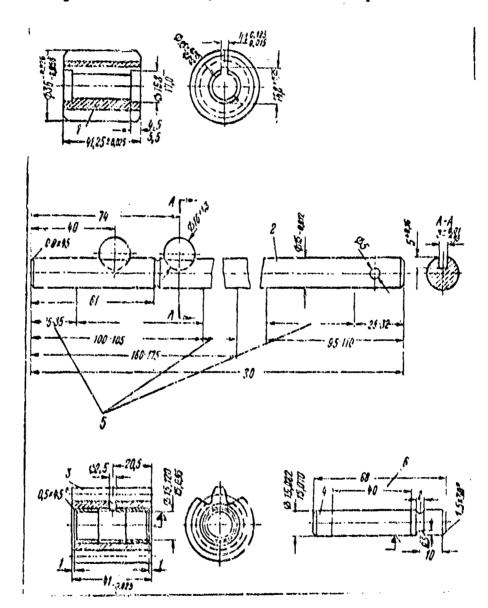


Plate 3-107. Dimensions of oil pump parts: 1) driven gear 2) drive shaft
3) drive gear 4) driven gear shaft 5) areas of shaft heating 6) area of drive
gear shaft heating

Cracks and chips on the vanes are not allowed. The diameter of the hole for the vane shaft has a dimension in the limits of 16.965-17.000 mm. The vanes are fitted on the shaft with an interference of 0.065 mm or with a clearance of 0.08 mm and subsequent fastening with a pin.

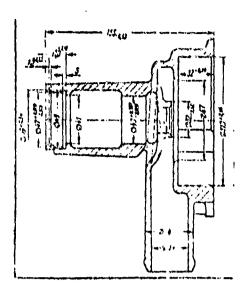


Plate 3-108. Water pump body

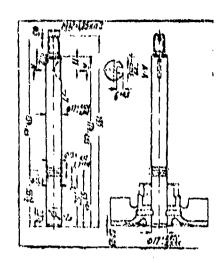


Plate 3-109. Water pump shaft with vanes and without vanes

Mothuds of renewing the cylinder block

The cylinder block is the base part and must be discarded as rarely as possible, leading to all possible methods of repair.

Renewal of threaded holes. If threads in the cylinder block are cut or worn, repair dimension threads are tapped or thread stoppers are inserted. Beaten down threads are trued with a tap. A thread stopper may be installed under the condition that the walls of the threaded hole have sufficient thickness.

The threaded hole can be renewed with thread stoppers in this way: the damaged hole is drilled out, threads are tapped in it, and the thread stopper is covered with red lead and scrowed into the hole. After installation of the thread stopper, its head is cut off and the stopper is fastered in its receptacle by punching, copper soldering, or pinning. After this, the stopper is marked, and a new hole is drilled according to the mark and new threads are tapped in it.

Cracks in the cylinder block are sealed by one of the following methods: installation of a patch; pinning; sealing with epoxy resins; or electric are welding.

In souling cracks with epoxy resins, two recipes of adhesive mastics (in parts by weight) are used:

	Recipe No.	Recipe No. 2
ED-6 epoxy rosin	100	100
Dibutylphthalate	20	20
Crushed No. 7 asbostos	е п	50-100
Steel powder	160	• •
Maloic or phthalmic anhydride	**	3 0 - 3 5
Polyethylene-polyamine or		
hexamethyldiamine	10	••

The order for preparation of the mastic is as follows: the epoxy resin is heated together with the packing in a water bath to a temperature of 60-80°C, after which the dibutylphthalate, serving as the plasticizer, goes into it. The mixture is carefully stirred and the filler is added. Steel powder serves as the filler. The mixture is again stirred, cooled to room temperature, and sealed up.

The surface which is to be scaled is cleaned of rust and dirt. The ends of the crack are drilled with a 5-3.5 mm drill, then, using a grinding wheel, the face is removed from the two sides at an angle of 90-120° to a depth equal to four-fifths of the whole thickness. The prepared surface is decreased with acctone and set out for 3-5 minutes, until the solvent is fully evaporated.

The hardener, polyethylene-polyamine (hexamethyldiamine) or maleic (phchalmic) anhydride is added to the prepared epoxy resin mixture. The mixture is carefully stirred. Upon adding the hardener, the mixture will spentaneously heat, and therefore the hardener must be added in separate portions, not allowing the mixture to heat higher than 40°C.

In this form, the mastic is usable at a temperature of 15-20°C for a period of 20 minutes, and at a zero temperature, it may be kept for eighthours. For better adherence of the mastic to the metal, the place subjected to scaling is heated to a temperature of 50-80°C.

A prepared mixture is applied with a spatula, carefully smearing it into the prepared surface. A second layer of mastic is applied on top of the crack, running over it by 10 mm on each side and 2-3 mm higher than the surface of the block.

A fiberglass patch can be applied after application of the mastic.

Forty-eight hours are required for full setting of the mastic prepared according to Recipe No. 1 at a temperature of 15-20°C. To accelerate the process, the cylinder block must be heated. Setting of the mastic prepared according to Recipe No. 2 requires heating to a temperature of 120-140°C and holding for a period of 16-24 hours.

Electric are welding of cracks is done with a copper electrode 3 mm in diameter, wrapped with tin plate or aluminum covered plate. The welding is done with direct current with reversed polarity (minus on the part, plus on the electrode). It is recommended that the power of the welding current be maintained within the limits of 120-130 amperes.

The ends of the creek are drilled with a 3-3.5 mm drill. The place of welding is cleaned of oxides, grease and dirt. The crack is excavated, sloping its odges so that the overall angle is 60-70°.

To avoid the appearance of new cracks, the cylinder block cannot be heated, and it is necessary to weld in 10-21 mm sections and allow it to cool to a temperature of 50-70°C.

A chalk coating on the electroic increases stability of the wolding arc.

While welding, the arc must be kept short, not allowing deep melting of the part metal.

Chapter 4. The V-Engine

General description

The ZIL-V-engines are 8-cylinder, carbureted, and 4-stroke, with a 2-row cylinder arrangement. The angle between the rows of cylinders is 90°. Production of the engine was first undertaken at the plant in 1964. The engine (Plates 4-1 and 4-2) is installed in the ZIL-130 and ZIL-131 trucks.

The base of a large group of easic parts of identical dimensions, such as cylinder blocks, crankshaft, its bearings, connecting rods, and gas distribution mechanism parts, made possible the creation of a series of short stroke engines capable of working in the most difficult conditions. Assembling the cylinter block with sleeves having an internal diameter of 100 mm produces an engine with a working volume of 6 liters, and assembly with sleeves having an internal diameter of 108 mm produces an engine with the working volume of 7 liters. Piston stroke in both cases is 95 mm.

The 7 liter engine carries the designation ZIL-375, and is used in trucks manufactured by the Ural motor vehicle plant.

Basic paremeters of the V-engines are:

Cylinder bore and piston str	oke, ms100 X 95
Compression ratio	6.5 : 1
Displacement, liters	6

The basic differences between the ZIL-13" (plates 4-3, 4-4), ZIL-131 (Plates 4-5, 4-6), and ZIL-131A engines are given in Appendix 1 (see Part 2). The plant number of the engine is stamped on a special surface located on the top face of the cylinder block, in the front right hand part. The number is also stamped on the plant plate, which is located on the right side of the driver's seat frame.



Plate 4-1. ZIL-130 engine

The crankshaft connecting rod and gas distribution mechanisms

The cylinder block (Plate 4-7) is cast of type CCh 18-36 iron (COST 1412-54). With the exception of the tappet guide holes, all friction surfaces in the cylinder block are changeable: the cylinder sleeves, crankshaft bearing inserts, and the camshaft support bushings. This block construction makes it practically non-wearing.

Without the sleeves in the block, the engine cooling system hollow is an open space which is easily accessible for creaning out scale.

To provide high block strength, the bottom assembly surface (cylinder block to oil pan) is dropped below the axis of the crankshaft by 65.9-66.1 mm.

The order of cylinder numbering is shown in Plate 4-8.

The cylinder block sleeves (Plate 4-9) are wet, directly wetted by the cooling liquid. The sleeves are cast of type CCh 18-36 iron (CDST 1412-54). To increase corrosion resistance in the sleeves, an insert 2 (manufactured of acid resistant alloyed iron) is pressed into its upper part.

The clutch housing (Plate 4-16) is iron. The rear engine mount feet are cast together with the clutch housing. Final drilling of the holes centering the transmission on the clutch housing takes place with the housing in assembly with the cylinder block, and therefore disassembly of the housing and the block is not recommended. The housing should be disconnected from the block only if necessary.

In the ZIL-131 engine, a plug with a hole through it and a pin inserted in it is screwed into the bottom cover of the clutch housing. This hole serves (also in the ZIL-130 housing) to drain oil which has gotten into the clutch housing.

In the operating instructions, it is projected that before fording a stream with a ZIL-131, the plug with the pin will be unscrewed from the housing cover and a spare plug without a hole will be screwed in. This spare plug is located on the bearing cover of the front axle reduction gear drive shaft.

After fording the stream, the plugs must be exchanged.

The cylinder head. Two heads (Plate 4-11), manufactured of aluminum alley, are installed on the V-engine. Each head is fastened to the cylinder block with 17 bolts.

Four bolts on each cylinder head are also used for fast ming the rocker arm shaft supports. Location of each cylinder head on the block is accomplished with two rins which are pressed into the cylinder block.

Since 1967, the cylinder heads have been manufactured with holes 12 mm in dismeter (instead of lo sm) for fastening the exhaust manifold in its middle part.

The steel-asbestos reinforced gasket is installed between the head and the cylinder block. Holes in the cylinder block for spark plugs have a thread of 14 mm and a pitch of 1.25 mm.

Intake and exhaust valves for each row of cylinders are located on each cylinder head.

The pistons are manufactured of Al. 30 sluminum alloy (GOST 2685-63) and covered with tin. An iron ring is cast into the piston head, and the groove

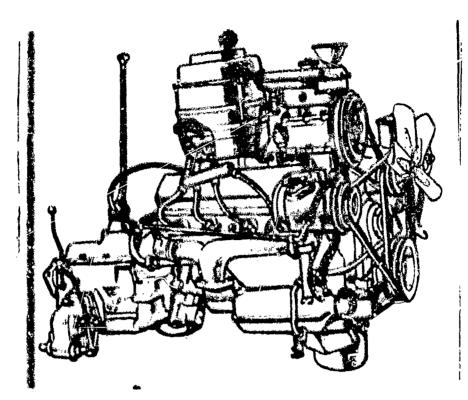


Plate 4-2. ZIL-131 engine

for the top, most atressed, compression ring is cut in this ring. 1 The piston, profile of piston grooves, and their dimensions are shown in Plate 4-12.

A piston skirt has the form of an elliptical cone whose large base is located at the bottom edge of the skirt, and the largest axis of the ellipse lies in a plane perpendicular to the axis of the piston wrist pin. For the purpose of redistributing pressure on the cylinder wall and eliminating rocking of the piston skirt near TDC, and consequently, for decreasing noisiness of the engine's operation, the axis of the piston wrist pin is displaced from the axis of the piston by an amount of 1.6 mm.

Piston wrist pins (Plazo 4-13) are manufactured of 15kh steel (WST 4543-61).

Piston rings are shown in Plate 4-14. Compression rings are cast of iron, alloyed with molybdenum (COST 846-18), of HRB 98-106 hardness. The surfaces of the two top compression rings are chromed. The oil ring is composite, consisting of two flat steel rings and two spreaders, an axial one and a radial one. The surface of the flat steel rings is chromed.

¹ Use of aluminum pistons without iron rings is permissible.

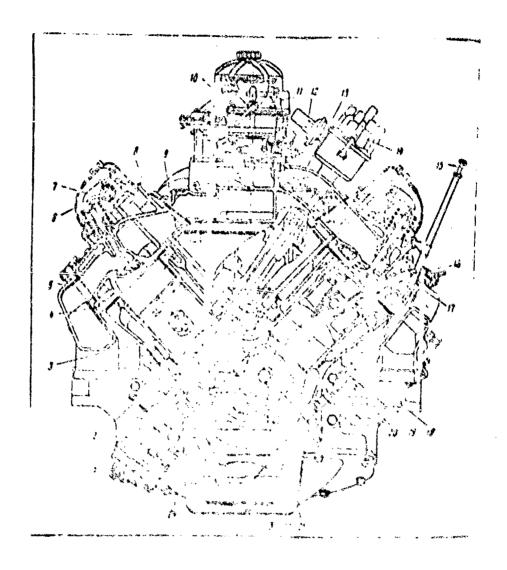


Plate 4-1. Cross section of 211-130 engine:
1) oil pump 2) cylinder block 3) piston
4) cylinder head gasket 5) exhaust manifold
6) valve cover 7) rocker arm 8) cylinder
9) tappet push rod 10) centrifugal oil
cleaning filter 11) carburetor 12) distributor
drive body 13) intake marifold 14) distributor
15) oil dipatick 16) spark plug 17) spark
plug protective plate 16) tappet 19) scarter
plate 20) starter 21) oil pan 22) oil pickup
23) cylinder sleeve 24) connecting rod

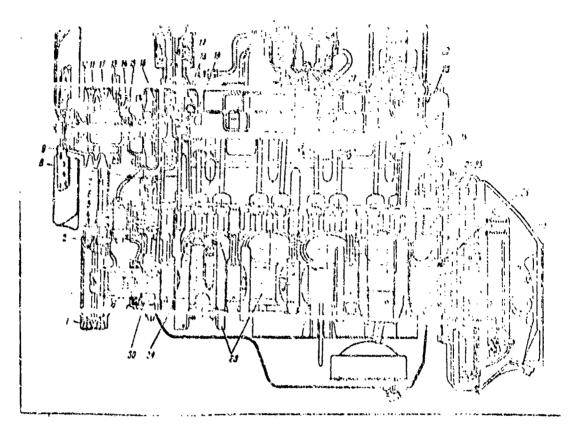


Plate 4-4. Profile section of ZIL-130 engine:

1) crankshaft pulley 2) ignition timing index 3) revolution governor switch 4) switch drive shaft 5) shaft spring 5) space ring 7) support flange 8) casshaft gear cover 9) water pump 10) water pump and fan pulley 11) generator drive belt 12) belt for hydraulic power attering pump 13) compressor drive belt 14) plug 15) lubrication fitting 16) engine lifting rings 17) crankcase ventilation filter 13) fuel pump 19) pump rod 20' fuel fine cleaning filter 21) ventilation system valve 22) centrifugal oil cleaning filter 25) oil pressure indicator switch 24) camshaft 25) insert 26) seal 27) clutch 28) crankshaft 29) support ring 30) crankshaft gear

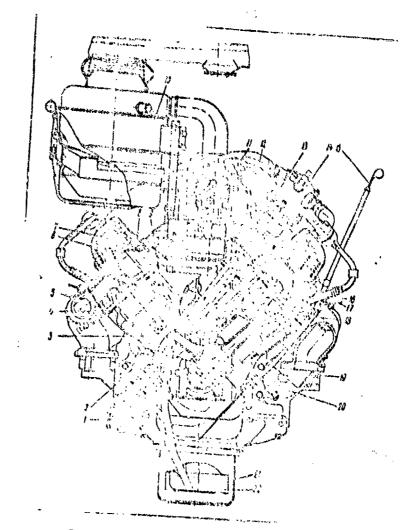


Plate 4-5. Cross section of ZIL 131 ongine:

ongine:

connecting rod 4) cylinder block 3) piston with haust manifold 6) valve cover 7) rocker arm 8) cylinder head 9) push rod 19) air filter 11) carburetor 12) distributor drive body 13) intake manifold 14) distributor 15) oil distributor 16) spark plug 17) spark plug protective plate 18) tappet 19) starter plate 20) starter 21) oil pan 22) oii pickup

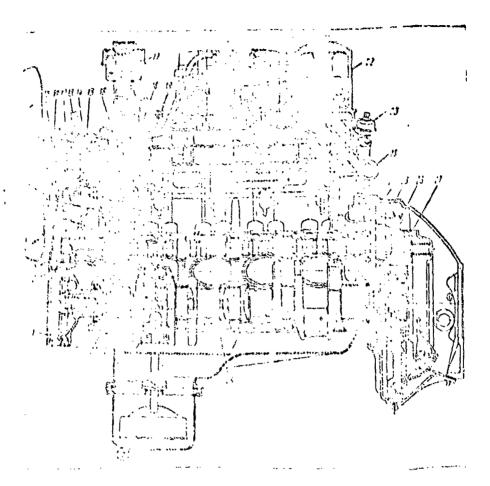


Plate 4-6. Longitudinal section of ZIL-131 engine:

1) crankshaft pulley 2) ignition timing index
5) revolution governor switch 4) switch drive
shaft 5) shaft spring 6) space ring 7) support
flange 8) camshaft gear cover 9) water pump
10) water pump and fan pulley 11) generator
drive belt 12) belt for hydraulic power steering pump 13) compressor drive belt 14) plug
15) lubrication fitting 16) engine lifting
rings 17) crankcase ventilation filter
18) fuel pump 19) pump red 20) fuel fine
cleaning filter 21) ventilation system valve
22) centrifugal oil cleaning filter 23) oil
pressure indicator switch 24) camshaft
25) insert 26) seal 27) clutch 28) crankshaft
29) support ring 30) crankshaft gear



Plate 4-7. Cylinder block

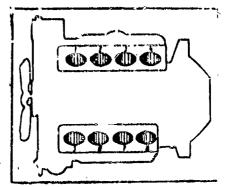


Plate 4-6. Order of cylinder numbering

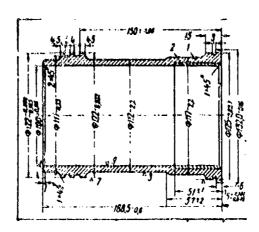


Plate 4-9, Cylinder block sleeve:
1) sleeve 2) sleeve insert

Part of the engines in 1964 and 1965 were released by the plant with iron oil rings. The connecting rods (Plate 4-15) are forged steel, with an I-section.

The crankshaft (Plate 4-16) is forged steel. To increase wear resistance, the main and connecting rod journals are subjected to surface hardening to a depth of 3.0-6.5 mm, with high frequency current. After hardening, the hardness of the shaft journal surfaces is HRC 52-62. The crankshaft is balanced. Allowable imbalance is no more than 30 gram cm. Imbalance is eliminated by drilling the crankshaft counterweights.

The crankshaft bearings, main and connecting rod, have thin-walled, easily removable inserts which are executed of trimetallic bands: a steel band, a sublayer of copper and nickel, and a layer of antifriction alloy.

ALT-6-6 alloy (antimony 5.5-6.5%; tin 5.5-6.5%; lead remainder) is used as the antifriction alloy in inserts. Thickness of the antifriction alloy on

the inserts is 0.08-0.12 mm. In the transfer to inserts made of steel-aluminum bands, their longevity is doubled over inserts made of trimetallic bands.

Sealing the crankshaft. Installation of crankshaft seals and packing is described in engine assembly. To eliminate oil leakage from the rear main bearing, oil-driving spiral grooves 4 are formed on the shaft journal (see Plate 4-16), and the seal area is knurled.

The flywheel (Plate 4-17) is iron, with a steel-toothed ring fitted on it for starting the engine with the starter. The flywheel and starter ring are press fitted.

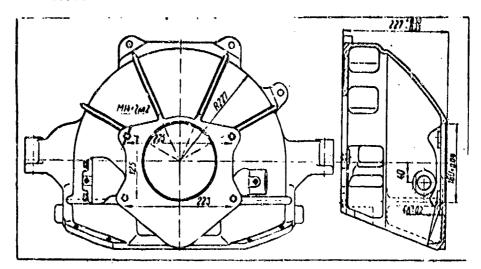


Plate 4-10. Clutch housing

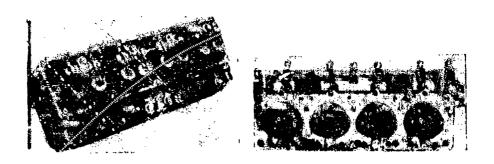


Plate 4-11. Cylinder head in assembly:
a) view from rocker arm side b) view
from compression chamber side

The camshaft (Plate 4-18) is steel, forged, and its support journals, lobes, and eccentric are subjected to surface hardening through high frequency current to a depth of 2-5 mm. After hardening, the journals have a hardness of HRC 54-62.

The gas distribution diagram for the engine is presented in Plate 4-19. The comshaft provides the following phases of gas distribution:

Intake valve opening31°	before TDC
Intake valve closing83°	
Exhaust valve opening	before BDC
Exhaust valve closing47°	after TDC

There is an eccentric on the drive shaft which drives the fuel pump, acting on the pump lever through rod 10 (see Plate 4-18). Spiral gear 15 is cut on the back end of the crankshaft, and, engaged with gear 13 and rotating shaft 17, drives the oil pump and distributor.

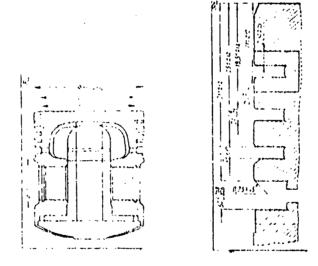


Plate 4-12. Piston: a) piston in section b) piston groove profile

Angles of gas distribution are given with a clearance of 0.30 mm between the rocker arm and the face of the valve stem.

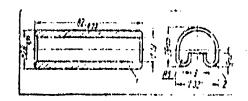


Plate 4-13. Piston wrist pin and stop ring:

1) wrist pin

2) ring

Nut 5, fastening the camshaft gear simultaneously fastens the drive assembly of the contribugal engine revolution governor switch, which consists of shaft 3 with spring 4 and washer 2, which in connection with the shaft goes into a slot in nut 5 and is fastened by stop ring 1.

The camshaft is installed in the cylinder block on 5 sliding bearings, which are bimetallic bushings pressed into the cylinder block. The camshaft is held in the cylinder block in a longitudinal direction by flange 9, which is mounted on it and fastened on the cylinder block with two bolts.

The profile of the camshaft lobes (Plate 4 20) is identical for both the intake and exhaust valves. The height of tapper lift is 6.85 ± 0.5 mm, and the height of valve lift is 10.25 mm.

The camshaft gears. The crankshaft gear (Plate 4-21, a) is steel. The camshaft gear (Plate 4-21, b) is cast iron.

The camshaft gear cover (Plate 4-22), made of aluminum alloy, is installed on a gasket. The cover is centered with two installation pins which are pressed into the cylinder block. The centering holes in the cover have a dimension of 10.023-10.050 mm.

The toothed indicator for timing setting and the switch of the centrifugal engine revolution governor are fastened onto the camshaft gear cover. The seal 1 of the front end of the crankshaft is pressed into assembly in the receptacle in the cover. The seal is self-pressing, and rubber with a metallic body, which is pressed into the cover receptacle with a mendrel 2 and hammer.

In all cases where there is nuticeable wear, visible cracks, or other damage on the working surface of the seal, and also in cases where the seal rubber is hardened or stretched, the seal is replaced.

The valves (Plate 4-23) are everhead, located in the cylinder head inclined to the axis of the cylinders, and are brought into motion by the camshaft through a push rod, tappet, and rocker arm. The valves are manufactured of

heat resistant steel, and the valve stems are chromed. The stem of the exhaust valve has a canal which is filled with sodium coolant, and for increased wear resistance, the working face has a surface made of heat resistant alloy. Holes in the valve are closed with a plug which ensures tightness. The plug aust sit tightly in its receptacle.

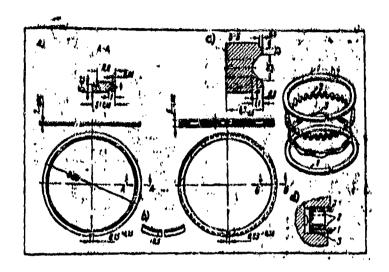


Plate 4-14. Pistor rings:
a) middle compression ring b) designation of repair dimension piston ring c) iron oil ring d) cross section of disassembled oil ring 1) ring disks
2) axial spreader 3) radial spreader 4) chromed cover layer of ring

To increase the life of the working surface of the exhaust valve, it has a compulsory rotating mechanism. (Plate 4-24, a). The mechanism consists of: a stationary body 4, five balls 5, and five return springs 12, located in depressions in the body, a conic disk spring 11, a washer 6 which absorbs valve spring load, and also a lock ring 7.

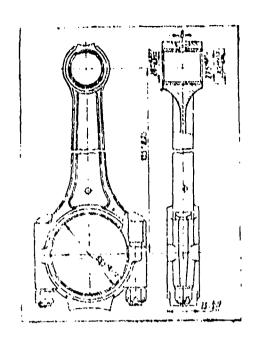


Plate 4-15. Connecting rod

The support washer and disk spring are freely fit with a clearance on body 4, which is located in a special receptacle in the cylinder head. With a closed valve, the effort of spring 8 through the support washer 6 is transmitted to the exterior edge of the disk spring 11 (Plate 4-24, b), which at that moment rests on the shoulder of the body 4 on its internal edge. During opening of the valve, through action of the compressed valve spring, the conic disk spring 11 begins to straighten out and rotate around the balls, pressing on them. From this moment, the force of the valve spring begins to be transmitted to the balls 5 (plate 4-24, c), which, rolling along the inclined surface of the cavity in body 4, rotate the conic disk spring 11 and support washer 6 around their axes, rotating the valve spring and valve together with them.

During closing of the valve, pressure of the valve spring decreases, and bend of the disk spring increases and, nearing its initial position, it ceases pressing on the balls. At this moment, the balls 5 are freed, and through action of the springs 12, returned to their original position, preparing the mechanism for the next step of rotation. If the rotation mechanism is damaged, it should be replaced.

The plate 9 of the valve spring is fastened with two keys 10, fitted on the valve stem, and holds the spring and valve in the cylinder head in assembly.

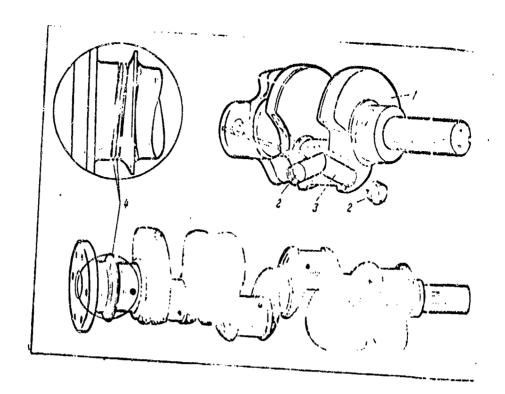


Plate 4-16. Crankshaft:
2) plug 3) dirt collector 4) oil driving spiral grooves

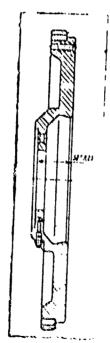


Plate 4-17. Plywheel

there was the same the same

Plate 4-18. Camshaft:

1) lock ring 2) centrifugal switch drive shaft washer
3) centrifugal switch drive shaft 4) shaft spring 5) gear
fastening nut 6) lock washer 7) camshaft gear 8) spacing
ring 9) support flange 10) fuel pump drive rod 11) end
of fuel pump lever 12) camshaft 13) oil pump and distributor
drive gear 14) drive body flange 15) gasket 16) shaft gear 17) oil pump and distributor drive shaft

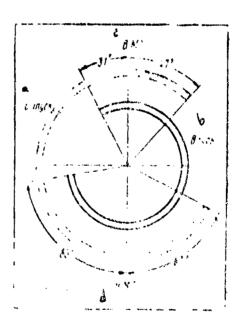


Diagram of gas distribution

Key: a) exhaust

c) TOC

b) intake

d) BDC

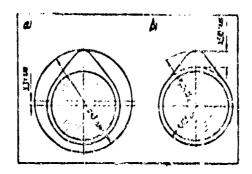
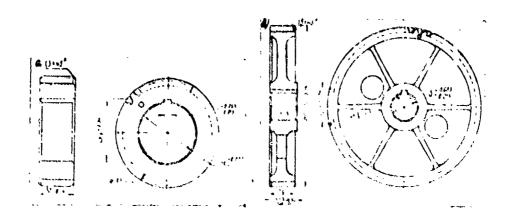


Plate 4-20. Camshaft lobes:
a) profile of eccentric for lifting fuel pump lever b) profile of lobe for lifting valve



Plato 4-21. Camshaft goar:
a) crankshaft goar
b, camshaft goar

In the process of the engine's operation, the valves will begin to leak as the result of harmful action of hot gases, corrosion, shock loads, and deposits of gummay substances on the working surface. Valve leakage with proper clearances between the stems and rocker arms (0.25-0.30 mm in a cold condition) and also with a properly adjusted carburetor and ignition equipment, is revealed through characteristic popping from the muffler and carburetor (the engine runs with a miss and does not develop full power).

The valve guides are pressed into the cylinder head. The valve springs are manufactured of type C-65-A wire. Valve seats are inserted and manufactured of heat resistant steel with a hardness of HRC 33-45. Seat dimensions are presented in Table 4-15.

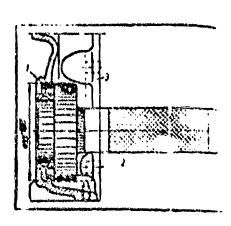


Plate 4-22. Camshaft gear cover:
1) seal 2) mandrel for pressing in seal 3) cover body

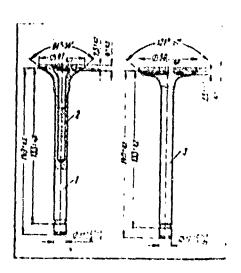


Plate 4-23. Valves:
1) exhaust valve 2) sodium filler
3) intake valve



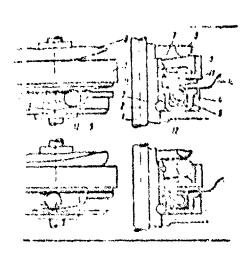


Plate 4-24. Exhaust valve rotation mechanism:

a) exhaust valve installed in cylinder head b) initial working position of mechanism c) finel working position of mechanism 1) exhaust valve 2) valve guide 3) lock ring 4) stationary hody 5) ball 6) support washer 7) lock ring 9) valve spring 9) valve spring plate 10) valve keys 11) disk spring 12) return spring 13) sodium filler 14) cylinder head 15) inserted valve seat

The tappets (Plate 4-25) are steel and hollow-bodied. They are arranged in holes in the upper part of the cylinder block. The holes do not have inserted bushings. To increase worksbility of the assembly pair (tappet and lobe), special cast iron is cast on the face of the tappet 5. Hardness of the tappet surface is no less than HRC 60, hardness of the tappet cup surface is within the limits of HRC 30-35, and hardness of the sphere beneath the push rod is no less than HRC 40

The valve push rod is steel. The tips of the push rod are heat treated with high frequency current so as to provide a hardened depth of no less than 2 mm and a hardness of the heated layer of no less than HRC 55.

The valve rocker arms are steel stampings. The ball surface of the rocker arm nose is hardened during during heating with high frequency current. Depth of the hardened layer is no less than 2 mm. A bronze bushing is pressed into the hole in the rocker arm. Interference in pressing this fitting must be 0.145-0.220 mm.

The adjusting screw is steel and has a passage for carrying oil from the rocker arm hole to the upper tip of the push Rod. The end of a screw with a spherical surface is subjected to hardening by heating with high frequency current to a depth of 1.2-2.0 mm.

Hardness of the sphere surface must be no less than HRC 52.

The rocker arm shaft (Plate 4-26) is manufactured of 45 steel (GOST 1050-60) and is hollow-bedied, allowing oil flow to the rocker arm as embly. The shaft surface is hardened by heating with high frequency current to a layer depth of 1.0-2.5 mm with a hardness of 1.8C 52-62 in the areas where the rocker arms ride on it.

Rocker arms with spacing springs and stands for fastening the shafts to the cylinder head are located on the shaft.

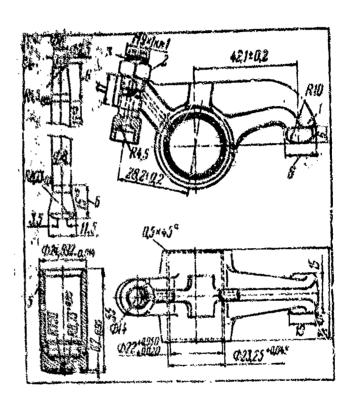
Stands 5, 7, and 13 of the shaft of the rocker arms 10 are cast of wrought iron and fitted with center steel bushings 14, pressed into their bolt holes. The rocker arm shaft is fastened to the cylinder head with four stands

The two middle stands are simultaneously oil removers. The rocker arm spacing spring 6 is steel, and is manufactured of 656 wire.

The intake manifold (Plate 4-27) is cast of aluminum alloy, installed on the top of the engine and fastened on study with nutt to both cylinder heads with rubber gaskets 12, and its end parts are fastened with rubber packing 7 and 13. The intake manifold simultaneously serves to heat the burning mixture, because passages 9, moving the burning mixture to the cylinders, are bathed in the hot liquid of the cooling system.

The carburetor, radiator pipe, and the oil filler neck with the crankcase ventilation filter and parts of the crankcase was exhaust system are fastened on upper flanges of the intake manifold. On the top of the manifold is the inscription with the numbers: "Firing order 1-5-4-2-6-3-7-8."

The intake manifold works at lower heat rates then the rest of the engine. and therefore it is not subjected to a great deal of warming.



- Plate 4-25. Valve mechanism parts;
 1) valve rocker arm 2) stop aut 3) rocker arm adjusting screw
- 4) tapper push rod 5) tapper 6) hurdoned eres

Exhaust manifolds. For the 211-130 engine, the exhuest manifolds are unit cast out of cast iron. For the ZIL-131, the manifolds are composite and cast out of wrought iron for their protection when fording streams. The right and loft munifolds and their gashets are interchangeable.

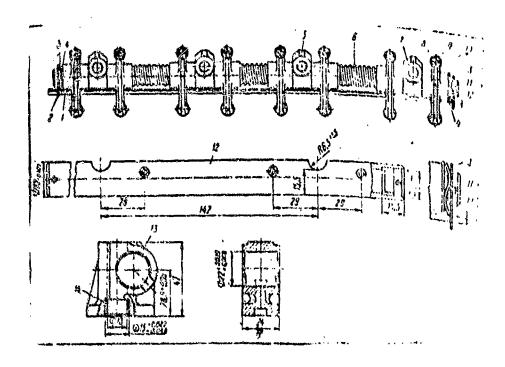


Plate 4-26. Shaft and rocker arm assembly:

1) oil line 2) line bracket 3), spring spacing washer

4) flat washer 5, 7, and 13) shaft stands 6) spacing apring 8) adjusting screw 9) screw stop nut 10) valve rocker arm 11) pin 12) rocker arm shaft 14) stand centering insert

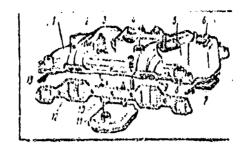


Plate 4-27.

1) manifold body 2) crankcase ventilation valve body 3) pipe fitting 4) milled surface for fastening carburetor 5) milled surface for fastening radiator pipe 6) milled surface for fastening oil filler neck 7 and 13) manifold face seals 8) cooling system passage 9) passages 10) oil trap and ventilation valve connecting sleeve 11) oil trap 12) manifold gasket

The lubricating system

The V-formed e gine lubrication system is mixed (under pressure and by splattering). Plate 4-28, a, shows a lubrication schematic for engines equipped with a partial flow filter (centrifugal filter and coarse oil cleaning filter), and Plate 4-28, b, shows a schematic with a full flow centrifugal cleaning filter (without coarse oil cleaning filter). The design of the full centrifugal oil cleaning filter is more perfect. Its installation in the engine began in the second half of 1967.

An oil radiator, installed in front of the water radiator, is projected for oil cooling.

Oil is pumped to the main and connecting rod crankshaft bearings, to the camshaft bearings, to the bearings of the distributor and oil pump drive shaft and to the tappets under pressure. Oil is pumped under varying pressure to

the rocker arm bushings through the hollow-bodied rocker arm shaft, at which the oil arrives through passages 8, leading from the middle bearing of the camshaft. Oil gets to the remaining working parts of the engine by gravity feed and splattering.

Oil is sucked through the stationary oil pickup 17 to the oil pump 3 from the oil pan. The oil pump moves oil through passage 4 in the rear wall of the block to the oil filter body, where the entire stream passes through the coarse cleaning plated filter 5. Part of the oil, about 50%, goes from the coarse cleaning filter to centrifugal oil cleaning filter 6, and from there to the oil pan.

The basic oil stream from the coarse cleaning filter goes into the distributing chamber 7, which is located on the rear wall of the cylinder block. From the distributing chamber, the oil moves in two longitudinal main passages 12 and 16, from which it goes to the crankshaft main bearings, and from them to the camshaft bearings. The oil moves through drillings in the crankshaft to hollows in the connecting rod journals, where if is additionally cleaned, and through holes in the connecting rod journals, it goes to the connecting rod bearings.

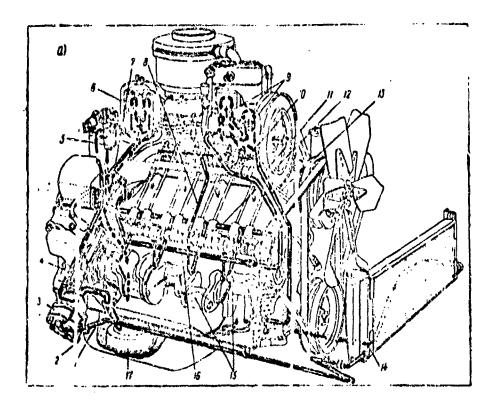
If the engine has a full flow contribugal oil cleaning filter, all the oil is cleaned in it alone, moves from it to the distributing chamber 7, and then into the longitudinal passages 12 and 16 and to the lubricated parts of the engine.

The big end of the connecting rod has a hole, and when it coincides with the hole in the crankshaft journal, oil is splashed onto the cylinder walls, from where it is removed by the bil ling, and then through holes in the oil ring groove, it moves to the inside of the piston and lubricates the wrist pin bearings in the piston end boss and in the small end of the connecting rod. Oil moves from the front right end of the main passage 16 through line 13 for lubricating the crankshaft and the connecting rod mechanism of the compressor.

The middle camshaft journal has two holes, bifurcated at an angle of 40° , and when these coincide with holes in the cylinder block, once per camshaft revolution, oil for lubricating the valve mechanism flows into passage 8 in each cylinder head.

From passage 4 (Plate 4-29) in the cylinder head, oil flows to hollow 3 through a slot in the bearing surface of the shaft stand and through the clear-ance between the stand and the connecting rod shaft fastening bolt. From hollow 3, oil flows from holes in the shaft to bushings in the rocker arms 2, and through passage 7 to the spherical joint between the testing screw 6 and tappet push rod 5. Wil flows through passage 8 to the cylinder head surface and, falling into the passages for the push rods, flows into the crankcase.

The valve stems in their guides and the exhaust valve rotation mechanism are lubricated with an oil mist and drops of oil which flow by gravity from the rocker arm mechanism joint.



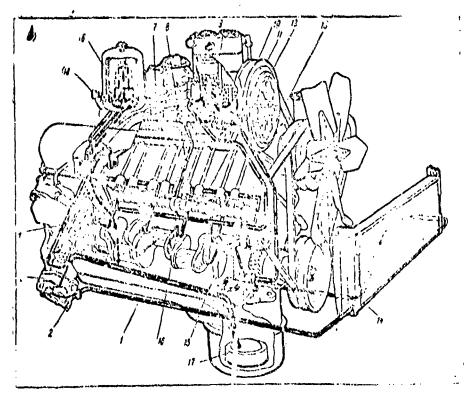


Plate 4-28

Plate 4-28 (on previous page): Schematic of engine lubrication:
a) ZIL-130 b) ZIL-131

1) pipe oil feed to the oil radiator 2) shut-off valve for oll radiator
3) oil pump 4) passage leading oil from pump to filter 5) coarse cleaning
filter 6) centrifugal cleaning filter 7) distribution chamber 8) oil feed
passage to rocker arms 9) direction of oil feed to compressor crank and
connecting rod assembly 10) hollow rocker arm shaft 11) pipe for oil flow
from compressor 12) left main passage 13) oil feed line to compressor
14) oil flow line from radiator 15) dirt collectors and crankshaft connecting
rod journals 16) right main passage 17) oil pickup 18) oil pressure indicator switch

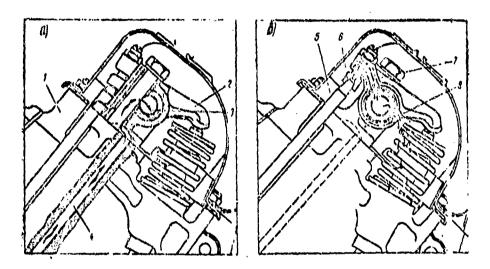


Plate 4-29. Schematic of rocker arm mechanism lubrication:
a) oil flow to rocker arm shaft b) rocker arm lubrication
and oil exhaust 1) cylinder head 2) rocker arm 3) rocker
arm shaft hollow 4) oil passage in cylinder head 5) push
rod 6) adjusting scrow 7) passage for oil supply to scrow
and push rod joint 8) oil exhaust passage from rocker arm
shaft

The oil pump (Plate 4-30) is geared, with two sections. Productivity of the upper section of a new pump at an engine crankshaft speed of 3100 rpm is 50 liters per minute, and that of the lower section is 23 liters per minute. The upper section of the pump moves oil to the centrifugal oil cleaning filter, and then to the engine lubrication system. Working pressure created in this section and in the lubrication system is maintained by a reduction valve installed in the intermediate cover of the pump, and adjusted to 2.75-3.30 kg/cm². In the event of pressure increase, the reduction valve bypasses oil from the

pressure hollow of the oil pump to the suction one.

With a properly working upper section reduction valve, oil pressure in the lubrication of a new warm engine at 1200 crankshaft rpm, must be no lower than 2.5 kg/cm². For a warm engine in operation, the minimum allowable oil pressure in the lubrication system must be 1.5 kg/cm² at 1800 rpm, and 0.5 kg/cm² at 500 rpm.

With an oil pressure lower than the cited limits, operation of the engine is not allowed, in order to prevent its early failure. If deviation from the cited reference pressures are observed during checking, it is necessary to remove the reduction valve—assembly and check the condition of its parts. The parts, after having oil residue cleaned from them and having been washed in kerosene, must freely move in the reduction valve body.

The bottom section of the pump moves oil from the oil radiator through a needle valve which is screwed into the pump cover body. Pressure in this section is supported by a by-pass valve which is installed in the lower section body and adjusted to a pressure of $1.2-1.5 \text{ kg/cm}^2$.

Crankcase ventilation of the ZIL-130 engine is forced, with extraction of worked-out gases into the engine intake manifold through valve 5 (Plate 4-31).

The valve is installed in the intake manifold in a hole connected to the internal space of the engine. When valve 5 is opened, gases are sucked along tube 3 to the central portion of the intake manifold 6, from which they are attracted together with the burning mixture into the engine cylinders 7 and burned there.

The extraction of gases basically takes place during the operation of the engine with a fully opened throttle, when vacuum in the intake manifold increases and the valve falls under its own weight, fully opening the passage section for exhaust of gases which are accumulated in the engine crankcase.

When the engine is operating with the throttle plate less than fully open, the valve 5, due to action of the weaker vacuum in the intake manifold, moves upward, the upward step section of the valve moves into the hole in the pipe nipple 3 and decreases the passage section for gas exhaust.

Fresh air moving into the engine crank.case is cleaned in filter 1, which is fastened on the oil filler pipe.

Before reaching valve 5 on the passage from the inner hollow of the engine, spent gases pass through an oil trap 2, which separates particles of oil from the gases being extracted.

The ZIL-131 engine has, besides this, a valve on tube 3 between valve 5 and the intake manifold for shutting off the ventilation system. When fording streams, this valve must be closed.

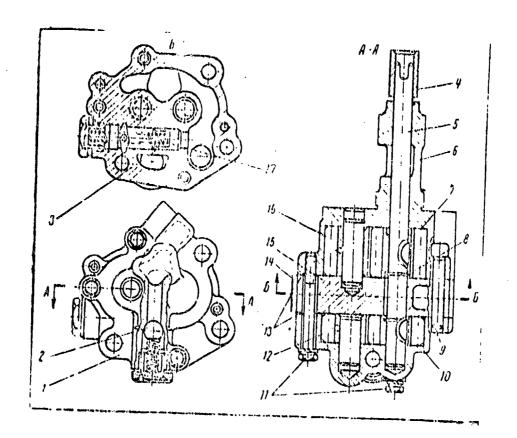


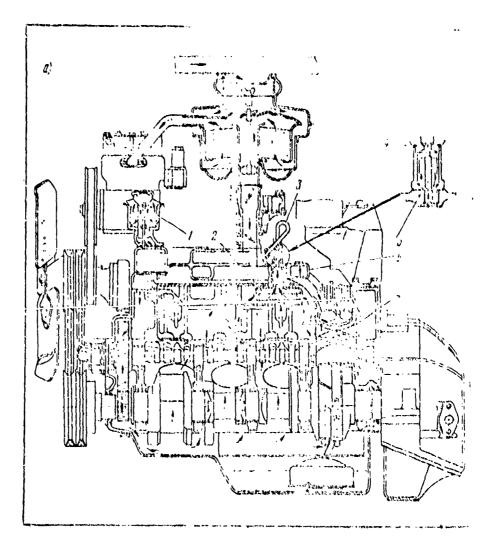
Plate 4-30. Oil pump:

sleeve 5) pump shaft 6) upper section body 7) upper section drive gear

8) stop ring 9) pin 10) lower section drive gear 11) bolts 12) lower section driven gear 13) gaskets 14) plug 15) pump intermediate cover 16) upper section driven gear 17) reduction valve spring

The oil filters. The coarse cleaning oil filter (Plate 4-32) is a slotted type, with plates, and with a by-pass valve adjusted to a pressure drop of 1 kg/cm². The by-pass valve spring must have a length of 62 mm in its free state and a length of 44 mm under a load of 0.9-1.1 kg. The centrifugal oil cleaning filter works with reaction drive. Both filters are connected and installed in one aluminum housing. For ease in turning the coarse cleaning filter element, the filter on the ZIL-131 truck has a lengthened handle.

The centrifugal oil cleaning filter rotates due to reaction to the force of the oil stream projected through two nozzles under pressure. Under oil pressure of 2.75-3.30 kg/cm², the filter body and the oil is it rotate at a speed of 5000-6000 rpm. Due to action of the arising forces, mechanical articles located in the oil are thrown against the cover, where they adhere, forming a cleanings is set in the lubrication chart.



然 对他们 扩展:特别连续的成体

Plate 4-31. Schematic of engine crankcase ventilation:
a) ZIL-130 b) (on next page) ZIL-131 1) oil filler
tube filter 2) oil trap 3) gas exhaust tube 4) nipple
5) valve 6) intake manifold 7) engine cylinder

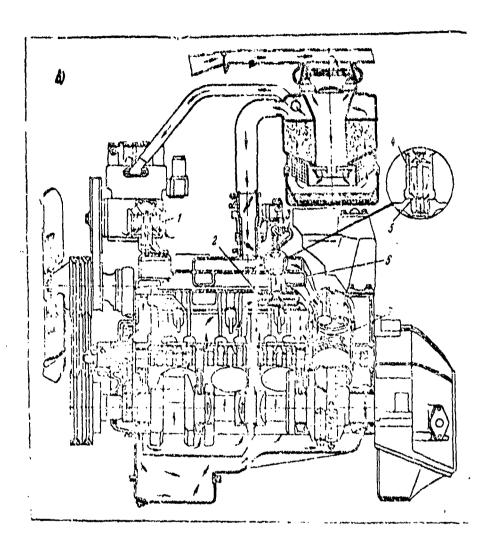
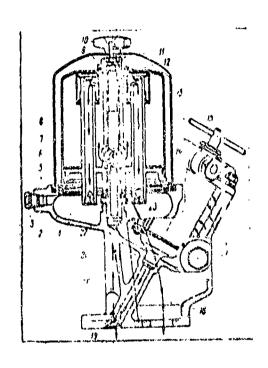


Plate 4-31 b.

Cleaned oil passes through the nozzles into the oil filter body 1, from which it drains into the oil pan.

Centrifugal oil cleaning in the engine is additionally provided in the dirt collectors formed in the connecting rod journals of the crankshaft. The crankshaft dirt collectors should be cleaned when the inserts are replaced.

Since the third quarter of 1967, the new design (without coarse cleaning filter) oil filter (Plate 4-33) has been installed on the ZIL-130 and ZIL-131 engines. This is a full flow centrifugal oil cleaning filter with reaction drive.



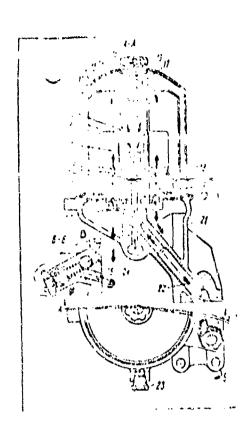


Plate 4-32. Combined oil filter (contribugal cleaning filter and coarse cleaning filter); 1) body 2) nozzle 3) plug 4) jacket packing ring 5) jacket 6) cover packing ring 7) centrifugal oil cleaning filter body 8) cover 9, 10, 11) nuts 12) stop ring 13) mesh filter 14) hollow shaft 15) handle 16) coarse cleaning plate filter 17) plug for draining oil from course cleaning filter 16) direction of motion from filter to crankcase 19) direction of oil motion from filter to lubricating system 20) direction of oil movement in centrifugal oil cleaning filter 21) direction of oil movemeth from oil pump to coarse cleaning filter body 22) support bearing 25) oil deflection plate

Plate 4-33. Full flow contrifugal eil cleaning filter: 1) nozzles 2) gasket 3) body 4) cover packing ring 5) cover 6) mesh filter 7) filter insert 8) jacket 9) shaft 10) insert packing ring 11) stop ring 12) gasket 13) washer 14) filter cover nut 15) jacket fastening nut 16) shaft 17) support washer 18) shaft pipe 19) bearing support ring 20) support bearing 21) filter body 22) passage directing oil to centrifuge 23) plug 24) passage directing oil to engine block distributing chamber 25) direction of oil in engine oil pan 26) bypass valve ball 27) by-pass valve pressure passage D and F) by-pass canals

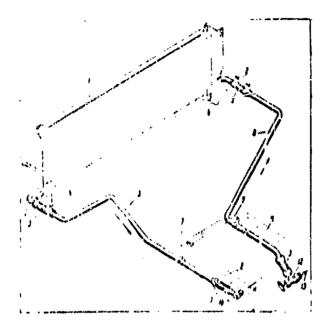


Plate 4-34. Oil radiator:

1) radiator frame 2) tension clamps 3) connecting hose 4 and 6) radiator side brackets 5) radiator oil exhaust line 7 and 9) line fastening brackets 8) radiator oil intake line 10) angle fitting 11) engine oil pan 12) valve 13) direction of oil from oil pump lower section 14) direction of oil into oil pan

Oil, driven by the engine pump, goes into passage 22 of the filter body. From this passage, oil moves under insert 7 through the circular clearance around pipe 18 and through the radial holes in the tube and filter body 3. From here, part of the oil moves to the nozzles 1 through the mesh filter 6, preventing the nozzles from clogging, and the other part of the oil, passing through the holes in the insert, has dirt removed from it in the filter. The principle of operation of the ivil flow filter is the same as that of the combined filter (centrifugal cleaning filter and coarse cleaning filter). Oil, passing through the nozzles, flows into the engine oil pan.

Clean oil, driven above insert 7, through the radial holes in the upper portion of body 3, through the circular clearance around shaft 9 and the radial holes in the upper part of the shaft, moves into tube 18 and into passage 24 of the filter body and the cylinder block distributing chamber, and then into the longitudinal engine lubrication system passages.

The by-pass valve ball 26 is installed in the passage of filter body 21 and is adjusted to a pressure drop of 1 kg/cm². The by-pass valve is intended

to release part of the oil into the distributing chamber of the cylinder block avoiding the filter, when starting a cold engine with high oil viscosity, and also with significant wear of the engine bearings and the increased flow of oil through the filter in connection with this.

The by-pass valve spring is manufactured of class 1 spring wire, 0.9 mm in diameter (GOST 9389-60) and has 14 working coils. The length of the spring is 58.5 mm in a frae condition, and 34 mm under a load of 1.06-1.26 kg, and spring diameter is 11.5 mm.

The full flow filter in assembly is interchangeable with the partial flow filter. Certain of their parts, besides the jacket, are not interchangeable.

The oil radiator (Plate 3-34) is fastened by four bolts to brackets which are fastened to the frame of the water radiator louvres. In 1966, height of the oil radiator was decreased to 28.5 mm (three rows of pipes were eliminated).

The cooling system

The engine cooling system (Plate 4-35) is liquid, closed type, with forced cooling liquid circulation. For normal engine operation, temperature of the cooling liquid is maintained within the limits of 80-95°C.

The cooling system includes: the water jacket of the cylinder block and head, water pump with its drive, fan with its shroud (diffuser), radiator, plug valves, radiator louvres, thermostat, connecting pipes with homes, drain valves and control devices. The voiler of the starting preheater is hooked into the cooling system.

The cooling liquid, heated to a temperature of 80-95°C, moves from the bottom tank of the radiator 2 to the water pump 5 through the pipe and rubber hoses. It is then driven by the water pump into both hollows of the water jacket of the cylinder block 13, bathing the cylinder sleeves on all sides. The liquid simultaneously rushes through holes in the cylinder block into the space of the cylinder head cooling jacket, bathing and cooling the ribs for the valve receptacles, after which it moves into the space in the intake manifold 11, where it heats the working mixture moving into the engine cylinders. From the space in the intake manifold, the liquid moves into the upper radiator tank, passing through the upper pipe 9, thermostat 10, and rubber hose. The liquid is cooled in the radiator and once more repeats the process of circulation through the closed circuit through the engine cooling spaces.

When the engine is cold and while the liquid is heating, it circulates through a (small) closed circuit in the following order. From a space in the intake manifold 11, liquid moves through hose 7 into the space in the compressor, and then through hose 6 into the hollow of pump 5, from which it is again directed into the engine cooling system, avoiding the radiator. When

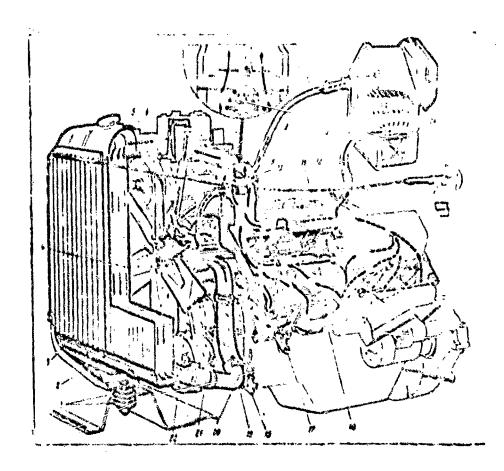


Plate 4-35. Cooling system of the ZIL-130 (ZIL-131) engine:

engine:

1) radictor support 2) radiator 3) radiator louvres 4) fan

5) water pump 6) water hose from compressor 7) water hose to

co-pressor 3) water hose from heater 9) upper pipe 10) thesmo
stat 11) intake manifold 12) heater water shut-off valve

13) water hose to heater 14) cab heater 15) louvre operation

hundle 16) cylinder block 17) cylinder block water jacket

drain plus 10) radiator drain cock 19) radiator bottom pipe

20) drain cock control lever 21), lower pip 22) augmentor hose

the cooling liquid is heaten and reaches a set 'emperature, the thermostat valve opens and begins to release I quid into the registor, and it will then circulate around a (large) closed circuit through the radiator.

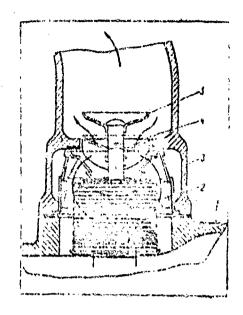


Plate 4-36. Liquid type thermostat with pipe:

- 1) intake manifold 2) bellows 3) pipe
- 4) valve in closed position 5) valve in open position

For improving the working conditions of the engine cooling system and to eliminate the possibility of overheating the engine, an exhaust mainline was introduced in 1967; it connects the cylinder head cooling jacket hollow with the intake hollow of the water pump through augmenter hose 22 and lower pipe 21. With this, hot water exhaust takes place constantly with the thermostat valve either closed or open. The first models of the ZIL-130 angine have a liquid type thermostat. Later models have thermostats with hard fillers.

The liquid type thermostat is installed in its pipe 3 (Plate 4-36), which is installed on the intake manifold. The thermostat valve begins to open when the cooling liquid reaches a temperature of 70 ±2°C. At a lower liquid temperature, the cylinder of bellows 2 is in a pressed condition, with which valve 4 of the thermostat is closed, as a result of which the cooling liquid does not reach the radiator. When the cooling liquid reaches 70 ±2°C, the corrugated cylinder of the bellows begins to expand. With a temperature of 83 ±2°C, the valve 4 is fully opened to a valve raising height of no loss than 9 mm, with which the cooling liquid from the intake manifold space is freely directed into the radiator.

With the installation of a liquid thermostat, a radiator cap with valves

maintaining cooling system overflow pressure at 0.65 kg/cm² was used. With this pressure, water in the system boils at a temperature of 114°C.

A thormostat with a hard filler has an active mass of a mixture of ceresin and powdered copper. The active mass 2 (Flate 4-37, a) is located in a thin-walled copper capsule 1 enclosed with a rubber diaphragm 3. A rubber buffer is installed above the diaphragm, protecting it from damage. A rod 5 is installed above the buffer and is connected through lever 8 with valve 6, which is retained in the closed position by spring 9.

When the cooling liquid is heated to a temperature within the limits of 69 *2.5°C, the active wass in the capsule begins to melt and expand, moving the diaphragm upward.

With this, the diaphragm acts on the burfer and the rod, which, rising, presses on the lever and opens the valve. With a temperature of 83 *2°C, the valve is fully opened and the cooling liquid begins to circulate around the large circulat through the water radiator.

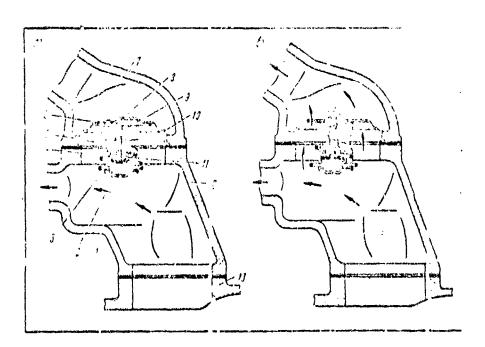
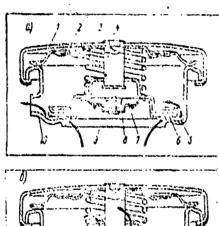


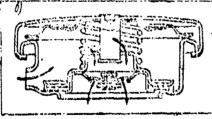
Plate 4-37. Schematic of operation of thermostat with hard filler:
a) thermostat with closed valve b) thermostat with open valve 1) copper capsule 2) active mass 3) rubber diaphragm 4) body 5) rod 6) valve 7) upper pipe 8) lever 9) spring 10) valve seat 11) rubber buffer 12) lower pipe 13) intake manifold

Plate 4-37 b shows the thermostat valve in an open position. When cooled, the active mass hardens, its volume decreases, the diaphragm moves downward, and the valve is closed by action of the spring. When this happens, the cooling liquid begins to circulate ground the small circuit, missing the radiator. Thermostats are not repaired. The allogable overflow pressure of 1 kg/cm² requires precise tightening of the hose clamps. If the clamps are insufficiently tightened, the overflow pressure might blow off the hose. Overflow pressure is regulated by the outlet valve 6 (Plate 4-38), which opens at a pressure of 1.0 kg/cm². At this pressure, water in the cooling system boils at 119°C.

The inlet valve 9 of the cap opens and connects the radiator hollow with the atmosphere at a vacuum equal to 0.01-0.13 kg/cm².

If the rubber packing washers of the valves on the cap are missing or damaged, the cooling system will not work as a closed one, cooling of the liquid will begin at 100°C, and the engine will begin overheating significantly sooner. In these cases, either the cap should be replaced or the vacuum washers of the valves should be replaced.





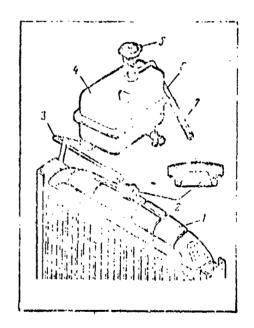


Plate 4-38. Radiator cap:

- a) with open outlet valve
- b) with open inlet valve
- 1) cover body 2) support washer
- 3) outlet valve spring
- 4 and 5) outlet valve cup
- 6) outlet valve (packing) 7) in-
- let valve cup 8) inlet valve
- spring 9) inlet valve (packing)
- 10) overflow opening

Plate 4-39. Connection of condensation tank to radiator:

- 1) radiator 2) radiator cap (without valves) 3) connecting line 4) condensation tank 5) tank cap (with valves)
- 6) overflow line 7) rubber hose

On special order, the ZIL-130 and ZIL-131 trucks intended for work in tropical climatic conditions are equipped with a condensation tank 4 (Plate 4-39). With this arrangement, cap 5 with valves is removed from the radiator and installed on the condensation tank, and the radiator neck is covered with cap 2 (without valves).

The presence of the condensation tank makes the engine cooling system more effective, working without loss of water. With an increased water temperature in the radiator (to belling temperature), steam moves along the connecting line 3 to tank 4 and condenses into water. When the water temperature decreases, the vacuum is created in the top tank of the radiator, and water is sucked from the condensation tank brek into the radiator, bringing it to its full level.

The radiator (Plate 4-40) is tubed, with a cooling surface executed in the form of blades 0.15 mm thick or in the form of a corrugated band 0.1 mm thick layed in a serpentine manner. The radiator tubes are made of L90 tombac the cooling band (serpent) for the radiator is manufactured of M3 copper, as are the cooling plates.

A three-row radiator is used for the ZIL-130 motor vehicles, and the ZIL-131 and ZIL-1308 motor vehicles are assembled with four-row radiators. The radiator, together with its louvres and fan shroud, is fastened with bolts into a special frame, which is fastened with a central bolt through rubber cushions to a frame cross-member of the truck. The top ends of the frame, locked in with the tension rod and sainforcement of the radiator jacket, serve as the front support for the truck's body work, including the radiator jacket.

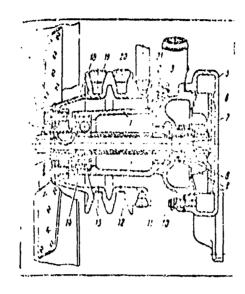
Water release from the radiator hollow is accomplished through drain cock 18 (see Plate 4-35), whose valve is rotated by lever 20.





Plate 4-40. Cooling system radiator:

- a) with shroud
- b) without shroud



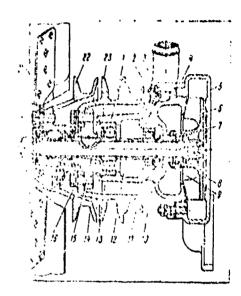


Plate 4-41. Water pump with fan
of ZIL-130 engine:

1) bearing body 2) plug 3) lubrication fitting 4) gasket 5) pump
body 6) impeller 7) rubber packing
8) support washer 9) impeller race
10) deflector 11 and 13) bearings
12) spacing bushing 14) water pump
shaft 15) conic pulley bushing
16) pulley flange 17) fan
18) pulley 19, 20, and 21) drive
belts

Plate 4-42. Water pump with fan of

ZIL-131 engine:

1) bearing body 2) plug 3) lubrication fitting 4) gasket 5) pump
body 6) impeller 7) rubber packing
8) support washer 9) impeller race
10) deflector 11 and 13) bearings
12 and 19) spacing bushings 14) water
pump shaft 15) pulley bushing
16) pump pulley flange 17) lubrication fitting 13) bearings 20) nut
21) fan 22) pulley 23) pump pulley

The water pump. The ZIL-130 engine uses a pump with a fan whose hub is rigidly fastened to the pump shaft with a key (Plate 4-41). The ZIL-131 engine uses a pump with a fan whose hub is installed on the shaft on two hell bearings (Plate 4-42). This allows the fan drive belt to be loosened for deep fording, stopping rotation of the fan without stopping operation of the water pump, compressor, or hydraulic power steering pump.

Both water pumps are centrifugal, with a productivity of 350-360 liters per minute at an engine crankshaft speed of 3000 rpm. The turning ratio between the water pump drive pulleys and the crankshaft is 1.17: 1.

In the process of the engine's operation, the following water pump parts wear out: bearings 11 and 13 (Plates 4-41 and 4-42), bearings 18 (Plate 4-42), bearing seat holes in the pump body 1 and in the pulley hub 22, and the packing

and pump shaft assembly.

Water pump bearings have a packing which holds grease and protects them from dirt.

The water pump shaft is subjected to hardening by heating with high-frequency current. The depth of the hardened layer is 1-3 mm. Hardness is HRC 52-62.

The fan is six-bladed with turned-out ends, which increase its effectiveness. To increase the exhaust of heat from the radiator, the fan is enclosed in a shroud (diffuser), which promotes the increased speed of the air stream passing through the radiator.

Blade material thickness on the first models of the trucks was 1.2 mm. Since 1964, blade material has been 1.5 mm thick.

It should be kept in mind that up to 1965, fans with single cross pieces were installed on the ZIL-130 motor vehicles and fastened with bolts 25 mm in length. Since 1965, fans with double cross pieces have been installed and fastened with bolts which are 28 mm long.

The starting preheater. Some of the ZIL-157K, ZIL-130, and all of the ZIL-131 motor vehicles are equipped with P-100 starting preheaters (Plate 4-43).

The starting preheater works on gasoline. In consideration for its mounting on various engines, the preheater pipes are welded on in various fashions, and for this reason the preheater boils are not interchangeable. The preheater is a one-pice boiler 18, consisting of four cylinders inserted one inside the other, welded together and forming a combustion chamber 28, heat pipe 31, and gas exhaust 32, with two liquid hollows 29 and 30, which are connected together (heat exchanger). The boiler is permanently connected to the engine cooling system.

On the ZIL-130 engine, fuel flows from the tank to the boiler combustion chamber by gravity. For even flow of fuel to the combustion chamber, and to provide a normal burning process, the fuel feed regulator 7 is provided, and confists of a float chamber with adjusting needle 9 and solanoid valve 8. Fuel level in the float chamber is adjusted by the needle valve. From the float chamber, fuel flows to the solanoid blocking valve along a passage. The valve works in the following manner: when the switch 23 on the control panel is disengaged, the core, under action of the spring, blocks the fuel line; when the switch is engaged, current flows to the coil, the core is withdrawn, and fuel flows unhindered to the boiler combustion chamber.

Air is driven to the combustion chamber by a fan which is turned by electric motor 5, which is installed under the engine hood in the ZIL-130 and ZXL-131 motor vehicles, and in the cab on the ZIL-157K motor vehicle.

The mixture is ignited with a glow plug 14. After steady burning takes place in the chamber, the plug is turned off and fuel ignition is sustained by

the burning flames.

Control of the preheater's electrical system is concentrated on panel 21, on which the glow plug switch 24 is installed. The control spimal (resistance) 22, sequentially engaged in the plug circuit, and the switch 23 of the solanoid and fan electric motor are also installed on the panel. This switch has three positions:

After ignition, the hot gases move in a twisting stream along the heating ripe and transfer heat to the heated liquid or into the boiler. Gases flowing out of the outlet pipe are directed to the engine oil pan by trough 16 and warm the oil located in it. The liquid hollow of the preheater boiler is connected with the engine cooling system by pipes 19 and 15.

Engine starting sequence using the preheater. For preheating and starting an engine in which there is no water, it is necessary to prepare 32-35 liters of water. Close the radiator louvres, and with heavy freezing, install the warming cover on the radiator jacket, open the radiator cap, close the preheater boiler drain cock and preheater pipe drain cock. If there is no fuel in the tank or it is insufficient, it is necessary to fill the tank with fuel, unscrewing the plug. Pour 1.5 liters of water into the preheater boiler through funnel 3.

Move the handle of switch 23 into position II for 15-20 seconds, so that the fan electric motor is on and the solanoid valve is open. In very low temperatures, this time must be increased to 60 seconds.

Place the switch handle into position 0 and turn on the glow plug. When a light red glow is attained on the control spiral, ignition will occur in the combustion chamber, during which a weak pop will be heard. Then start the preheater, moving the handle of switch 23 into position II. When steady operation of the preheater is attained, turn off the glow plug.

If, for some reason, the preheater does not begin to work, repeat its starting. When 1-2 minutes have elapsed after starting of the preheater, add 6-8 liters of water to the engine through the boiler funnel, close the fumel cap and continue heating the engine. When water in the engine is warm and light steam appears from the radiator filler nock, turn the engine crankshaft a few times with the starting crank. For the crankshaft to be ready for starting the engine, it must be rotated easily.

After heating the entire, turn off the preheater, moving switch 23 into position I (to boiler flowing) and close valve 4. When humming of the flame

in the preheater boiler stops (after 50-60 seconds), turn off the fan and, after moving the switch to position 0, start the engine.

If this order of preheater shutdown is not observed, flames may shoot up and ignite the air hose 13. Warming the engine at middle revolutions, it is necessary to add water to the engine through the radiator filler neck until the entire volume of its cooling system is filled.

The P-100 preheater can be used equally well with either water or antifreeze as a cooling liquid. Since the preheater boiler need not be used during the summer, it is recommended that it be removed and kept at the motor vehicle transport anterprise warehouse for the summer period.

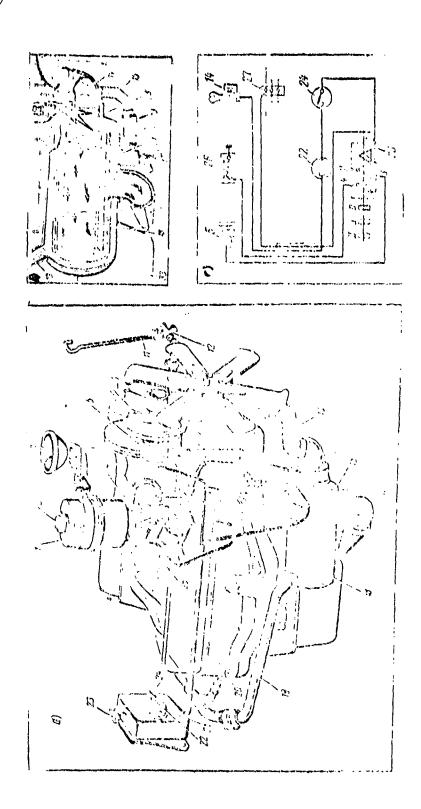
Technical servicing. Assembly drive belts (Plate 4-44 a) on the engine must be tightened so that bend of one side of the belt under a load of 4 kg is within the limits of 8-14 mm for the hydraulic pump and generator belts and 5-8 mm for the compressor belt. Belt tightening (Plate 4-44 b) of the generator, fan (water pump), and power steering hydraulic pump is accomplished by moving the generator and hydraulic power steering pump.

On compressors having a cast pulley 1 (Plate 4-45) with an adjustable groove width, compressor belt tensioning is accomplished by the method of screwing in the thread adjusting sleeve to the wrench 3, with stop screw 4 loosened. The amount of compressor belt bending with cast or stamped pulleys must be 5-8 mm under a load of $4 \, \mathrm{kg}$.

The factory is preparing a method of compressor belt tightening by moving the compressor for introduction into production. This involves changing its brackets, in which longitudinal holes are made to move the compressor in a direction perpendicular to the geometric axis of the engine.

Tightening the cylinder head fastening bolts should be done on a cold engine. Each cylinder head is fastened to the block with 17 bolts. Bolts fastening the head to the cylinder block must be tightened with a torque wrench, allowing the torque moment to be controlled. When the engine heats up, cylinder head tightening bolt torque increases, and when it cools, bolt torque decreases. Cylinder head bolt torque moment must be 7-9 kg meters of a cold engine, and closer to the lower limit (7 kg meters) with lower engine temperatures. With an engine temperature of 20-25°C, the moment must be closer to the upper limit of 9 kg meters. For the first 6000 km of running, the cylinder head fastening bolts must be tightened at every TS-1, and after this period, every TS-2.

Tightening of cylinder head bolts should be done in a determined sequence (Plate 4-46) beginning from the center of the head. Attention should be paid to the fact that on the ZIL-130 and ZIL 131 entines, four bolts fastening the rocker arm shaft are also cylinder head fastening bolts, and should also be tightened. Whenever the cylinder head fastening bolts are tightened, it is necessary to check for possible changes in the clears. between the rocker arms and the valves. The rocker arm cover nuts should be tightened equally a moment of 0.5-0.6 kg meters, and no more. Increasing the corque moment on the rocker arm cover will lead to deformation of the rubber gasket installed beneath it.



22) control spiral 17) boiler drain valve 18) heater c) control panel electrical solanoid valve 9) adjusting needle 10) line from 21) control panel b) schematic of preheater mutor operation glow plug 15) outlet line 16) air funnel 20) feader fitting 4) valve Preheater: 3) filling funnel Plate 4-43. 19) feeder line from boiler to engine 7; fuel feed regulator 6) tank drain cock

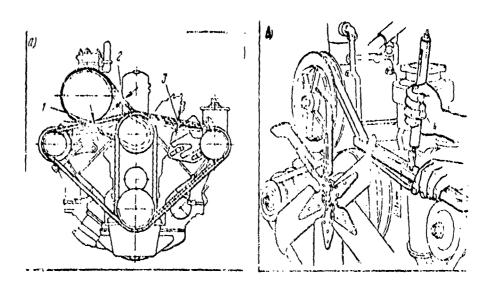


Plate 4-44. Location diagram and method of checking engine drive belt tightness:

a) belt location diagram b) method of checking hydraulic power steering pump drive belt tightness 1, 2, and 3) drive belt

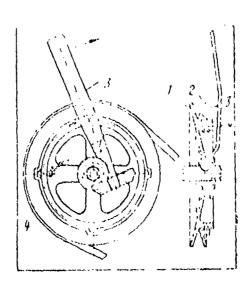


Plate 4-45. Method of adjusting compressor drive belt tension

[Key to Plate 4-43, continued]: 23) switch 24) glow plug switch 25) line for draining fuel 26) solanoid valve coil 27) connecting panel for left nozzle 28) combustion chamber 29) boiler internal liquid cavity 30) boiler external liquid cavity 31) boiler heat pipe 32) boiler exhaust gas passage 33) engine oil pan

Checking and adjusting clearances in the engine valves is necessary upon appearance of splattering in the valves. Before adjusting clearances, it is necessary to remove the high tension leads, disconnect them from the spark plugs, unscrew the rocker arm cover nuts, and remove the covers and gaskets. Clearances between the valves and rocker arms is adjusted on a cold engine, with the adjusting screw and stop nut which are on the short end of the rocker arm.

Adjustment of clearances by the first method is done in the following order. Set the piston on the number I cylinder at TDC (compression stroke), using the installed notched indicator (Plate 4-47). For this, the crankshaft should be rotated until the mark on the shaft pulley coincides with the TDC mark on the indicator.

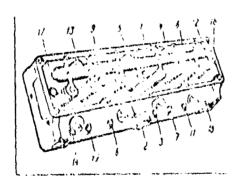


Plate 4-46. Tightening order of cylinder head bolts

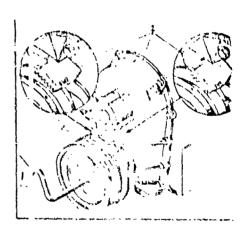


Plate 4-47. Setting the piston of the number 1 cylinder at TDC using the notched indicator: a) mark on pulley 2) notched indicator (Numbers show rotation of the crankshaft in degrees)

In this case, both valves, intake and exhaust, of the first cylinder will be closed, the maximum clearance will be formed between the valve stem and the contact end of the rocker arm; it can be measured with a leaf gauge and, if necessary, adjusted.

To adjust the clearance, it is necessary to loosen the stock nut with a wrench while holding the adjusting screw with a screwdriver (Plate 4-48, a). After this, the leaf gauge is inserted between the valve stem and the contact end of the rocker arm, and the adjusting screw is turned with a screwdriver (Plate 4-48, b), setting the required clearance. After this, leaving the leaf gauge in the clearance, tighten the adjusting screw with the stop nut, using the wrench and screwdriver (Plate 4-48, c). After adjustment, the clearance must be equal to 0.25-0.31 mm for intake and exhaust valves, so that a 0.25 mm leaf gauge may freely pass through the clearance, and a 0.30 mm gauge cannot pass through.

For adjusting the clearance in the valves of the other seven cylinders, it is necessary to rotate the crankshaft with a crank by one quarter of a revolution (by 90°) and perform the adjustment according to the indicated method. With clearance adjustment being performed sequentially, agreeing with the cylinder firing order 1-5-4-2-6-3-7-8, which is illustrated by the connecting lines and arrows on Plate 4-48, d. In order to accurately turn the crankshaft by one quarter of a revolution, it is necessary to make marks on the crankshaft pulley with soap, separating them by an angle of 90°, with the number 1 cylinder located at TDC (compression stroke). In the second method, valves are adjusted simultaneously for several cylinders. Adjustment takes place in the following sequence. Set the piston of the number 1 cylinder at TDC (compression stroke) according to the method shown above, and adjust the clearances of the: intake and exhaust valves of the first cylinder, exhaust valve of the second cylinder, intake valve of the third cylinder, exhaust valve of the fourth cylinder, exhaust valve of the fifth cylinder, intake valve of the seventh cylinder, and intake valve of the eighth cylinder. Clearances in the remaining valves should be adjusted after retating the crankshaft 360° (a full revolution). After completing valve clearance adjustment, it is necessary to install the rocker arm cover with its gasket in place and fasten it with nuts and flat washers. Start the engine and listen to it run. A warm engine must work without valve clatter, "coughing" in the carbureter, and 'backfiring" in the muffler.

To avoid grinding of the ball springs, it is necessary in any disassembly of an engine having run 70,000 km to disassemble the exhaust valve rotating mechanisms and turn the ball disk springs upside down so that their worm side is down.

The order of checking compression in a V-engine is the same as in in-line engine cylinders. Compression in the cylinders of a warm V-engine must be within the limits of 7.5-8.5 kg/cm².

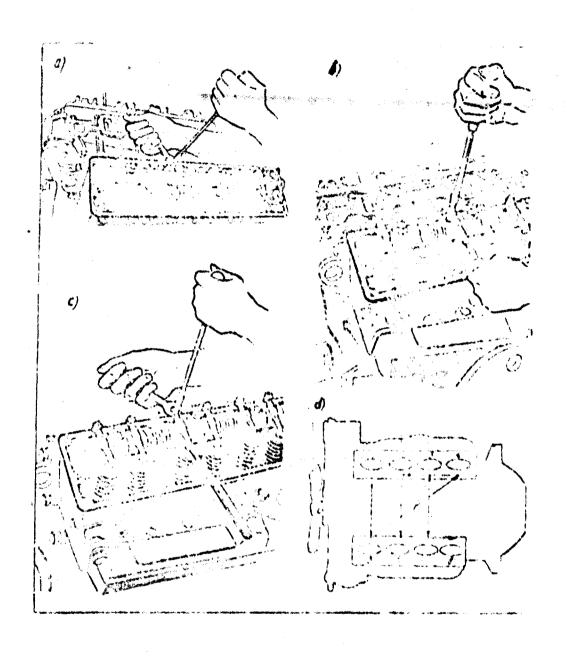


Plate 4-48. Valve edjustment:

a) loosening the stop out b) adjusting and checking clearance with a leaf gauge c) tightening the stop out and adjusting screw d) cylinder membering order (arrows indicate cylinder firing order)

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Comprossion decrease during eneration is allowable : 0.: g/cm2.

It is necessary to clean the plates of the coarse of aning filter daily, turning its handle by three to four revolutions. The filter should be cleaned with a completely warmed engine. Use of an extension lever to ease rotation of the filter handle is forbidden. If the filter handle turns with difficulty, it is necessary to unser-, the cover bolts, resove the filter, and wash it out in kerosene. For convenient access to the oil filter handle, an extension running along the filter axis is built into the ZIL-131.

Checking the proper operation of the partial flow centrifugal oil cleaning filter is done by sound. After stopping the engine, the filter will continue to work for 2-3 minutes, making its own peculiar sound during this operation. The absence of this sound indicates that the filter is not working. The filter is cleaned every TS-2, at the same time that the angine oil is changed. To clean the filter, it is necessary to: unscrew nut 10 (see Plate 4-32) and remove the jacket, then, having unscrewed plug 3, hold the jacket with a large punch inserted in the hole left by the plug, unscrew the nut, remove the filter cover, and clean diff deposits from it. A layer of deposits more than 8-10 mm thick must not be allowed on the filter cover. After cleaning, wash the filter and screen in gasoline or kerosene.

If the filter works poorly, it is necessary to remove the body from the shaft and clean the shaft, bushings, and nozzles. Before uncovering the filter, it is recommended that the oil be drained from it by unsurewing plug 17. This takes approximately 30 minutes after stopping the engine.

The full flow centrifugal oil cleaning filter is cleaned in the same way as is a partial flow filter. After cleaning and finishing assembly, check the operation of the filter on a warm engine by sound.

The crankcase ventilation air filter is serviced simultaneously with changing oil.

For servicing, the crankcase ventilation filter is disassabled, dirt is cleaned from it, and it is carefully washed in gasoline or kerosene.

After the crankcase ventilation filter is washed, free engine oil is poured on and the filter is assembled.

Before the water pump bearings are intricated, it is necessary to clean the dust and dirt off the area around the inbrication fitting and the centrol opening, and to unscrew the plug from the control opening.

Grease should be pressed in with a grease gan through the pressure labrication fitting until fresh grease appears from the control opening. After lubricating the bearings, the plug is installed in place.

Disascembly and assembly

Removing the power unit

To provide the best access to the motor vehicle's parts from below (during removal of the power unit), it is recommended that the motor vehicle be placed over an inspection pit, over which there is a hoist mechanism. The weight of the power unit in assembly without finid is 540 kg; therefore it is necessary to have a hoist mechanism with a load capacity of no less than 1 ton for its removal. Height to the hook must be no less than 2 meters.

Before removing the power unit from the motor vehicle, it is necessary to drain the veter from the cooling system and desirable to also drain the oil from the engine crankcase and the transmission. Water is drained through three drain cocks. During disassembly, it is recommended that small parts be placed in a saperate box, and when wires are disconnected from electrical equipment, scrows and nuts should be scrowed back into their places by hand.

Before removing the power unit, it is necessary to perform the following preparatory tasks. Remove the storage battery nest hatch cover and free the positive terminal of the battery, remove the starter 1 4, and, in the ZIL-131 mater vahicle, disconnect the ground with the switch.

Raise the engine hood and disconnect the leads from electrical equipment and the front terminal blocks, and remove the distributor cap and rotor.

Loosen the hose clamp screws and remove the water and oil radiator hoses. Remove the heater hoses and lines.

Disconnect the louvre cable and $p_{\rm s}$ it, together with its jacket, from the hole in the cab fire wall.

Free and remove the radiator jacket.

Unscrew the radiator fastening nuts, remove the radiator either by hand or with device KZ-Dab5 (Plate 4-49, 8), and remove the rubber cushions with their spacing bushing.

Disconnect the carburetor linkage and remove: the accelerator linkage, the manual throttle cable, and the manual choke cable.

Disconnect and ramove: the compressed air outlet line from the compressor; the pressure regulator line; and the fuel inlet line to the fuel pump.

Disconnect the high and low pressure horas from the hydraulic power steering pump body.

Disconnect the steering mechanism power inlet and remove the steering column universal shaft.

Driving off the stop rings and unscrowing the nuts, disconnect the exhaust collector pipe from the exhaust manifold.

Unscrewing the fastening bolts, remove the inspection cover in the floor of the cab.

Unscrewing the fastening bolts, remove the transmission shift lever housing with its gaskes in assembly with the shift lever.

Cover the hole in the transmission cover with a cardboard cover, fastening it down with two bolts.

Disconnect the speedometer drive, unscrewing the sleeve tensioning nut.

Disconnect the foot brake drive, removing the rod from the pedal lever.

Disconnect the drive for the manual trailer brakes.

Remove the handbrake lever from the transmission, unscrewing its fastening bolts.

Disconnect the universal shaft from the handbrake drum, unscrewing its fastoning nuts.

Disconnect the clutch drive, separating its drawbar and pedal lever.

On the ZIL-131, disconnect the universal shaft from the flange on the transmission output shaft.

Disconnect the transfer case drive and control lever.

If the motor vehicle has a winch, disconnect the universal shaft of the power take off box, and remove its cover and control lever.

Free the fastening bolts of the front mounts and two tear mounts of the engine, as well as the engine bracing rod.

Engage the hoist apparatus (Plate 4-49, a) in the brackets of the engine, and carefully raising it and moving it forward, remove the power unit from the motor vehicle.

Upon removing the power unit from the motor vehicle, install it on a special carriage (Plate 4-50,a) for its transportation to the disassembly point.

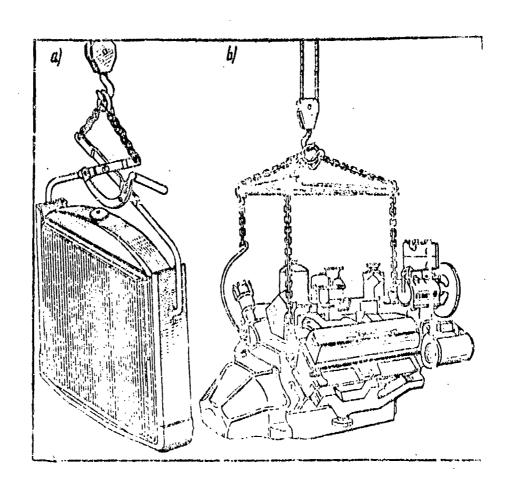


Plate 4-49. Devices for removal from motor vehicle of:

a) the radiator

b) the engine

Engine disassembly

Before disassembling the power unit, it is necessary to clean the dirt and oil from it, washing it in kerosene or with a degreasing solution. For drying, blow the engine off with compressed air.

It is expedient to conduct removal of the assemblies and parts mounted on the engine with the engine mounted on a GARO model 2473 stationary rotating stand, or on the stand shown in Plate 4-50, b. Rotation of the engine around the horizontal axis of the stand is accomplished with a worm mechanism installed on the stand. The engine may be held during disassembly or assembly in any position with a brake on the worm mechanism. During engine disassembly, run-in parts assembly surfaces which are usable for re-installation without

being exchanged should be protected from damage.

Parts of assemblies removed from the engine should be placed in a specially prepared box, in which they are again placed for assembly after washing, checking, and elimination of deficiencies.

The majority of engine parts are interchangeable (although many require individual fitting to their assembled parts) and allow their non-individualized exchange, with the exception of connecting rod caps and main bearing caps (the first are machined with the connecting rods in assembly, and the second are machined in assembly with the cylinder block). Connecting rods, with their caps in assembly, are stamped at the factory with numbers corresponding to the number of their cylinders, and main bearing caps are stamped with numbers corresponding to the main bearing order number.

Before installing the engine on the stand, the transmission must be removed from it. For this, the transmission and fastening bolts should be unscrewed with a box and wrench, the transmission disconnected from the clutch housing with the help of an assembly pry bar and, rocking it, it is removed with a block and tackle or hydraulic jack model 444 (see Plate 4-50,a).

Air filter removal. Disconnect the lines leading from the air filter to the compressor, remove the transfer cover with its sleeve, unscrew the compression nut and remove the air filter, and then remove the transfer flange.

Carburetor removal. Disconnect the fuel line running from the fine cleaning filter, the vacuum advance line, and the two lines running to the centrifugal switch, free the fastening nuts, and remove the carburetor and heat insulating gasket.

Remove the engine crankcase ventilation filter, unscrewing its fastening bolts.

The fine cleaning fuel filter. Disconnect the pipe from the fuel pump, unscrew the fastening nuts of the bracket, and remove the filter in assembly with the bracket and pipes.

Oil filters. Unscrew the oil pressure indicator switch from the filter ling. Disconnect the drain lines. Unscrew the filter body fastening bolts and remove the filter together with its packing gasket from the engine.

The distributor and distributor drive. In the Z1L-131 motor vehicle, remove the shielding hoses. In all motor vehicles, unscrew the cooling liquid temperature indicator switch. Unscrew the bolts fastening the distributor to the pump plate of the octane corrector and remove it.

For removal of the octane corrector plates, it is necessary to unscrew the bolts fastening the plate to the top flange of the distributor drive body.

For removel of the distributor drive, it is necessary to unscrew the bolts fastening the drive body to the cylinder block and pull the distributor drive in assembly with its body, sheft, and gear from the nest in the block.

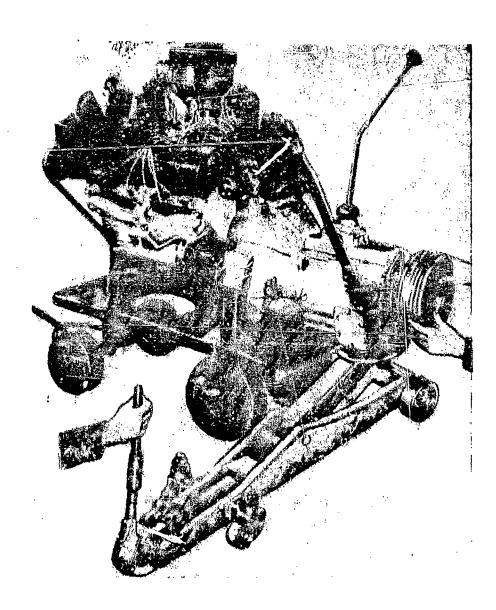


Plate 4-50. Engine installation for disassembly:

9) on a cert

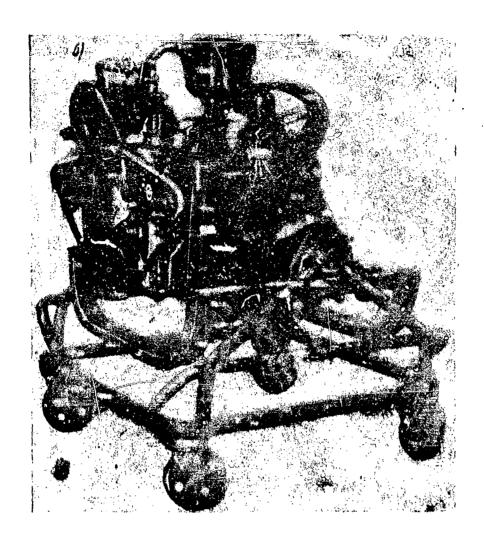


Plate 4-50 b. On a rotating stand

The starter. Unscrew the bolts fastening the starter to the clutch housing and pull the starter from its receptacle in the housing.

The generator. Unscrew the nuts fastening the generator tensioning arm. Unscrew the nuts fastening the generator to its bracket and, freeing the generator pulley from its drive belt, remove the generator and generator drive belt.

Unscrew the generator brackets from the engine, unscrewing their fastening bolts.

The hydraulic power steering pump. Unscrew the nuts fastening the tensioning bracket to the cylinder head, and, freeing the pump fully from its drive belt, remove the pump in assembly with the brackets and pump drive belt.

Remove the bracket from the pump, unscrewing its fastening bolts.

The fuel pump. Unscrew the pump fastening nuts and remove it together with its gasket.

The compressor. Unscrew the coupling nuts fastening the lines supplying cooling liquid to the compressor from the intake manifold and exhausting liquid from the compressor to the water pump, and remove the lines.

Unscrew the coupling nuts of the lines supplying oil to the compressor from the oil main line of the cylinder block and exhausting oil from the compressor to the engine crankcase, and remove these lines.

Unserew the bolts fastening the compressor to its bracket and, freeing the pulley from its drive belt, remove the compressor and compressor drive belt.

For removal of the bracket from the engine, it is necessary to unscrew the nuts fastening the bracket to the cylinder head.

The starting pre-heater. On motor vehicles equipped with starting pre-heaters, it is necessary to drain the fuel from the tank and disconnect: the electric leads from the preheater instruments; the air supply hose from the fan and from the boiler; the fuel line from the regulator and boiler; lines for cooling liquid from the engine and boiler.

Remove from the engine the funnel and pipe; fuel tank; preheater electric motor and fan; fuel feed regulator with its solemoid valve; unscrew the glow plug and remove the boiler with its funnel.

The centrifugal crankshaft revolutions givernor switch. Unscrew the coupling nuts fastening the lines connecting the switch to the carburetor and remove them. Unscrew the bolts fastening the centrifugal switch to the camshaft gear cover and remove the switch with its gasket.

The fan and water pump. Unscrew the bolts fastening the fan to its hub and remove the fan, drive belts, and pulleys. Unscrew the bolts fastening the water pump body to the base of the block and remove the pump with its gaskets.

The oil pump. Unscrew the bolts fastening the oil pump and remove the pump with its gaskets.

The cooling system upper pipe. Unscrew the nuts fastening the pipe to the intake manifold and remove the pipe in assembly with the thermostat and

pull the thermostat from the pipe.

The spark plugs. To protect the spark plugs from damage, unscrew them from their holes in the cylinder head. The holes are closed with plugs.

The exhaust manifolds. During removal of the exhaust manifolds, it is necessary to disconnect the spark plug protector plates, pull out the oil dipstick, and disconnect the control drive rods of the cooling system drain cocks.

Unscrew the nuts fastening the exhaust manifold and remove it with its gasket. If the gasket is burnt onto the cylinder head surface, it must be carefully separated with a screwdriver. The operation is repeated with the second exhaust manifold. During removal of the exhaust manifolds from the ZIL-131 engine, they must not be disassembled. When there is no necessity to remove the exhaust manifolds separately, they may be removed in assembly with the cylinder heads.

The intake manifold. Unscrew the nuts fastening the intake manifold to the cylinder heads with a socket wrench, and, lightly tapping it with a hammer, remove the manifold by hand. Remove the two gaskets and two rubber seals, carefully separating them from their contact surfaces. Unscrew the cooling liquid temperature indicator switch from its receptacle.

The tocker arm covers. Unscrew the nuts fastening the covers and remove them together with their gaskets.

The rocker arm shafts, push rods, and tappets. Unscrew the four bolts fastening the rocker arm shaft to each cylinder head with a socket wrench. Remove the shaft in assembly with the rocker arms and stands, withdraw the tappet pash rods, and pull the valve tappe from their nests in the cylinder block with a metal rod whose end is bent to a right angle.

For removal of the rocker arms and stands (see Plate 4-26), it is necessary to unpin one end of the shaft and remove from it: the first flat washer, spacing spring washer 3, the second flat washer 4, the first rocker arm, the rocker arm stand, the second rocker arm, the spacing spring, and then remove all the remaining rocker arms, stands, it spacing springs

The cylinder heads. Unscrew the cylinder head fastening bolts with an angle socket wrench and remove them. Remove the gaskets. If the gaskets are burned, it is necessary to carefully separate them with the screwdriver.

Removal of the engine oil pan, clutch housing cover, oil trap, and oil pump pickup. Rotate the engine on the stand by 90° and set it vertically with the clutch housing downward. Unscrew the bolts fastening the clutch housing shield and cover, and remove them. Unscrew the bolts fastening the oil pan with the socket wrench and remove it from the engine by hand. Remove the oil pan gasket, carefully separating it from the cylinder block surface with a screwdriver. Unscrew the bolts fastening the oil trap and remove it. Un-

screw the bolts fastening the oil pump pickup and remove it together with its gasket.

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The piston and connecting rod assembly. Unpin the connecting rod bolt nuts, unscrew the connecting rod nuts with a socket wrench, check the stamping on the caps and connecting rods, and if necessary mark them with a punch, and then remove the caps from the rods, tapping lightly on the caps with a hammer, and remove the connecting rod bolts.

Rotate the engine on the stand by 90°, drive the pistons out of the cylinders in order, install the connecting rod caps in their places and fasten them with their bolts and nuts, screwing them on by hand.

During removal of the piston and connecting rod assemblies, it is necessary, after having removed the connecting rod bolts, to remove the connecting rod caps in pairs (1 and 5, 2 and 6, 3 and 7, and 4 and 8), rotating the crankshaft during this process with a lever on the toothed crown of the flywheel.

The flywheel pulley and camshaft gear cover. Drive the lock washer away from the edge of the crank ratchet, unscrew the ratchet with a socket wranch, having locked the crankshaft with a wooden mandrel placed under a crank of the shaft.

For removal of the crankshaft pulley, a three-pronged puller is used (Plate 4-51). A model 2492 puller can be used. After removal of the pulley, drive out the key from the crankshaft slot.



Plate 4-51. Crankshaft pulley removal

For removal of the camshift gear cover, it is necessary to unscrew the cover fastening bolts with a socket wrench and remove it. lightly tapping it with a wooden mallet, and remove the cover gasker, care thy separating it from the cylinder block surface.

The crankshaft. Unscrew the main bearing cap fastening bolts with a socket wrench and remove them, check the cap stamping and mark the caps with a punch if necessary, then remove the caps together with the inserts, and the rear cap together with the rubber end with seals. Remove the oil deflector from the shaft.

Remove the crankshaft with the flywheel and clutch in assembly, using a block and tackle.

Remove the main bearing inserts, and lay them in numerical order. Remove the rear main bearing seal. Set the main bearing caps in place.

The camshaft. In order to remove the camshaft from the engine cylinder block, it is necessary to remove the rocker arm shaft with the rocker arms in assembly, pull out the push rods and tappets, remove the camshaft gear cover, unscrew the two bolts fastening the flange through the holes in the gear, (Plate 4-52), and pull out the camshaft.

In pulling out the shaft, it is recessary to pay particular attention to ensure that the tops of the lobes do not strike the camshaft bearings and damage their surfaces. The shaft is pulled out in assembly with the camshaft gear and flange.

The camshaft gear (Plate 4-53) may be fitted on the shaft with a maximum clearance of up to 0.008 mm, or with a maximum interference of 0.036 mm.

The diameter of the chaft where the gear fits on it is 30.015-30.036 mm. The gear 1 is prevented from turning on the shaft by key 10. Width of the shaft keyway is 5.954-5.990 mm. If the keyway is worn, its width is allowed to be increased to a dimension of 6.945-6.990 mm for installation of a repair dimension key.

For removal of the camshaft gear from the shaft, it is necessary to pull off the lock ring 6, unscrew the gear fastening nut 5, remove it and pull out shaft 2 with spring 11 of the centrifugal switch drive, and remove the washer.

Instail the camshaft on a press and press off the gear (Plate 4-54), then remove the support flange 7 (see Plate 4-53), and the spacing ring 8, from the gear.

Removal of the gear from the shaft may also be accomplished with the model 2491 puller (Plate 4-55, a), as shown in Plate 4-56, a, as can fitting the gear on the chaft (Plate 4-56, b).

The clutch housing is final machined in assembly with the cylinder block, as a result of which it is not interchangeable. Therefore, it should not be removed from the cylinder block unless necessary.

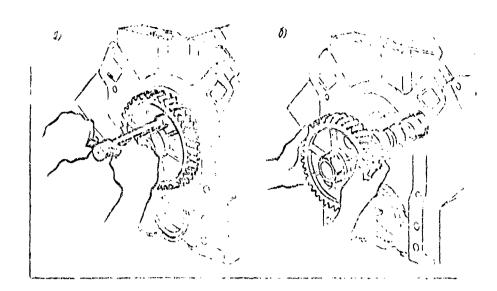


Plate 4-52. Camshaft removal.

- a) unscrewing camshaft fastening bolts
- b) removing the shaft

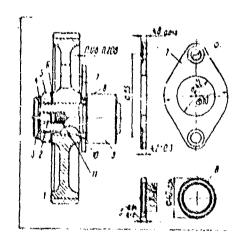


Plate d-SJ. Gear fastening on the camshaft:

- 1) gear 2) centrifugal switch drive shaft 3) stop ring
- 4) drive shaft washer 5) nut
- 6) lock washer 7) support flange 8) spacing ring 9) camshaft 10) key 11) drive
- shaft spring

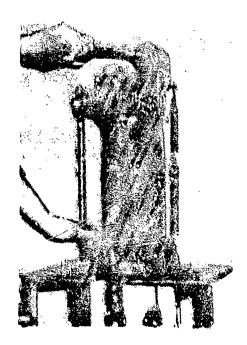


Plate 4-S4. Pressing the gear from the camshaft

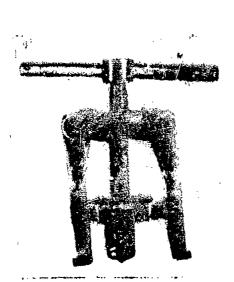
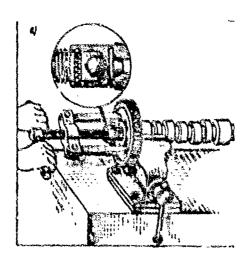
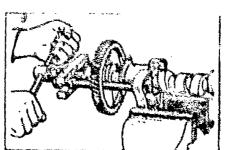




Plate 4-55. Pullers:
a) camshaft gear (model 2491) b) piston ring (model 2479)





Place 4-56. Pressing off and pressing on the camsheft gear:
a) pressing off b) pressing on

Remove the cylinder block with the clutch housing from the stand with a hoist, free the hoist from the compression brackets of the stand, and set the cylinder block on supports or a bench. Unscrew the bolts fastening the clutch housing the the cylinder block with a box end wrench, and remove the clutch housing in assembly with the disengagement fork and the clutch pedal lever.

For removal of the clutch disengagement fork from the housing, it is necessary to unscrew the lever tension bolt and remove the lever from the fork shaft. Unscrew the bolts fastening the flange with the bushing and pull the bushing with its flange and sell from its receptacle in the housing. Then, having freed the right end, and moving it in the bushing nest hole, remove the clutch disengagement fork.

Removal of scale from the cooling water jacket.

Scale in the cylinder block water jacket is removed mechanically or with a solution (20 grams of trilone per 1 liter of water).

In a case where there is no necessity to press out the sleeves but scale removal is required, the two face plugs on the rear part of the block and the side collars, together with the cooling system drain coeks, should be unscrewed for washing out the cylinder block couling jacket.

Disassembly and assembly of engine components.

The piston-connecting rod assombly. It is recommended that the connecting rod and piston be fastened into a vise for disassembly. Remove the piston rings (Pisto 4-57) with a model 2479 nuller (see Pisto 4-55, h), remove the piston wrist pin step rings with pliers, press out the wrist pin and disconnect the piston from the connecting rod. Check the condition of the connecting rod wastl and bushings, the wrist pin and the piston

During removal of an assombled oil ring, it is necessary to remove the circular disks with a device, and then sanually extract the spreader.

Before assembly of the connecting rod and piston, the connecting rod with 'vs inserts must be matched to the shaft journal, the piston matched to the ylinder sleeve, the rings matched to the piston groove, and the clearance in the butt joints to the cylinder. The wrist pin must be matched according to the connecting rod small end bushing, and the holes in the piston bosses.

Piston metching. All operations of metching the listons to the cylinder sleeves must be conducted at a temperature of 17-22°C.

When a piston is exchanged while the cylinder sleeves are and without regrinding. It is expedient to remove the upper edge (shoulder) of the sleeve

which is formed as a result of sleeve wear soove the level of the top piston ring with a scraper or small-grained abrasive wheel.

The pistons wust be matched according to the cylinders so that cluarance between the cylinder walls and the piston skirt is within the limits of 0.3-0.5 mm. The amount of clearance is determined the method of pulling through a band thickness gauge which is 0.08 mm thick, 10 mm wide, and no greater than 200 mm long.

The band thickness garge is pulled into the clearance between the piston and cylinder with a force of 3.5-4.5 kg (with the piston stationary).

It is recommended that piston matching take place with the piston turned head down, and the band used must be located on the side opposite the notices in the piston skirt. Pistons may be matched with sleaves without pressing the sleeves out of the cylinder block (Plate 4-58, a), or in sleeves which have been pressed from the cylinder block (Plate 4-58, b).

llaving matched the piston according to cylinder sleeves, it is necessary to stamp or paint (chall) the order number of their cylinders on the piston heads.

For assembly with the connecting rod, a piston is heated in a water bath or in an electrical heating apparatus (see Plate 5-55) to a temperature of 75°C.

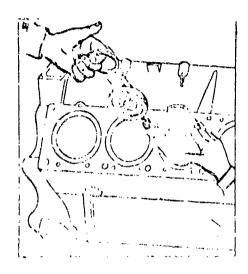


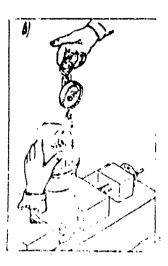
Fisto 4-57. Hemoval and installation of piston rings

Buring this, the wrist pin must enter in the boss hale of the warmed piston freely, under the force of a pen's thumb

with this assembly, after the pisson cools, the necessary interference within the limits of 0.0035-0.0078 ar .:11 appear

Check the order number of the piston and . anecting rod.





Flate 4-58. Matching pistons according to alcoves:

a) ustching piston to sleeve installed in the cylinder block
b) matching piston to sleeve pressed out of the cylinder block

The connecting rod is fastened in a vise, the piston is set on it and, inserting the wrist pin, it is assembled with a connecting rod.

During assembly with the connecting rod, the piston must be set so that the mark milled into the piston head is directed toward the front. The boss stamped on the connecting rod for the left group of cylinders must also be directed toward the front, i.e. toward the same side as the mark on the piston. For the right group of cylinders during piston assembly with the connecting rods, the connecting rod bosses must be directed toward the rear, and the mark of the piston heads toward the front.

With this assambly of the piston and connecting rods of the left group of cylinders, the oil slinging holes in the bottom ends of the connecting rods will be directed toward the side of the piston notches, and for the right group of cylinders, they will be directed toward the side opposite the piston notches.

After assembling and checking the piston and the connecting rod, it is necessary to install the stop rings in the piston bosses, fastening the wrist pins with this.

Then, carefully rub off the piston rings, matched according to grooves and fitted according to cylinders, and install them on the piston with the aid of a model 2479 device (see Plate 4-57).

The pistons' differences in assembled weight of units to be installed on one engine must not exceed 12 grams.

In this assembly, the connecting rods must of the same weight group.

Cleaning coke from piston ring grooves on a used piston is accomplished with a device shown in Plate 3-57. Coke must be cleaned exactly and carefully, so as not to damage the surface of the grooves.

Coke is cleaned from the oil outlet holes with a metal rod or a 3 mm drill.

In a case when the piston wrist pin is replaced with a pin of increased (repair) dimensions without replacing the piston, it is necessary to ream the hole in the piston bosses to a dimension providing the necessary interference (0.0025-0.0075 mm).

To maintain coaxiality of the holes, it is recommended that a reamer (Plate 4-59) with guiding tips be used. With this, the holes are reamed sequentially: first one, and then the other.

While reaming one of the holes, use the second for installation of the guide bushing. The reamer is equipped with a tail which is inserted into bushing 2. The exterior diameter of the bushing is in the form of a shallow cone.

The method of measuring clearance in the locks of new rings or their installation in the cylinder or in the control calibor is shown in Plates 3-59 and 3-60, and measurement of clearance in height between the ring and the piston groove is shown in Plate 3-61.

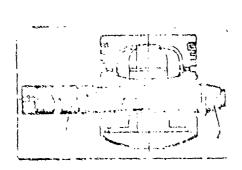


Plate 4-59. Reaming the wrist pin hole in a piston:

1) reamer 2) guiding bushing

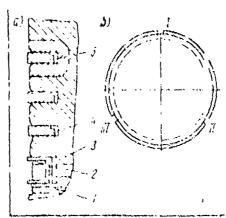


Plate 4-60. Piston ring installation:
a) location of the internal ring grooves in the piston grooves b) location of the ring butt joints on the piston
l) circular disk of assembled oil ring
l) acial spreader 3) radial spreader
4 and 5) compression rings

Clearance on a piston ring of corresponding dimension may be fitted in the lock with a fine toothed file. Pitting of the rings to the piston grooves should be done with fine-grained emery paper. The emery paper is laid on a flut plate and, lightly pressing, the ring is rubbed by hand. Rubbing continues until the required clearance between the ring and the groove is attained. A ring installed in the piston groove must move freely.

Increased clearance in the ring butt joint does not necessarily indicate reason for its discard. Usability of a piston ring can be determined by measuring the compression in the cylinders.

Operational experience of the ZIL-130 engine has shown a long piston ring life (up to 150,000-180,000 km of the motor vehicle's operation). Rings should not be changed unless necessary.

Premature exchange worsens the operation of the engine and increases wear on the cylinders. Ring installation should be done in accordance with Plate 4-60. Locate the compression ring butt joints around the circumference of the piston at 120° with an assembled oil ring. With installation of a cast iron oil ring, the ring butt joints should be located around the piston circumference through each 90°.

Ring flexibility in compression is checked with a flexible band instrument (see Plate 3-62). The compression force of the rop compression ring must not be less than 2.1 kg, that of the bottom compression ring, 2.3 kg, and oil (cast iron) ring, no less than 2.1 kg, and for the disks of an assembled oil ring, 0.48-0.53 kg.

The bottom end of the connecting rod is machined in assembly with its cap; therefore, during disassembly, checking, and assembly, the connecting rod and rod cap should be kept as a unit.

The connecting rod caps are centered according to ground surfaces on the rod bolts.

It is also not recommended that connecting rod units be changed among engines, since at the manufacturing plant, rods are selected and grouped according to weight. During selection and grouping of new rods, they should be selected according to the weight of one group. The rods are fitted according to weight by means of removing metal from the bosses on the cap and on the connecting rod end. Accuracy of selection according to weight of a group of rods for one engine is 16 grams.

Nonparallelners of the axes of the big end and little end holes of a connecting rod, sm. also deviation from a single plane (warping), is not allowed to be greater than 0.04 mm on a length of 100 mm.

The connecting rod in assembly is checked with a device (see Plate 3-63). The method of checking is described in Chapter 3.

Connecting rods having deviation from axial parallelness no greater than 0.08 mm and deviation in axial twisting of no greater than 0.08 mm on a length of 100 mm are admitted for correction.

The connecting rod may be corrected in a device (see Plate 3-63) or in a vise (see Plate 3-64) with a wrench or hand press.

The diameter of the connecting rod big and hale with the bolt nuts tightened must be within the limits of 69.500-69.512 mm (see Plate 4-15), and its nonellipticity must be no greater than 0.08 mm.

Connecting rods which go into repair with deviation in cylindrical form of their holes greater than 0.01 mm, or which do not fail within the limits of the indicated dimensions are discarded.

Repair of a connecting rod small end usually includes machining of the bushing for a repair dimension piston wrist pin (when the piston is capped) or exchange of the small end bushing and its consequent machining to a nominal dimension wrist pin (when a piston is exchanged). The connecting rod small end bushing is pressed into the hole with an interference of 0 147-0.200 cm, after which the hole for lubricating the wrist pin is drilled in it.

For the best contact of bushings newly pressed into connecting rod small end holes, and also for compacting the surface layer of the bushing metal, they should be previously subjected to drawing with a broach before reaming the hole, and the broach diameter must be 0.45-0.50 mm smaller than the final diameter of the hole for the wrist pin.

After drawing with a broach, the bushing is fitted with a reamer to the diameter of a nominal or repair dimension piston wrist pin.

Noncylindricality of the bushing hole is not allowed to be greater than 0.0035 mm.

Final machining of the hole for a piston wrist pin of any dimension (standard or repair) must be such that, at a temperature of $+20^{\circ}$ C, the piston wrist pin smoothly moves into the bushing hole with the effort of a man's thumb (see Plate 3-55). This fit corresponds to a clearance between the piston wrist pin and the bushing hole in the connecting rod within the limits of 0.0045-0.0095 mm.

For convenience in operation and repair, the factory produces a set of eight sleeves with pistons, rings, and wrist pins matched to them. This set bears the designation number 130-1000108.

The set, packed in a box, is shipped to requesters. For installation of a given set in an engine, it is necessary to remove the layer of preservative, and wash the parts in kerosene or gasoline. The pistons and rings are installed in those sleeves with which they came from the plant.

When sleeves are ground to repair dimensions, they are matched into similar groups, and used with repair dimension pistons and rings.

The crankshaft-flywheel-clutch assembly. The engine crankshaft is balanced in assembly with the flywheel and clutch. Allowable imbalance is not greater than 70 gram cm. Imbalance in the flywheel is eliminated by drilling holes 15 mm in diameter and no more than 25 mm deep on the internal side of the flywheel at a radius of 184 mm. Distance between the holes must be no less than 40 mm.

In the interest of maintaining the set (crenkshaft-flywheel-clutch), it is recommended that marks be placed on the assembled parts before the clutch is removed from the flywheel, and that they be used in reassembling the part so as to maintain its balance.

Removal of the clutch from the flywheel. Mark the relative position of the clutch cover on the flywheel, unscrew the clutch cover instending bolts with a socket wrench, remove the pressure plate in assembly with the clutch cover, and remove the driven disk in assembly.

Flywheel removal. Unpin the flywheel fastening nuts, unscrew them with an angle socket wrench (see Plate 3-65) and remove the flywheel. Drive the bolts out of the holes in the crankshaft flange.

If the front bearing of the transmission input shaft requires exchange, it should be pressed from the shaft with a puller (Plate 4-61, %) before removal of the flywheel, or, after flywheel removal, with a model 2476 puller, shown in Plate 4-61, c. After setting the clamps on the race faces of bearing 7, (Plats 4-61, b), they are spread by threaded support 3, and then the bearing is driven out by striking the slide against the support of shaft 5.

When crankshafts (see Plate 4-60) go in for repair, the deposits accumulated in their dirt collectors 3 should be cleaned out and oil coking products should be cleaned out of the passages. To clean out the dirt collectors, plugs 2 must be unscrewed.

The passages are cleaned with a wire brush.

The crankshaft must be checked for straightness.

The amount of bend in a crapkshaft must not exceed 0.05 mm.

If bend is present, the shaft may be corrected on a hand or hydraulic press. To check the crankshaft, it is necessary to set it with its extreme end journals on supports, and determine the amount of bend with an indicator.

If the shaft is not straight, it is corrected on the press until bend is eliminated, simultaneously checking shaft straightness with the indicator (see Plates 3-69 and 3-70).

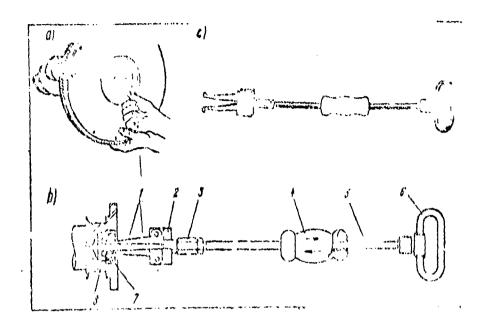


Plate 4-61. Pressing out the transmission input shaft bearing:
a) pressing the bearing out with a screw puller b) pressing
the bearing out with a slide hammer c) exterior view of the
model 2476 slide hammer 1) clamps 2) clamp retainer 3) support
4) slide 5) guiding shaft 6) handle 7) bearing 8) crankshaft

The gear is pressed from the shaft journal with a 1P-21305 puller, as shown in Plate 3-68.

Unit assembly. For assembly of the crankshaft, it is necessary to mount two support washers on the first main journal, insert the key in its slot, and press on the crankshaft gear.

Install the flywheel on the cranksheft flange, align the holes in the flywheel and flange, insert the bolts, scient the nuts on them, and tighten them with an angle socket wrench. Torquit is 14-15 kg mature.

Set the shaft with the flywheel on mounts (see Plate 5-71) and check escillation of the working surface of the flywheel with an indicator. Oscillation is allowed to be no greater than 0.10 mm. Place cotter keys in the flywheel fastening nuts. The sides of the pin on each bolt must lie tightly against the bolt face.

Grease the bearing receptacle in the flywheel flange with 1-13c grease and, with the aid of a mandrel, press the pilot bearing into it. Screw in

the lubrication fitting for greasing the bearing. Check the passage of grease from the lubrication fitting to the bearings.

Install the clutch driven disk and housing in assembly with the pressure plate on the flywheel and preliminarily fasten it with the bolts. Then, using the transmission input shaft or a mandrel in place of it, center the driven disk and final tighten the housing bolts. Torque moment is 2.0-3.0 k, meters.

During installation of the clutch on the flywheel, it is necessary to go by the marks placed during clutch disassembly, so that the crankshaft balancing with remain as before. If these conditions are not held to, it is necessary to balance the crankshaft in assembly with the flywheel and clutch.

Dynamic balancing takes place on a special machine. Allowable imbalance is 70 gram cm. Static balancing of the crankshaft in assembly may be done on balancing knives. A shaft, set on prisms, must not spontaneously rotate after it is stopped in any position.

Assembly and adjustment of the clutch and its halancing are presented in Chapter 6.

Balancing. In the process of operation and during regrinding of the shaft journals, or with repair or exchange of the clutch and its parts, imbalance of the crankshaft-flywheel-clutch assembly will increase. All these changes will lead to increased load on the bearings, increased vibration, and other undesirable phenomena, influencing long-vity and working ability of the engine in the most unfavorable manner after its repair.

Observations have shown that during the repair process, imbalance of the crankshaft-flywheel-clutch assembly increases to 1500 gram cm (allowable imbalance is 70 gram cm). The basic reasons for increased imbalance in the given assembly during engine major overhaul are: increased imbalance in the parts (crankshaft, flywheel, clutch disks), and also movement of the flywheel and clutch axes relative to the crankshaft axis. Therefore, during an engine's major everhaul, it is absolutely necessary that the crankshaft be dynamically balanced.

Basic equipment for crankshaft balancing is the model 2468 TsKB machine.

Crankshaft imbalance is eliminated by drilling holes in the journals of the end threws, and the assembly is balanced by drilling holes in the flywheel face.

The oil radiator. After removal from the motor vehicle, the oil radiator must be washed out with a degressing solution and hot water, then checked for tightness with air at a pressure of 4 kg/cm^2 in ϵ water bath. If a leak is discovered, it is eliminated by soldering the pipes with light solder. Small

noles in the radiator body are eliminated with welding and subsequent cleaning.

It is recommended that disassembly of the oil pump (see Plate 4-30) be conducted in the following order.

Wash the pump out in a degreasing solution and fasten it in a vise. Unscrew the three bolts 11 fastening the lower section body, remove the belts, remove the lower section body with its gasket, remove the lower section driven gear 12, and drive the shaft out of the body, lightly tapping it with a hammer. Unscrew plug 14 and remove the reduction valve (spring 17 and plunger 3). Press off the centering sleeve 4 on a bench press, remove the drive shaft 5 in assembly with the two drive gears 7 and 10, and with the intermediate cover 15, remove the gasket and upper section driven gear from the body and press out the driven shaft.

Fasten the pump shaft into a vise with soft inserts and remove the lower section drive gear from it, then extract the first key from the shaft keyway, remove lock ring 8 with a screwdriver, and remove the intermediate cover. Move the gear along the shaft and remove the second lock ring with a screwdriver. Press off the drive gear on a bench press and remove the second key from its keyway.

After disassembly, wash the pump parts and check their geometric dimensions.

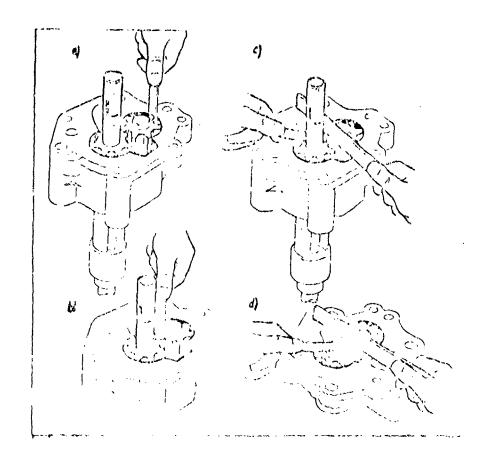
For checking tightness and appearance of leaks through invisible cracks, it is recommended that the oil pump body, intermediate cover, and lower section cover be checked with water under a pressure of 4 kg/cm².

Oil pump assembly takes place in a sequence opposite to that of disassembly. All paper gaskets must be replaced with new ones during assembly. Installation of the drive shaft in the pump body requires that a clearance of 0.030-0.078 mm be not taked between the shaft and holes in the body.

During installation of the drive gears, the clearance within the limits of 0.018-0.057 was must be maintained between the shaft and gear hole.

During pump assembly, special attention should be paid to the following. The driven gear shaft must be pressed into the body with an interference within the limits of 0.010-0.052 mm. The centering sleeve must be fitted onto the drive shaft with an interference within the limits of 0.004-0.048 mm. If the sleeve rocks (fits with a clearance) on the shaft, it should be replaced. When the centering sleeve is pressed on, the dimension from the pump shaft face to the upper end of the sleeve should be kept equal to 8 mm.

Clearance between the gear test and walls of the body receptable must be within the limits of 0.100-0.175 mm (Plate 4-62). Clearance in the gear test engagement must be within the limits of 0.140-0.240 mm. Clearance between the gear test faces and the intermediate cover must be within the limits of 0.120-0.195 mm, and between the gear faces and the lower section body, clearance must be within the limits of 0.135-0.188 mm.



Plats 4-6. Checking clearances in the oil pump:
a) between the body wall and gear b) in gear engagement
c) between the body surface and teeth faces d) between the

lower cover surface and teeth faces d) between the

The drive shaft of the pump, installed is the pump body, after tightening of the bolts must turn easily by hand without binding. Clearance between the pump goar faces and the cover is adjusted with inserts. If binding occurs, inserts must be added.

The assembled pump should be tested (Plate 4-63). Checking of pressure developed by the pump is done with petroleum based oil T (COST 1840-51) at an oil temperature of 18-70°C, outlet hole of 4.0 mm and loading nozzle length of 6.0 mm. Pressure at 450 rpm of the pump shaft must be no less than 2.4 kg/cm² fc. the upper section, and no less than 0.6 kg/cm² for the lower section.

The upper section reduction valve must open at a pressure of 2.75-3.3 kg/cm², and the lower section by-pass valve must open at a pressure of 1.2-1.5 kg/cm² with a corresponding increase in the number of pump shaft revolutions. The oil pump is driven through reductor 10 of the electric motor 11. The pump draws oil with a sucking action from tank 5 through pipe 6, whose end must be dropped into the tank to the minimum level. Pressure created by the oil pump is checked by manometers: manometer 12 for the upper section, and manometer 13 for the lower section, installed in pressure chambers 16 and 14, respectively. Oil flows from the pressure chambers through the loading nozzles 15 and then into the lower tank through pipe 20.

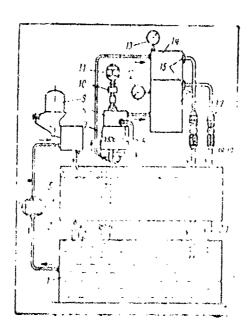


Plate 4-63. Stand for testing oil pump:

1) lower tank 2) drain pipe for maintainance of oil level in upper tank 3) pipe for draining oil into lower tank 4) pump 5) upper tank 6) pipe for oil feed from upper tank to pump 7) oil pump 8) transfer sleeve 9) contrifugal cil cleaning filter 10) reductor 11) electric motor 12) manometer for encoling oil pressure in pump upper section 13) manometer for checking oil pressure in pump lower section 14) pressure chamber for pump lower section 15) loading nozites 16) pressure chamber for pump upper section 17) valves 18) maximum oil level in tank 19) minimum oil level in tank 20) lines for oil flow from pressure chambers to lower tank

Oil is pumped from the lower tank by pump 4 and flows into filter 9, from which cleaned oil flows into the upper tank. To maintain the necessary oil level in the upper tank, drain pipe 2 is installed and excess oil flows through it into the lower tank.

Disessembly and assembly of the oil filters. For disassembly of the oil filter body, it is necessary to install it in a vise. Unscrew plug 3 (see Plate 4-32), insert a metal rod into the hole and brace the centrifugal oil cleaning filter body.

Removal of the coarse cleaning filter. Unscrew the four nuts fastening the filter cover and remove the plated filter 16 in assembly with the cover and gasket from the body.

Disassembly of the coarse cleaning filter element is done when the blades are damaged or heavily loaded with dirt.

Removal of the partial flow centrifugal oil cleaning filter. Unscrew nut 10 fastening the filter jacket and remove the jacket 5 and jacket packing ring 4. Unscrew the nut 11 fastening the filter, remove the spring and support washers, and then remove filter body 7 from 4haft 14.

In order to remove filter body 7 from the shaft, it is necessary to remove cover 8 while rotating nut 9. During rotation, nut 9 moves step ring 12 with it. The stop ring, moving to cover 8, raises it upward. With this, the cover, sliding along the packing ring 6, is separated from the filter body.

Remove the upper support washer of the ball bearing, remove the support washer of bearing 22 from shaft 14, and press off the oil deflecting screen 23. Drive off the lock washer with a screw driver, unscrew the filter shaft from the body, and remove the lock washer. Then, remove the filter body from the vise,

If nut 8 does not have to be replaced, ring 12 should not be removed and the nut should not be disconnected from cover 8. Remove the two screen filters 13 from the hollow side shaft of the body 7, remove packing ring 6 from the filter body base, and unscrew notates 2 from the lateral holes in the hollow filter body shaft with a screwdriver.

Filter assembly is done in the reverse requince. The parts must be carefully cleaned of dirt and washed. The rabber packing rings of the carefully cleaned of dirt and washed. The rabber packing rings of the carefully facket must not have signs of stretching or hardening, otherwise they should be replaced.

If the shaft bushings (lower and upper) are worn, they must be replaced with new ones. Bushings are present into the body with an interference of 0.145-0.200 mm. After pressing in the bushings, they must be eachined with a reason to a diameter equal to that of the shaft, asimpaining a clearance

between the shaft and bushing within the limits of 0.03-0.09 ma.

To assure coaxiality of the interior surfaces of the bushings, the must be machined by a resmer with a single installation.

Non-coaxiality of the diameters for the bushings must not exceed $0.015\ \mathrm{mm}$.

With a normally tightened shaft scal, the hendle of an assemble arso cleaning. Aller must easily rotate by hand. The torque moment mandle rotation must be no greater than 0.4 kg meters.

The coarse cleaning filter by-pass valve must open at an () pressure of 1 kg/cm².

An assembled oil liter must be checked with petrolous oil T (GOST 1840-51). With an oil pressure of 2.5 kg/cs² and temperature of $16-20^{\circ}$ C, rotation speed of the contribugal oil cleaning filter body must be no less than 5000 ppm.

Disassembly of the full flow centrifugal oil cleaning filter.

Disasterbly and assembly of the full flow filter is done in the same way as that of the partial flow filter, with the additional operations of removing the springs, insert 7 (see Plate 4-33), and screened filter 6.

Before assombly of the full flow filter, the parts are washed, cleaned, and checked. The assembled filter must be checked with petroleum oil T (GMT 1840-51) at an oil temperature of 18-20°C.

The body ! of an assembled filter must freely (by hand) rotage on its axis without interference or binding.

With oil feed into passage 22 at a pressure of 0.3 kg/cm², and with passage 0 closed, the filter body must begin turning.

With oil feed into passage 22 at a pressure of I kg/cm², and oil drainage from passages D and P through a nozzle 1.5 cm in diameter and 2 cm long, filter body rotation must be no less than 5000 rpm.

With oil feed into passage c at a pressure of 0.8 kg/cm² with passage 22 blocked, the happass valve must be closed, and with a pressure of 1 kg/cm², the valve must oven. In this, oil from passage 8 must flow into passage 8 in a constant stream.

Disassembly of the water pusp. For disassembly, it is necessary to clean oil and dirt from the pusp and wash it to a degressing contion. It is recommended that disassembly of a pump from a 211-130 engine be conducted in the following sequence.

Unscrew the bolks fastening the fan, remove the fan and pulley from its hub.

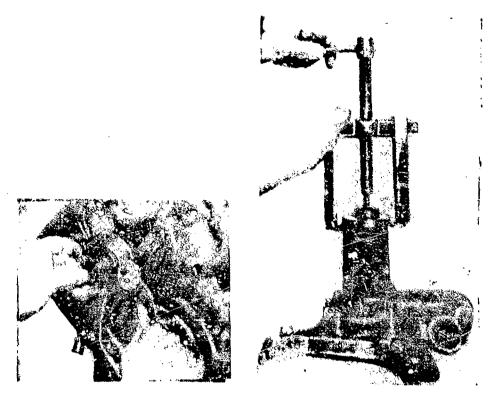


Plate 4-64. Pulley hub removal:

- a) with the bolts
- b) with the puller

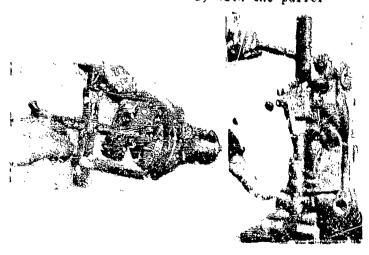


Plate 4-35. Removing and installing water pump parts:
a) removal of the impellor from the shaft b) pressing the shaft with bearings into the water pump body

Unpin the nut fastening the hub and preliminarily screen two bolts into the hub and hold it with a wedge, so that it cannot retate together with the shaft. Unscrew the nut and remove the hub from the shaft.

For removal of the hub, puller belts (Plate 4-64, a) or a special puller (Plate 4-64, b) should be used. Remove the split conic bushing with a screw-driver and drive out the key.

Unscrew the nuts fastening the bearing body to the pump body with a socket wrench and separate them, lightly tapping on them with a hammer. Remove the gasket, carefully separating it from the body with a screwariver.

Unscrew the bolt fastening the impeller of the water pump shaft, preventing shaft rotation with a screwdriver. Remove the impeller from the shaft with a puller (Plate 4-65).

To draw the packing from the impel)er receptacle, it is necessary to remove the packing in assembly and the textolite support washer with a screw-driver, and then separate the rubber cuff and spring.

Remove the front bearing lock ring with pliers (see Plate 3-76, a). Press the shaft in assembly with the bearings out of the body on a press. Unscrew the lubrication fitting and the control plug.

Faston the pump shaft in a vise and remove the stop ring and the water slinging washer. Press the bearings off the shaft, with the front and rear bearings being ressed simultaneously, and the spacing bushing located between the bearings of he reed.

Disastembly of the pump from the ZIL-133 engine should be conducted in the following sequence. Unscrew the bolts fastening the fan 21 (see Plate 4-42), and remove it from the pulley. Unpin nut 20, and, holding water pump pulley 23 by hand, unscrew it. Remove the fan pulley together with bearings 18 from shaft 14 of the pump by hand or with a puller. Remove the spacing ring from the shaft by hand, and then remove pump pulley 23 in assembly with its hub 16 with a puller. Remove the conic bushing 15. The pump pulley may be removed without its hub, after having unscrewed its fastening bolts. A pulley hub 16 may be removed with puller bolts (see Plate 4-64, a) or with a puller (see Plate 4-64, b). After this, the pump from the ZIL-131 engine is disassembled the same as is a pump from the ZIL-130 engine.

To remove bearings 18 (see Plate 4-42) from the hub hollow of the fan pulley 22, it is necessary to remove the stop ring, and then the bushings with the spacing ring 19.

Water pump assembly. Before assembly, wash out the pump parts, clean the rust off the pump and bearing bodies, and check usability of the parts. During pump assembly, it is necessary to check for face clearance between the impell r and the bearing and pump bodies.

Assembly of the pump from a ZIL-130 engine takes place in the following order.

Press the bearings on the shaft, having inserted the spacing bushing between them.

Mount the water slinging washer on the shaft and fasten it with a spring ring.

Insert the packing assembly and the textolite support washer in the impellor cavity, having lubricated their frontal surfaces with a thin layer of graphite lubricant and fasten them with a collar, pressing it on with a mandrel. Screw in the lubrication fitting and the control plug. Lubricate the bearing body with high-temperature grease lubricant 1-13c and press in the shaft with its bearings on a press (see Plate 4-65). Insert the front bearing support stop ring into its slot in the body, install the key in its keyway, mount the split conic bushing on the shaft, install the hub on the bushing, fasten it with a nut and flat washer, and pin it. The nut torque moment must be within the limits of 8.5-10.0 kg meters.

Install the impellor on the shaft, lightly tapping it with a hammer, and fasten it with a bolt and support washer.

Install the bearing body with its gasket on the pump body stude and fasten it with nuts.

If the stude are exchanged, it is recommended that they be coated with red lead or rubber pitch before being screwed into the body.

Mount the pulley and ran on the hub and fasten them reliably with bolts and spring washers.

Assembly of the water pump from a ZIL-131 engine is the same as that for a water pump of the ZIL-130 engine. Before installation of the fan pulley on the water pump shaft, it is necessary to insert bearings 18 (see Plate 4-42) and the spacing busning 19 into its hollow and fasten them with a stop ring, after which the pulley and bearings are fitted onto the nump shaft and fastened in assembly with the fan.

In connection with the introduction of an exhaust mainline into the engine design and interruption of the interchangeability in engine cooling system parts, the factory has produced a parts set under the number 130-1300053, intended for modernization of ZIL-130 and ZIL-131 engines which were produced earlier. The set includes the following parts: a water pump with plugs in assembly; an outlet pipe with thermostat in assembly; a by-pass hase from the pipe to the water pump; an outlet hose from the pipe to the radiator; an outlet hose spacing spring; an underwater hose from the radiator to the water pump; an underwater hose from the radiator to the water pump; an underwater hose spacing spring; a pipe gasket; #10 X 1 X 25 pipe fastening studs; M10 X 1 nuts; spring washers 10 mm in diameter; 16.2 mm

diameter washers; by-pass hose clamps; MS X 25 clamp scrow; and MS nuts.

In June 1965, a heat-treated pump shaft was introduced for water pumps of the ZIL-130 engine. The shaft has a threaded portion for the fan pulley fastening nut with a diameter of 14 mm (instead of 12 mm). The dimensions of the keyway for the fan pulley fastening key wate simultaneously changed and the hub was changed in correspondence with this. The new pump shafts can be installed in assembly with a fan hub, nut, washer, key, and conic bushings on ZIL-130 trucks produced before June 1965 as a parts set under the number 130-1307021.

Disassembly and assembly of the radiator with its jacket in assembly. For disassembly of the radiator and its removal from the motor vehicle, it is necessary to first disconnect the oil radiator, for which the following should be done: unscrew the fastening bolts to the water radiator suspension frame, loosen the two fastening screws of the oil radiator hoses, and remove the oil radiator in assembly with its brackets.

To disconnect the hoses from the pipes, it is necessary to loosen the tension screws with a screwdriver and remove the rubber hoses. For removal of the brackets from the oil radiator, it is necessary to unserew the nuts, did 3 the bolts out, and remove the two brackets from the oil radiator frame. In the ZIL-131 motor vehicle, besides this, it is necessary to disconnect and remove the oil radiator of the hydraulic power steering system.

To disconnect the suspension frame from the radiator, it is necessary to unscrew the bolts fastening the right and left radiator plates and disconnect the radiator from the frame suspension.

Thom, unscrew the nuts fastening the fan shroud to the right and left plates of the radiator, drive out the bolts, disconnect the fan shroud from the radiator and remove the radiator frame brace.

For removal or the louvres, it is necessary to unscrew the nuts fastening the louvres to the radiator plates, drive out the bolts, and disconnect the louvres from the radiator.

Before assembly, ic is necessary to clean dirt from the radiator and wash it out with a regular water nose. Water under pressure should be directed into the lower pipe of the radiator so that i. flows our of the upper pipe. The radiator cap must be closec. After the water flowing out of the radiator becomes clean, the washing out _ ross may be slopped.

The cleaned and washed-out ralistor must be checked for tightness by air under a pressure of 1.5 kg/cm² with the radiator placed in a water bath.

Assembly of the radiator parts is conducted in the reverse order.

Engine assembly

It is recommended that the engine be assembled on a GARO model 2473 stationary rotating stand, or on a stand such as the one shown in Plate 4-50, b.

The ZIL-131 engine is assembled with provisions for sealing all assembly surfaces. As packing, non-leaking pastes U-20s (TU 3512-54) and UN-25 (VTU 58khP 3336-52) are used.

before assembly, coat the following with a backing of non-leaking paste: the rear face of the cylinder bloc, the front face of the clutch housing (including the starter contact flange), the butt surfaces of the upper and lower parts of the clutch housing (including the groove for the gasket), the threads of the bolts fastening the lower part of the clutch housing and the threads in the cylinder block, gaskets, and also the starter flange. This coating is not necessary for the ZIL-130 engine.

The cylinder block goes into assembly pre-assembled with the clutch housing, and with a matched set of main bearing caps, camshaft bushings, cooling system valves, and lubrication system plugs. All oil passages in the cylinder block must be washed out and blown out with compressed air.

For cleaning the oil passages in the cylinder blocks, the end plugs of the longitudinal oil mainline and the tappet lubrication passages should be unscrewed. The cylinder block should be tested for tightness of its cooling system with water (under a pressure of 3-4 kg/cm²).

For testing the cylinder block, all connecting passages from the cylinder head assembly surface should be closed, the urain valve should be unscrewed from the cylinder block, till nipple with a water hose screwed into its threaded hole, and testing conducted.

The front and rear face surfaces of the cylinder block may have a non-flatness no greater than 0.1 mm. Non-flatness of the oil pan assembly surface is not allowed to be greater than 0.15 mm on its entire length or 0.04 mm on a length of 50 mm. Non-flatness of the assembly surfaces of the intake manifold and the cylinder head must not be greater than 0.15 mm on their entire length, or 0.04 mm on a length of 50 mm. Non-flatness is checked with a straightedge gauge and leaf gauges, laying the straightedge on the plane and measuring clearances between the straightedge and the plane with a gauge.

Before assembly, the front part of the cylinder block is fastened to the stand with supports, and the rear part is fastened with bolts and nuts, connecting the clutch housing supports to the stand.

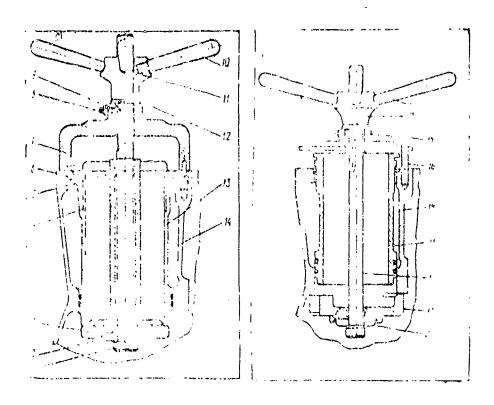


Plate 4-66. Model 2500 device for pressing out and pressing in cylinder sleeves:

- a) pressing out b) pressing in 1) rod 2 and 12) rod washers
- 3) sleeve support ring 4) rubber sleeve protector 5) drive busning 6) pins 7) puller body 8) stop screw 9) stop nut
- 10) handle, 11) working nut 13) sleeve 14) cylinder block
- 15) pressure plate 16) guide stud 17) cup

Cylinder sleeves are pressed out with the model 2500 device shown in Plate Plate 4-66, a. The sleeves are pressed in with the same device. The method of pressing is shown in Plate 4-66, b.

Sleeve installation. Mount the rubber packing rings on the sleeves, attempting not to tighten them excessively and watching so that the rings do not become twisted when they are laid into the circular grooves of the sleeve. The sleeves should be installed in the cylinder block carefully, not allowing the packing rings to be cut on the sharp edges of the boring and the block.

When the sleeves are pressed into the cylinder block, the upper part of the sleeve is self-sealed by pressure between the block and cylinder head on the sleeve shoulder. The lower part of the sleeve is sealed by rubber rings. The shoulder of a sleeve seated in its cavity must project above the upper surface of the block by 0.027-0.10 mm.

The clutch housing is installed on the cylinder block with two bushings which are pressed into the block face. When the clutch housing is changed, it is installed on installing bushings and fastened with bolts. The torque moment is 8-10 kg meters. Coaxiality of the holes, centering of the transmission with the crankshaft axis and perpendicularity of the rear face of the housing relative to the crankshaft axis are checked after installation of the crankshaft.

The clutch housing is checked with a IU-2376 device which is fastened on the crankzhaft flange (Plate 4-67). The amount of oscillation of the interior surface of the hole and the clutch housing face relative to the crankshaft axis must not exceed 0.1 mm.

The cylinder block is rotated on the stand so that the crankcase assembly surface is upward (Plate 4-68).

Crankshaft installation Remove the main bearing caps. Press the pin preventing the seal from rotating into the rear main bearing cap with its sharp end upward. Press the pin in with the mandrel, protecting its sharp end from damage. Rub down the insert beds in the cylinder block and caps with a soft cloth and blow out the cylinder block with compressed air. Insert the matched upper inserts into the main bearing beds in the block.

Insert the rear bearing seal into the slot in the cylinder block and into the slot in the cover (Plate 4-69), and then install the rubber face packing of the rear bearing cap into its receptacle.

Install the lower halves of the inserts into the main bearing beds. During this, it is necessary to carefully ensure that the upper and lower inserts are not confused, since the upper inserts have holes for oil feed to the main bearings and for oil supply to the camshaft bearings. If the inserts are incorrectly installed, the oil passages will be blocked and the bearings will work without lubrication, which will lead to immediate failure of the engine.

Take the crankshaft in assembly with the flywheel, clutch, camshaft gear, and support washers, set it in a convenient position with the aid of a device (see Plate 3-49), blow out the oil passages with compressed air, rub down the shaft main journals with a soft cloth, lubricate the surfaces of the top inserts with clean engine oil, and lay the crankshaft in the cylinder block bearings. Check the projecting ends of the rear bearing seal, and if necessary clean them. Lubricate the surfaces of the lower inserts and the

main journals of the shaft with oil. Install the main bearing caps in their places.

Insert the bolts and spring washers and screw them in at first by hand, and then tighten them with an angular socket wrench.

Check the main bearing bolt tightness with a torque wrench. The torque moments for the bolts on all the bearings must be 11-13 kg meters. After tightening the bolts, check the ease of crankshaft rotation. The moment of rotation must be no greater than 7 kg metals.

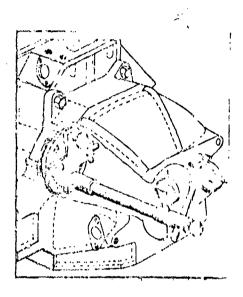


Plate 4-67. Checking coaxiality and perpendicularity of a clutch housing installed on the cylinder block

Thrust wasners. The front crankshaft bearing has thrust washers (Plate 4-60) on both sides for absorbing axis; loads arising during operation of the engine. These are made of bimetallic bands. Washer thickness is 2.46-2.50 mm. The washers installed on the shaft must be formed of antifiction alloy: the front one, on the side of the camshaft year, and the rear one on the side of the crankshaft.

If the axial clearance is the crankshaft shows in Piate 4-71 is increased to 0.4 mm as a result of thrust washer wear, they should be replaced.

Axial clearance between the front support journal of the crankshaft and the thrust washer is checked with the oil pan removed with a leaf gauge and lever. Moving the shaft forward and backward in the direction of the longi-

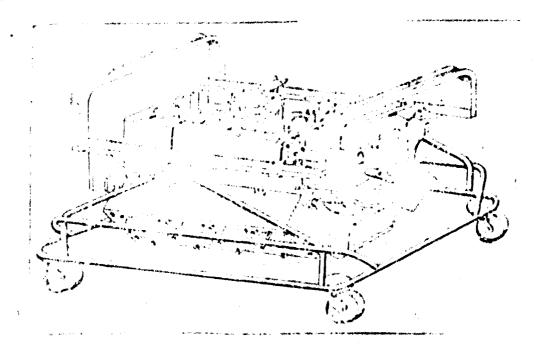


Plate 4-68. Stand with cylinder block

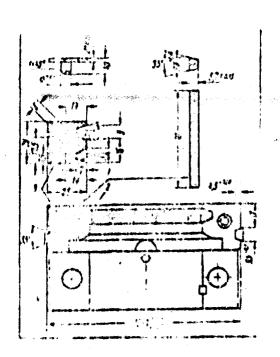


Plate 4-69. Packing the rear main hearing:
1) wooden packing 2) seal 3) rubber packing 4) cover

tudinal axis of the engine, clearance is measured and must be within the limits of $0.075-0.25~\rm mm$ in the first main hearing, and the clearance is free in the remaining bearings. The amount of clearance in the first main bearing is set by the thickness of the thrust washers. Axial clearance in the crankshaft may be checked without removing the engine from the motor vehicle (see Plate 4-74), for which it is necessary to remove the camshaft gent cover.

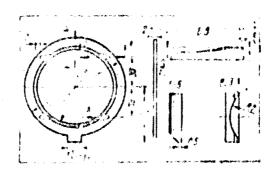
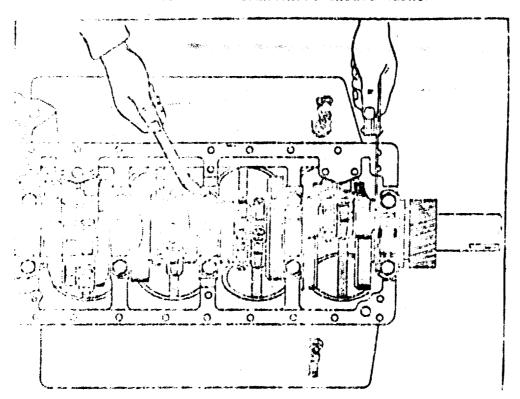


Plate 4-70. Crankshaft thrust washer



Place 4-71. Checking crankshaft axial clearance

Insert the wooden packing in the vertical slots of the rear main bearing cap and press them to the end with a hammer. Smooth the projecting face of the wooden packing off flush with the assembly surface of the bearing cap and the cylinder block.

Crankshaft supports and packing. Crankshaft main bearing caps are bored together with the cylinder block, and therefore they are not interchangeable. During boring, the caps are fastened with bolts. Torque moment is 11-13 kg meters.

The main bearing caps are centered in slots in the cylinder block along shoulders which are located nonsymmetrically, eliminating incorrect installation of the caps.

The nominal diameter of the main bearing insert beds is 79.506-79.525 mm. Non-coaxiality of the beds is not allowed to be greater than 0.02 mm.

The front crankshaft journal is packed with a rubber seal which has a metallic casing, and is installed in the camshaft goar cover.

The rear journal of the shaft is packed with seal 2 (see Plate 4-69), which is made of graphite-asbestos cord, and is installed in the groove formed in the cylinder block and cap 4 of the rear main bearing.

The seal is pressed in with a hammer and mandrel set on seal 2. The seal is also pressed into the slot in the bearing cap. Projecting ends of the seal are precisely cut off.

The rear bearing cap is packed along its lateral surface with wooden seals 1, which are installed in slots in the lateral surfaces of the rear cap. It is recommended that the wooden seals be replaced whenever the rear main bearing is disassembled. The seals must be manufactured of dry pine wood.

The rubber scale 3 are installed in the real part of the journal surface of the rear main cap. They should be replaced whenever necessary, or when the rubber is cut or stretched.

The flywheel is mounted on the crankshaft flange by six nonsymmetrically positioned bolts.

The nominal dimension of four of the holes is 14.000-14.035 mm (maximum allowable is 14.0° o mm), and that of the other two is 14.3 mm. It should be kept in mind that since October 1364, the flywheel fastening bolts have been lengthened by 4.5m, and their nuts have been increased in height by 5 mm.

There mus, he a clearance between the crankshaft journals and the hearing inserts of a new engine within the limits of 0.926-0.085 mm for main bearings

and 0.026-0.072 for connecting red bearings. When seel-aluminum inserts are used, this clearance must be 0.032-0.076 mm for connecting red bearings and 0.050-0.107 mm for main bearings.

Changing crankshaft bearing inserts. It is necessary to keep in mind that up to May 1966, the Jower inserts of the front and intermediate bearings did not have imprication passages. To improve lubrication, since May 1966, lubrication passages have been provided in these inserts.

To replace connecting rod inserts, it is necessary to remove the oil pan, its baffle, and oil pickup. Then, rotating the crankshaft, set the connecting rods at their extreme lower position with respect to the indicated order of connecting rods (1st and 5th; 2nd and 6th; 3rd and 7th; 4th and 8th).

Having set the crankshaft in the required position, it is necessary to: unpin and unscrew the connecting rod bolt nuts, remove the connecting rod cap, move the connecting rod end piston secount upward in the cylinder, pull the inserts from the rod and cap, rub the insert beds with a cloth and install the new inserts; rub the connecting rod journals of the crankshaft with a cloth, lubricated with oil (engine), pull the connecting rod to the journal, ser the cap in place so that the numbers on the cap and on the rod are on the same side, serew the nuts on to the connecting rod bolts, tighten them to a torque moment of 7.0-8.0 kg meters, and pin them. This same operation is conducted for the second connecting rod on the same journal of the shaft.

operations for changing the inserts of the next pair of connecting rods. For exchanging the main bearing inserts, it is necessary to unacres the bolts fastening the main bearing caps, remove the caps, and change the inserts.

When the inserts are exchanged without moving the crarkshaft from its bed, extractor 3 (see Plate 3-87) is used, easing the resoval of the insert upper halves.

for this, the following must be done: remove the hearing cap; set the crankshuft so that the oil passage hole in the main journal is uncovered; insert the extractor 3 in the oil passage hole; rotate the crankshaft until the extractor fingers rest against the face of the hearing and set its head parallel to the exposed exterior surface of the insert; rotate the crankshaft by 180° and extract the worn insert as shown in Plats 3-82.

The new insert is installed in the reverse sequence. The shaft journal must be carefully rubbed off with a soft cloth, and the insert must be lubricated with engine oil. After exchanging the inserts, install the covers in place, insert the bolts with their spring weaters, and tighten these. The torque moment must be 11-13 kg meters.

After the main bearings are tightened, the moment applied for rotation of the engine creakshaft must not be greater than 7 kg meters, and after tighten-

ing the main and connecting rod bearings, it must not be greater than 10 kg meters.

After exchanging the bearing inserts, it is necessary to set the oil pickup and oil pan baffle in place, having previously cleaned and washed them in kerosene, and checked the gasket and replaced it if necessary. Then, install and tighten the oil pan and fill the crankcase with fresh oil.

After any exchange of bearings (with shaft journal repair or without it), it is recommended that clearance be checked in each of the bearings, so as to ensure that repair of the shaft and selection of the repair inserts were dene properly.

whenever a craskshaft on an engine is replaced with a new one, it is necessary to simultaneously exchange all inserts. For this exchange, the factory puts out a set (130-1000107), a crankshaft with normal dimension connecting rod and main bearing inserts and thrust washers.

Installation of the pistons with connecting rods in the engine cylinders. For installation of the pistons with connecting rods, rotate the cylinder block, setting it on the stand vertically, front and upward, and insert the pistons in the cylinders correspondingly: 1st and 5th, 2nd and 6th, 3rd and 7th, and 4th and 8th, arranging the connecting rod bearings in pairs on their corresponding connecting rod journals of the crankshaft.

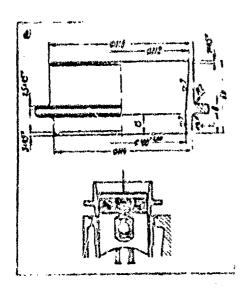
Sequentially, one after the other, take the piston with the connecting rod in assembly and corefully wipe down the belief for the insert in the connecting rod big end with a soft cloth, unscrew the nuts, and remove the rod cap.

During installation of the connecting rod with the piston, it is necessary to mount tin or copper tips on the connecting rod bolts, so as to protect the mirror finish of the cylinder sleeves from damage.

Check and blow out the holes in the lower end of the connecting rod which serve to splash lubrication on the cylinder walls, and install the inserts in the connecting rod and in the cap. Wipe off the upper coanecting rod inserts, pistons, cylinder sleeves, and connecting rod journals with a soft cloth. Lubricate the coarecting rod insert surface, piston, piston rings, and cylinder sleeves with clean engine oil.

Insert the pixton with the connecting rod in the cylinder, having directed the mark on the pixton head forward. Mount the device (Pixte 4-72, a) on the pixton from the skirt side, and compress the pixton rings. The rings must compress freely. Ouring installation of the pixton in the cylinder, the pixton rings may be compressed with the help of a model 7477 device (Plate 4:72,b). Moving the pixton along the cylinder with a wooden mandrel, bring the connecting rod bearing to the crankshaft journal. Lubricate the shari journal with oil, and pull the connecting rod big and to it. Remove the protective tips from

the connecting rod bolts, set the lower connecting rod cap in place, and fusten it with a connecting rod bolt, using a socket wrench.



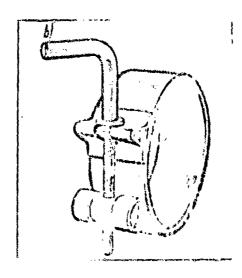


Plate 4-72. Device for installation of the piston with its rings in the cylinder:

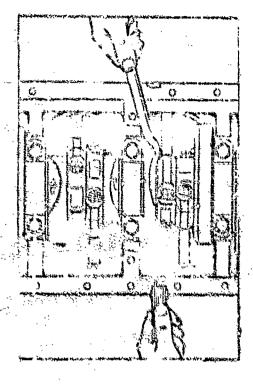
a) device in the form of a steel conic ring b) band device

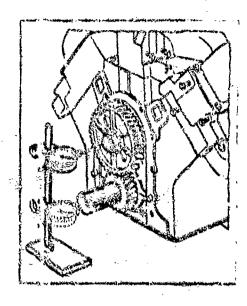
The same operations are conducted during installation of the remaining pixtons in the cylinders.

Check the total clearance between the faces of the connecting rod bearings and the faces of the crankshaft journal with a leaf gauge (Plate 4-73). Clearance must be 0.30-0.56 mm.

Final tightening of the connecting rod bolt nuts is done with a torque wreach. The torque moment on the nuts must be within the limits of 7.0-8.0 kg meters. Screwing on the nuts, it is necessary to bring their slots into alignment with the pinning holes. The nuts are brought to coincidence of their closest slots with the pinning holes in the bolts only in the direction of increased lightness.

After tigatening the main and connecting rod bearings, rotation of the cranschaft should be checked. The moment for shaft rotation with properly subjected radial clearances in the bearings must be no greater than 10 kg maters. Having finished checking connecting rod bearing tightness, it is necessary to pin the connecting rod bolt nuts, beading out both ends of the cotter key.





Place 4-73. Checking exist cleapance in connecting rod bearings

Place 4-74. Checking axial clearance of the crankshaft and cashaft with an indicator

Assambly of the camebatt includes installation if the spacing ring, support floage, key and gear.

Press the gear onto the shaft until 't rests against the specing ring. After pressing the gear on, install a luck washer, tighten the nut until it stops, and bend the lock washer onto one flat of the nut. During this, the support flange saist freely rotate, and clearance between the flange and the face of the support journal of the shaft must be 0.080-0.208 mm.

in the process of engine operation, the support flange also wears out. Increased axial clearance causes longitudinal movement of the shaft, and a knock in the engine. The amount of clearance may be decreased by using a smaller spacing ring by the amount of wear on the flange and face of the front shaft journal.

Axial creature in the cambuft may be checked without removing the engine from the motor vehicle or on a removed engine with an indicator (Plate 4-74), for which the cambuft gear cover is removed, the indicator is installed

against the face of the conshelt geer rin and axial elearance is checked, paying the shaft forward and bresward in an exial direction with a lever.

Cinerances between the cameltest journals and bushings must be within the limits of 0.030-0.095 km for the first four shaft journals, and 0.025-0.077 mm for the fifth shaft journal. In the process of operation, increased clearance may be allowed to 0.135 km for all bushings.

To set the clearance between the shaft journal and the bushing, it is necessary to massive the commonst journal with a micrometer, and measure the hole in the bushing which is installed in the cylinder block with an indicating plug gauge. Variation between the dimension of the shaft and the dimension of the bushing provides an emount of clearance which must be no greater than 0.135 mm.

In case of cameback bushing wear to more than the indicated limit, the bushings should be pressed out of their receptacles in the cylinder block with a model 2001 too set (Plate 4-75), and then now bushings pressed in with the same tools.

The method of pressing out bushings is shown in Place 4-76, a; the method of pressing them in is shown in Place 4-76, b.

When repair or new bushings are pressed in, they must be set so that the lubrication holes formed in the bushings precisely coincide with the holes in the cylinder block.

The pressed-in bushings must be fitted with a reamer to the diameter of the camehaft support journals, providing a clearance between the shaft journal and bushing within the limits of 0.03-0.09 mm.

During resming of the bushings, It is necessary to remember that the thickness of the antifriction layer in the bushing is small, and therefore a very small amount of non-concentricity in the bushing or increased thickness of shavings removed may lead to localized removal of the antifriction layer and to the operation of the crankshaft in steel.

After reaming of the bushings, it is necessary to carefully blow out the bearings and cylinder block with compressed air, removing all shavings, and once more to check the coincidence of the oil holes in the bushings with the passages in the cylinder block.

The plug of the rour camshaft support must seal tightly. Its installation with red lead or another scaler is allowable.

The characteristic deficiencies in the camenaft which arise in the process of work of the shaft are: its bending, and wear on the bearing journals, lobes, and keyways.

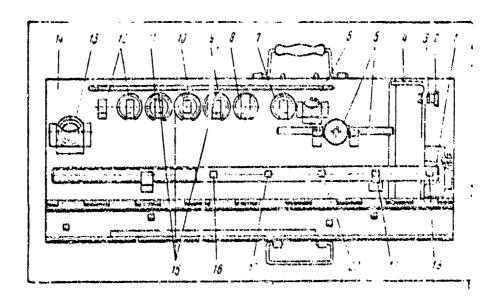


Plate 4-75. 'Tool set for repairing the camshaft seating location:

1) working screw 2) tension screw 3) set screw 4) bracket 5) nut handle 6) washer 7) mandrel for pressing out rear bushing 8) guiding mandrel 9) mandrel for pressing in front bashing 10) mandrel for pressing in middle bushings 11) mandrel for pressing in rear bushing 12) mandrel for pressing out front and middle bushings 13) centering bushing 14) storage box 15) pins 16, 17, 18, 19, and 20) slots

For checking straightness of the shaft, set it with its extreme supports on prisms; the shaft journals should be checked with an indicator (Plate 4-77). If oscillation of the middle journal exceeds 0.025 mm, the shaft must be corrected.

In connection with the fact that the diameter of the rear camshaft journal support is smaller than the other journals, it is necessary to make support 5 of the tool smaller in height.

Cam lobe wear in height must not exceed 0.65 mm. Wear on the fuel pump drive eccentric is not allowed to be greater than 0.80 mm. The nomina' dimension of the eccentric is 42.66-43.00 mm (see Plate 4-20, a). A camshaft on which lobes or the eccentric are worn above the allowable dimension must be exchanged.

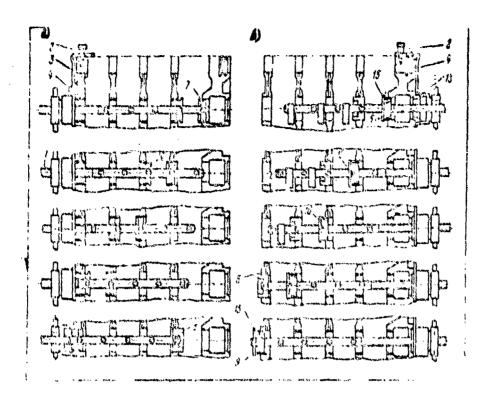


Plate 4-76. Pressing out and pressing in camshaft bushings with a model 2501 tool set:

(see caption to Plate 4-75 for numbers)

- a) pressing out
- b) pressing in

Smoothness of the lobe surfaces and sheft journals is assured by grinding. Oscillation of the front face of the first journal of a shaft is not allowed to be greater than 0.025 mm.

After regrinding the journals, it is recommended that shaft straightness be checked again. Non-cylindricality of the journals must be no greater than 0.02 mm.

Installation of the camshaft. Rotate the cylinder block to a horizontal position, setting the crankcase assembly surface upward. Wipe down the camshaft bearings in the cylinder block with a soft cloth, check colneidence of the oil passages, and lubricate the shaft journals and lobes with engine oil.

Install the camshaft with its gear, flange with a spacing ring and with the drive for the centrifugal revolutions governor switch in assembly, into the cylinder block. Installation is conducted carefully, without damaging the surfaces of the bearing bushings, lobes, and bearing journals of the shaft.

The camshaft and crankshaft goars are set so that the tooth which is marked by a dot on the crankshaft goar goes into the slot marked by a dot on the camshaft goar (Plate 4-78). Check the amount of clearance between the goar teeth with an indicator (Plate 4-79).

The clearance must be within the limits of 0.04-0.05 mm. The clearance should be checked in three places on the gear circumference at angles of 120° from each other.

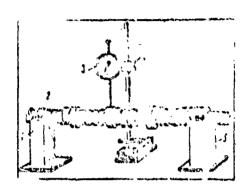


Plate 4-77. Checking the camshaft for bend:

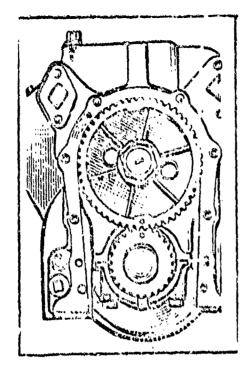
1 and 5) supports 2) shaft 3) indicator
4) indicator set screw

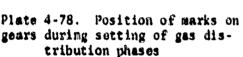
Having checked the clearance, it is necessary to align the holes in the support flange with the threaded holes in the cylinder block and fasten the camshaft flange with bolts and spring washers with a socket wrench (see Plate 4-52, a), directing it through the two holes in the gear. Torque moment on the bolts must be 2.0-3.0 kg meters. After tightening the bolts fastening the flange, axial clearance between the face of the shaft journal and the support flange must be no greater than 0.08-0.208 mm.

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Lubricate the camshaft gear, mount the oil deflector on the end of the camshaft, install the camshaft gear cover in assembly with its seel and gasket, and fasten the cover with bolts, installing the bracket for the engine suspension sion reaction rod beneath the bolt on the right side. Torque moment on the bolts is 2.0-3.0 kg meters.

Install the centrifugal switch for the engine revolution governor on the camshaft gear cover and tighten it, having installed the toothed indicator for setting the pistons at TDC beneath the two switch fastening bolts on the cover beforehand.





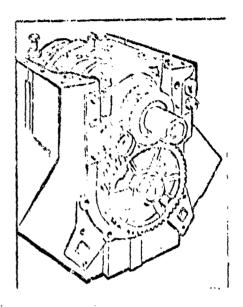


Plate 4-79. Checking clearance in the gas distribution gear teeth engagement

For installation of the crankshaft pulley, install the key in its slot on the shaft and press the pulley on with a mandrel, screw in the crank ratchet with its stop washer, tighten it with a wrench, and, having made sure that the ratchet is screwed in to its end, lock it with the washer by bending the washer's edge up against a flat on the crank ratchet.

Installation of the oil pan on a ZIL-130 engine. Install the baffle and fasten it with bolts, and install and fasten the oil pickup in assembly with bolts. Ensure that there are no foreign objects in the engine, and check to ensure that the oil pickup does not strike against the oil pan.

Lay the gasket on the cylinder block assembly surface, blow out the oil pan with compressed air, and install it on the cylinder block. Screw in the oil pan fastening bolts with spring washers by hand, and tighten them with a socket wrench. The bolts should be tightened sequentially from the middle of the oil pan toward the ends.

During installation of the oil par on a ZIL-ill engine crankow, he gasket should be glued to the oil pan to afford capability of foreing streams. In this, it is necessary to prevent glue from failing on the upper part of the gasket, which lies against the cylinder block assumbly surface.

Before installing the oil pan, it is necessary to greate the assembly surface of the engine crankcase and the gasket with UN-25 (VIU MKhP 3336-52) non-leaking packing paste.

Installation of the clutch housing cover and disengaging fork. Install the clutch disengaging fork in the housing and fasten the fork flange with bolts. Install the clutch housing cover and cover plate, and fasten them with bolts. Rotate the engine on the stand, setting the cylinders upward.

Assembly of the cylinder heads. For installation, carbon deposits should be cleaned from the combustion chambers with a metal brush or scraper.

Non-flatness of the surface of the head which lies against the cylinder block must not exceed 0.15 mm on its entire length, and 0.03 mm on a length of 50 mm. Non-flatness of the surface beneath the flanges of the exhaust and intake manifolds must not exceed 0.15 mm.

If the cylinder head surfaces are warped by amounts exceeding those cited, they should be milled or scraped. During milling, it is necessary to remember that compression chamber volume should not be decreased by more than 1.5 cm³.

Control of milling or scraping should be accomplished with a set of leaf gauges on the control plate or along a straightedge gauge.

The valves. For removal of the valves, it is necessary to set the cylinder head on a bench, and, compressing the springs with a model 2486 puller (Plate 4-80), remove the keys, remove the plate and spring, and then pull the valve out of the guiding bushings. Brackets are formed on the rear faces of the cylinder heads for lifting the engine. During cylinder head repair, these brackets need not be removed.

The cylinder heads are washed with a 1% solution of triethamolamine in water, or with pure hot water.

Scale in the cooling hollows of the cylinder heads is removed with the same solution as that in the cylinder block (20 grams of technical trilone per 1 liter of water).

The cylinder heads are checked for tightness with water or emulsion fed under a pressure of 3-4 kg/cm².

checked with the valves installed in the spark plugs, screwed in with water poured into the compression chamber with a measuring vessel.

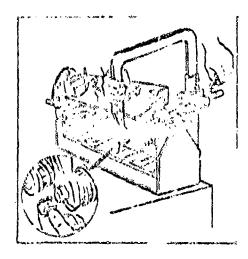
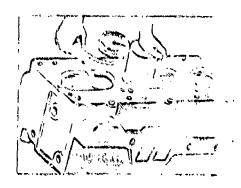


Plate 4-80. Valve romeval



Plat 4-81. Checking a valve for tightness

Valve tightness is renewed in the process of lapping the working faces of the valves and their seats. If pits or marks are present on the working face of the valve and cannot be removed by lapping, the face is subjected to grinding and subsequent lapping in its seat.

Rotation of the valve in the process of manual lapping is accomplished with a drill which rotates the valve laterally to the right and to the left. If the valve has a slot in its head, it is grasped by a mandrel which goes into this slot, and if there is no slot in the valve head, it is grapsed by a rubber suction cup.

During lapping, it is recommended that a low-elasticity spring be placed beneath the valve. To accelerate lapping, lapping paste or light emery powder mixed with engine oil is used.

The working face of the valve may be ground if the height of the cylindrical belt on the valve head exceeds 0.3 mm. Valves whose belt is smaller than 0.3 mm should be discarded.

The valve stem must be straight. The mominal diameter of the stem for an exhaust valve is 10.915-10.940 mm, and for an intake valve, it is 10.895-10.920 mm. Checking for straightness is conducted with an indicator on

prisms (see Plate 3-93, a). Valve stem curvature must not exceed 0.015 mm on a 100 mm length. Oscillation of the working surface of a valve face relative to the axis of the stem is checked on a device (see Plate 3-93, b).

The amount of oscillation wast not exceed 0.03 mm. The allowable wear of a valve stem dismeter without repair is: for an exhaust valve, 10.90 mm, and for an intake valve, 10.88 mm.

If wear on the stem exceeds 0.015 mm, the valve should be replaced. During repair, the valve stem diameter may be increased by 0.25 mm.

In a case where the working face of a valve is worked out (worn) or there are pits or marks on the face, the valve is subjected to grinding. Working faces of valves may be ground on a circular grinding machine by fastening the valve into a jaw chuck 3 (see Plate 5-92) or on a special table grinding machine model 2178. Machine construction allows installation of the valve at the required angle relative to the grinding wheel. The face of an exhaust valve is ground to an angle of 30° (relative to the horizontal axis), and that of an intake valve is ground to an angle of 45°. The grinding machine described above is also capable of grinding a valve stem face if it is worn.

Valves may be tested for tightness with a NIIAT instrument. For this, the instrument is tightly installed over the lappod-in valve, as shown in Plate 4-81, and air is pumped into the space in the cup with the squeeze bulb. If, during this process, the residual air pressure of 0.7 kg/cm² does not fall during the course of half a minute, the valve is lapped in correctly.

Valve contact tightness may also be checked by feeding air under the valve through the exhaust or intake passages of the cyclider head, which is analogous to checking the valves on an in-line engine (see Frate 3-95, b). Air is directed through a pipe with a rubber gasket which is pressed tightly against the passage. For determining the location of air leakage at a valve, kerosene or liquid oil is poured on. If the valve is not tight, air will leak from beneath the valve in the form of bubbles.

After lapping and checking the valves for tightness, the cylinder head and valves should be washed out and blown out with compressed air.

The valve guides. Maximum allowable wear on the valve guide holes must not exceed 0.05 mm. With a large increase in the bushings' diameter, they should be replaced. The valve guides are pressed our with a device (Plate 4-82, a).

When valve guides are pressed into holes in the cylinder head, it is necessary to mount a stop ring on the guide and press the guide in with a mandrel unbil the stop ring rests against the head (Plate 4-82, b).

We make pressing of the guides easier, it is recommended that the cylinder head be heated to a temperature of 180°C. If an installation for heating the head is not available, guide pressing without heating is allowable.



Plate 4-82. Replacing valve guides:

a) pressing guides out b) pressing guides in e) fitting guides with a reamer 1) puller body 2) support bearing

3) washer 4) pulling nut 5) shaft 6) support nut 7) cylinder head

After pressing the guides into the cylinder head, the dimension of the hole in the guide is brought to the diameter of the valve stem to be installed in it with a reamer (Plate 4-82, c), maintaining a warm clearance between the bushing and the stem which must be: 0.060-0.112 mm for an exhaust valve, and 0.080-0132 mm for an intake valve.

It is recommended that clearances within the valve guide be maintained within the described limits, since if the; are increased, heat dissipation is worsened, acting negatively on the longevity of the working face of the valve.

Valve guides should be replaced before correcting valve seats by grinding.

The valve seat. Wear of the seat face will lead to leaky valve seating, in which passing gases will form exidation and pits on the working surface of the face, and sometimes on the valve. Small deficiencies in the seat may be corrected by lapping the valve into the seat, and deep ones may be corrected by grinding (Plate 4-83), with consequent lapping of the valve against the working face of the seat.

Conic abrasives at an angle of 30° (relative to the horizontal axis) are used for exhaust valve seats and abrasives at a 45° angle are used for intake valve seats.

Valve seat working face repair is conducted by grinding with apecial abrasive stones, since steel millers are not as hard as the valve seat alloy. For exhaust valves, grinding is conducted in the following order: the working surface of the valve is preliminarily machined with a conic stone to an angle of 30°, as shown in Plate 4-83, b; then, the face at the lower part of the valve seat is removed by a miller at an angle of 75° (Plate 4-83, c), after which the face on the upper portion of the seat in removed at an angle of 15° (Plate 4-83, d); the working surface of the valve seat is then machined smooth with a fine grained conic wheel at an angle of 30° (Plate 4-83, c). These same operations are conducted for intake valve seats using the base cenic stone at an angle of 45°.

Before correcting the valve sust, the condition of the valve guides should be checked. If the latter must be replaced, this operation should be performed before the seats are corrected, since the base for machining the receptacle is the valve guide. Smooth milling ms: replace grinding with an abrasive stone and corresponding dressing of the stone (see Plate 3-98).

If width of the working face of the seat is greater than 1.4 mm for an intake valve, or greater than 1.1 mm for an exhaust valve, it is necessary to reduce the face by grinding the seat at angles of 75° and 15° (see Plate 4-83).

Having finished correction of the valve seat, it is necessary to check the accuracy of its machining with an indicator. Oscillation of the working surface of the valve relative to the axis of the valve guide hole is not allowed to be greater than 0.035 mm.

If the valve seats are worm too much to be corrected by grinding, they are pressed out of the cylinder head with a device (Plate 4-84), and new seats are pressed in.

Before pressing in the valve seat, the cylinder heads should be heated to a temperature of 180°C. The seats are pressed in with an under [Plate 4-85] until they rest against the bottom of their cavity. The valve seat is fitted with an interference of: 0.140-0.200 mm for exhaust valves, and 0.148-0.200 mm for jutake valves.

Seat faces are machined, achieving their coaxiality relative to the guide bushings, and then the valves are lapped into them.

After the valve seats have been repaired, the cylinder head is washed out and blown out with compressed air.

During installation of the valves in the cylinder head, the stem and valve guides should be libricated with a thin layer of oil.

Set the head on a bench and insert the valves. Install the valve rotation mechanisms on the intake valves (see Piate 4-24). For the exhaust valves, mount the spring support washers install the valve springs, mount the rubber cuffs on the exhaust valves, install the piates on the springs, and then, compressing the springs with the puller (see Plate 4-80), install the valve keys, fastening the valves with their springs into the cylinder head.

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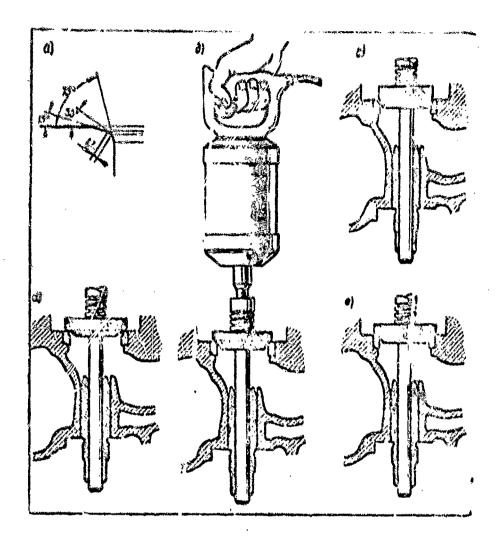
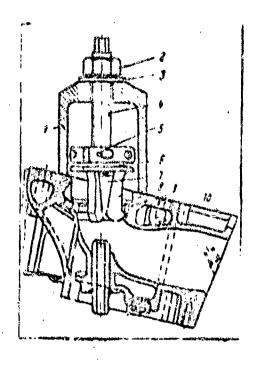


Plate 4-83. Correcting valve seat faces:
a) angles of machining and face dimensions b) coarse seat machining to an angle of 10° c) removal of seat face at an angle of 75° d) removal of the face at an angle of 15° e) fine machining of the seat at an angle of 30°

If the rocker are bushings are replaced, the oil passage hole depicted in Plate 4-25 must be drilled in them.

Wear on the rocker arm surface which contacts the valve stem may be eliminated by smoothing it with a hand file, but a radius of 10 mm curvature must be maintained.

Cylinder head installation. Check the upper part of the cylinders, making sure that there is no dirt in them, and if necessary wipe the pistons and the assembly surface of the block and blow them off with compressed air. The cylinder head gasket may be installed on the cylinder block on either side.



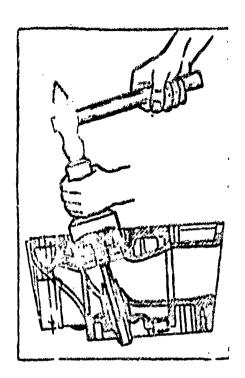


Plate 4-84. Pressing an inserted valve seat out of the cylinder head:
1) puller device body 2) nut
3) washer 4) screw with spreader cone 5) special nut with three fingers 6) tension spring 7) finger spreader cone 8) device finger
9) inserted seat 10) cylinder head

Plate 4-85. Pressing valve lest into cylinder head

Set the head on the pins on the cylinder block. Install the tappets into their receptacles in the cylinder block, lubricate them with clean oil, install the push rods, directing their upper ends into the holes in the head. Norm out tappets must be replaced or repaired.

Clearance between the wall of the guiding note and the tappet shaft must be within the limits of 0.008-0.045 mm.

A tappet which is correctly selected according to the dimension of its guiding hole in the cylinder block must freely fall into the hole under its own weight, for which the tappet must be lubricated with a thin layer of oil. Assemble the shaft, after having mounted the mocker arms and the spacing aprings, and placing the shaft stands as shown in Plate 4-26, and fasten the rocker arms with pins, inserting them into the holes in the end of the shaft.

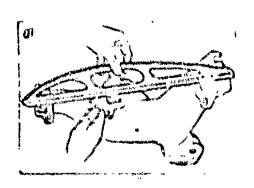
Install the shaft assembly on the cylinder head, connecting the tagget push rod ends with the rocker arms. Insert the bolts with flat washers into the holes in the rocker arm shaft stands, and preliminarily tighten them. Then, install the remaining bolts with flat washers and, having connected the spark plug protective shields and drain gutters, tighten the cylinder head. Torque moment on the bolts is 7-9 kg maturs. Bolt tightening order is shown in Plate 4-46. Bolt tightness is checked with a torque wrench. All the installation operations are repeated on the second cylinder head. The cylinder head bolts are tight ened on a cold engine.

There must be no nicks or dents on the assembly surfaces of the intake manifold with the heads and cylinder block, and if they are present, they must be smoothed off with a fine grained file or scraper. The surface must be clean, smooth, and free from traces of corrosion.

Warping of the centact surfaces is chacked with a straightedge gauge and a set of leaf gauges. Non-flatness of the surface is not allowed to be greater than 0.10 mm. If surface non-flatness exceeds the limits specified, the manifold should be replaced.

The manifold must also be checked for tightness under a pressure of 3-4 kg/cm². Before checking, it is necessary to clean tar deposits from passage 9 (see Plate 4-27) and scale from passage 3. Scale is separated with the solution used for cleaning the hollows in the cylinder block water jacket.

The surfaces of the intake manifold flanges must be straight. Haximum deviation must not exceed 0.2 mm. Straightness is checked with a straightedge gauge and leaf gauge (Plate 4-56).



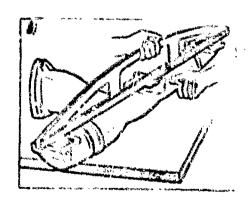


Plate 4-86. Checking the intake manifold:

a) IIL-130 engine
b) IIL-131 engine

The presence of small cracks on the interior portion of the manifold woes not necessarily mean that it is refined.

During respair, the walls of the manifold chroid be checked, and deposits formed on them should be cleaned off, since a significant amount of deposits noticeably constricts the passage section in the manifold, decreasing the power of the angine and lewering its fuel economy. The manifold is cleaned with a metal acraper or wire brush with subsequent washing in kerosene and blowing out with compressed 2.2.

Intake manifold installation. Install the cil trap on the interior side of the intake manifold on the two pins, and fasten it with nuts. Screw the crankcase ventilation valve assembly into its recoptacte on the exterior side of the manifold, screw the sleeve into the outlet passage of the manifold, install the pipe for exhaust of worked-out gases on the sleeve and fasten it with nuts. For the LiL-131 engine, the crankcase ventilation valve must be in assembly with a shut-off velve. Screw the water temperature switch into its faceptacle. Then, lay the packing gaskets on the assembly surfaces of the cylinder block and cylinder heads, install the intake manifold on the cylinder block studs; and fasten it with nuts. The turque moment on the nuts must be 1.5-1.0 kg maters. The nuts should be tightened evenly and sequentially (from the center to the edges).

Installation of exhaust manifolds on the FIL-130 ongine. Install the exhaust manifold with its gasket and fasten it on the stude with nuts and flat washers. Repeat the same operation on the other manifold. Torque moment on the nuts must be within the limits of 4.0-5.0 kg meters.

Simultaneously with installation of the left manifold, fasten on the starter shield, and install the dipatick tube, which is fartened with a nut on the slower in the hole between the cylinder head and the manifold.

Before installation of the chaust manifolds on the IIL-131 engine, they want be assembled. The exhaust manifold is assembled on a device which must provide positioning of the exhaust manifold flanges in a single plane, and typer location of the manifold holes to an accuracy of 0.25 mm. The butt of the gasket must be located beneath the tension bolt on the class. The classes are installed with tension bolts from beneath. The axes of the bolts must be perpositicular to the flanges fastening the manifolds to the cylinder head. After manifold and fasten it with note and flat weshers. Torque sement on the flanges fastening the manifold is 4-5 kg meters for the expect of flanges and 1-3.5 kg exters for the end flanges.

efter installation of the exhaust monifolds on the engine, check the class bolt rightness. Torque money must be 1.4-1.7 kg majors.

Consider the same operation on the other madifica-

The exhaust exaifolds may be installed in assembly with the cylinder heads, after they have been installed on the cylinder heads.

Installation of the oil filters. Install the oil filters with their gaskets, connect the drain passage and fasten the filter body with bolts and serew the oil pressure indicator switch into the filter body.

Installation of the oil filler pipe with the crankcase ventilation filter. Install the filter with the oil filler pipe, having previously laid down the gasket and installed the fuel pump rod, and fasten them with bolts and washers. If the engine has a straight flow of hot water from the cylinder head cooling jacket hollow into the pump hollow, install an additional pipe and thermostat and connect its hose to the water pump. Install the upper pipe and fasten it.

Installation of the water pump and fam. Install the water pump with its gasket, having previously mounted the drive belts of the compressor, the hydraulic power steering pump, and the generator on the pullay. Fasten the water pump in assembly with the fan on the engine with boits (or the ZIL-151 magine, the generator drive belt is also the drive belt for the fan).

Install the valve operation levers and fasten them with pins.

Fiel pump installation. Install the fuel pump on its study after installation of its gasket, and fasten the pump with auts and washers.

Installation of the carburetor and air filter. After laying its gasket, install the carburetor on study which are screwed into the intake manifold and fasten it with nuts. Install the tune gipes and fasten their ends on nipples in the carburetor and centrifugal switch with the coupling nuts. Connect the regulator vacuum line to the nipple on the carburetor (only on the ZIL-130 engine). Fasten the transfer flange on the carburetor, install the air filter body with its filtering element on the carburetor, and fasten it with a nut, and then install the transfer cover with its sleeve and fasten it with a bing nut.

On the ZIL-131 engine, the mir filter is installed on two studs which are screwed into the intake manifold. The filter is connected to the carburator by a rubber hose.

Installation of the fine cleaning fuel filter. Install the filter in assembly with its bracket on the intake manifold body and fasten it with nuts and washers. Connect the filter tubes to the fuel pump, and fasten their coupling nuts.

Installation of the hydraulic power steering pump. After fitting its drive belt on the pulley, install the pump in assembly with its bracket on study which are acrowed into the face of the cylinder block, and fasten it with nuts and washers. Simultaneously, adjust the tension on the drive belt, as shown in the description of the engine's technical service.

Compressor installation. Install the compressor on study which are screwed into the face of the right cylinder head, simultaneously fitting its drive belt on the pulley, and then fasten the compressor with nuts and washers. Adjust the drive belt consion as shown in the origine's technical service.

Connect the compressor cooling system lines and fasten them on their nipples with the coupling nuts, connect the compressor lubrication system lines and fasten their coupling nuts.

Connect the compressor to the air filter with the air outlet line and fasten it.

Generator installation. Install the generator brackets on the body of the compressor cover, and fasten them with bolts and washers. After mounting its drive belt on the pulley, install the generator on the brackets. Then, align the holes in the generator cover and brackets, insert the bolts, and fasten them with nuts and washors.

Adjust the tension on the drive belt, and fasten the generator tensioning arm with a nut as shown in the description of the engine's technical service.

Correct installation. After connecting the starter gear with the toothed ring of the flywheel, install the starter in its receptable in the clutch housing, and, holding it by hand, tighten its bolts.

Installation of the distributor drive. Before installing the distributor drive in its receptacle in the cylinder block, it is necessary to lubricate the drive geor and shaft with engine oil.

On an installation which has been disassembled and assembled, the distributor drive should be installed in the following sequence. Set the number 1 piston at TDC, as shown in the description of the engine's technical service.

Position slot 11 (Plate 4-87) of shaft 12 on the drive in the body so that it is parallel to mark 14, which is formed on the top flange 9 on the drive body, and its movement is directed toward the distributor gear cover.

In this position, install the distributor drive assembly into its receptacle in the cylinder block. During this, ensure that the holes in the lower flange 6 of the drive body coincide with the holes in the block at the moment of initial engagement of gear 13 on the drive and the distributor shaft gear, after which slot 11 of the distributor drive shaft, set in place, must be located parallel to the axis connecting the holes on the upper flange 9. In this position, fasten the distributor drive body onto the cylinder block 7 with bolts 5. If the distributor drive does not seat to its end during installation because of misalignment of the drive shaft top with the oil pump driving shaft slot, it is necessary to rotate the engine crankshaft by two revolutions, simultaneously pressing lightly on the distributor drive body.

Set the engine crankshaft with the starting crank so that the mark on the crankshaft pulley is located opposite the mark 9 on the ignition setting indicator at the end of the second crankshaft revolution (Plate 4-47). Rotation of the crankshaft by an amount of a 90° angle setting (on the indicator mark 9) allows setting of the earliest angle of ignition advance, providing easy engine starting.

Installation of the distributor, spark plugs, and high tension leads. Before installing the distributor, it is necessary to check, and if necessary adjust, the chearance between the contact breaker points and also align the indicator arrow on the upper place to the zero mark on the lower place of the octane corrector.

Install the ignition distributor in essembly with the octane corrector plates on flange 9 (see Plate 4-87) of the drive body, so that the vacuum regulator is directed toward the side of the carburstor, and the rotor electrode is located opposite the pole for the first cylinder. In this position, fasten the octane corrector plates with two bolts 10, thereby fastening the distributor. Connect the line to the vacuum regulator nipple and fasten it.

During installation of the spark plugs and high tension leads, blow out the depressions in the cylinder block for the plugs with compressed air, pull the plugs from the holes, and screw in the spark plugs.

While screwing the spark plugs into holes whose access is not fully free, a wrench must be used to ease correct guidance of the threaded portion of the plug. For this, the spark plug is inserted in the wrench and fastened in it with a small wooden wedge. Torque moment on the spark plugs is 3.2-3.8 kg meters.

Install the high tension leads, connecting their ends to the spark plugs and to the holes in the distributor cap. On the ZIL-131 $\exp_{\epsilon}^{i}(z)$, fasten the shielding hoses of the spark plugs.

Installation of the high tension leads must be conducted in correspondence with the cylinder firing order (1-5-4-2-6-3-7-8), considering that the distributor rotor rotates in a clockwise direction.

The ignition setting is checked (with the storage hattery connected) by a small rotation of the distributor, causing a spark in the number 1 cylinder. The checking order is the following.

Loosen boit 8 fastening the upper plate of the octane corrector to the distributor body to provide rotation of the latter by hand. If rotation is affected by the adjusting nut 3 of the octane corrector, then the bolt fastening the upper plate must not be loosened, or else rotation of the distributor body will not occur.

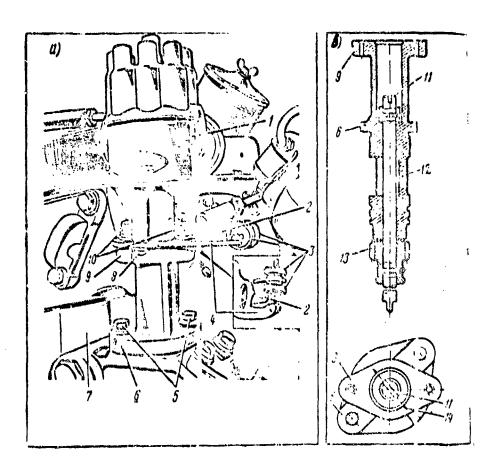


Plate 4-87. Installation of the distributor on a ZIL-130 engine:

a) distributor installed on the engine b) drive of distributor and oil pump 1) distributor 2) octane corrector lower plate 3) adjusting nut 4) became corrector upper plate 5, 8, and 10) bolts 6) lower flange 7) cylinder block 9) upper flange 11) drive shaft slot 12) drive shaft 13) drive shaft gear 14) mark on flange

Switch on the ignition and rotate the distributor body in a countercleckwise direction to the position where the contact breaker points begin to open and a spark appears between the ends of the central lead and the enging ground in an air clearance of 2-3 mm for a non-transistorized ignition system, and 3-10 mm for a transistorized ignition system. In this position, tightly fasten bolt 8, fastening the upper plate of the octane corrector to the distributor, thereby fastening it on the drive body. The beginning of contact point opening may also be checked by the lighting of a lamp connected to the engine ground and to the low tension pole of the distributor.

Installation of the transmission. Set the transmission on a hydraulic hoist cart 444 (see Plate 4-50, a) and move it to the engine. Raise it to the necessary height, connect it to the clutch housing, and fasten it with bolts, using an angular socket wrench until the bolts refuse to turn further. Having finished assembly, it is necessary to conduct running-in and testing of the engine.

Running the engine in

Plate 4-88 shows a stand with electric brake for running in and testing a V-shaped engine.

During old running-in of the engine, the electric motor works as a motor and requires alternating electric current from the network. During hot rolling of an engine being tested, the electric motor works as a generator, transmitting electric current into the network. Current transmission in this process vasses through electric rheostat 15, whose control is effected with handle 16 of the drive. The electric motor is started and stopped with buttons 17. The generator stator is connected with a weighing mechanism. The weighing mechanism of the electric motor is located in the body of the device control panel 24.

The electric motor is connected with the tested engine by a Cardan drive which is covered by protective grating 13. Control of the carburetor throttle is effected by rod 26.

Before testing, the engine is filled with oil corresponding to the lubrication chart, and also 15-20 grams of oil are poured into each cylinder through the spark plug holes. The engine is installed on the stand and fastened with a Cardan shaft of the stand fastened to the flange of the transmission, and the engine connected to the cooling system and the fuel system (on gasoline or gas). The protective grating is installed.

Engine running-in is conducted with the transmission in high gear. Engine crankshaft revolutions are increased by a smooth opening of the throttle.

During the running-in process, the engine is listened to, and the absence of extraneous knocks, leaks, localized overheating, or other deficiencies is assured.

Running in and testing the V-shaped engine after repair should be conducted according to the rate shown in Table 4-1.

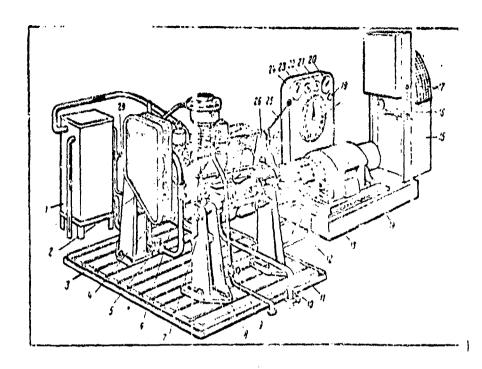


Plate 4-88. Stand for rolling and testing engines (ZIL-130 and ZIL-131):

1) tank with cooling liquid 2) engine 3) stand base 4) pulley protective screen 5) cooling system shut-off valve 6) front engine mount fastening nut 7) liquid fuel shut-off valve 8) stand upright fastening nut 9) gas fuel shut-off valve 10) exhaust pipe fastening bolt 11) stand upright 12) rear motor mount fastening bolt 13) Cardan shaft protective grating 14) electric motor 15; liquid rheostst 16) rheostat control handle 17) electric motor control buttons 18) scale dial 19) indicator lamp 2:) tachometer 21) oil thermometer 22) water thermometer 23) engine oil pressure gauge 24) panel body 25) transmission lever 25) throttle control rod 27) hand brake lever 28) clutch pedal 29) water line shut-off valve

After running the engine in, it is recommended that the hot oil be drained and fresh oil be poured in.

An engine in which defects requiring parts disassembly are discovered during the process of testing is subjected to a repeated testing.

TABLE 4-1

Running-in	Schedule of Running Load, hp	In Engine Number of crankshaft revolu- tions, rpm	Running-in time, minutes
Cold	 •=	400-600	15
Same	**	800-1000	20
Hot, without load	· •-	1000-1200	20
Same		1500-2000	15
Hot, under load	15-20	1600-2200	25
Same	40-60	2500-2800	25

Installation of the power unit in the motor vehicle

Before installing the engine, it is necessary to check the fastening of the motor mounts on the frame. If loosened rear motor mount fastenings are discovered during this, it is necessary to unpin the rear mount bolts, tighten the nuts, and re-pin them. If the front mount fastenings are loose, it is necessary only to tighten the bolts and spring washers.

To install the engine on the frame, it is necessary to move it to the motor vehicle on a transport carriage, mount the chain hooks of the device on the brackets for lifting the engine, raise the engine with a hoist (see Plate 4-49, b), and install it on the three mounts of the motor vehicle frame.

Insert one bolt in each of the rear motor mounts from the bottom, screw nuts onto the bolts, and tighten and pin them.

Insert two bolts in the holes in the front motor mounts, mount the electric equipment "ground" connector on the right bolt, screw on nuts with spring washers, tighten them, and then fusten the second end of the connector to the frame cross member.

Connect the reactor bar to the front motor mount and fasten it.

After installing and fastening the engine in the automobile frame, it is necessary to install the transmission shift lever housing and fasten it with bolts and spring washers. Connect the speedometer cable to the transmission and fasten it.

Connect the exhaust pipe to the flanges of the exhaust manifold of the engine on both sides, fasten them with bolts and nuts, and block them with washers, bending the edges up against flats of the nuts.

Connect the lever for hand drive of the pneumatic brakes to the hand brake control lever and fasten it. Connect the brake valve red to the foot brake pedal lever and fasten it (for adjustment of brake linkage, see Chapter 16).

Connect the clutch rod to the clutch pedal lever and fasten it (for adjustment of clutch pedal free play, see Chapter 6).

Connect the propellor shaft. Instail the cab floor inspection plate and fasten it with bolts.

Connect the carburetor linkage, cable for the manual choke and throttle, and fasten them. Connect the lines to the fuel pump and compressor and tighten them.

Connect the hoses to the hydraulic power steering pump and tighten them.

Install the cooling system radiator in assembly with the oil radiator on the front frame cross member, fasten the radiator with nuts on the stud, and pin the nut. Install the radiator jacket and fasten it to the fenders and splash guard with bolts, and then connect the radiator louvre control cable. Connect the hoses (upper and lower) of the water radiator pipes and fasten them. Connect the oil radiator hoses and fasten them.

Connect the ignition system and lighting system leads and fasten them on the poles of the appliances and transfer panels. Connect the starter lead to the storage battery post and fasten it, and then fasten the cover and lateral shield of the storage battery.

On the ZIL-131 motor vehicle, additionally connect the drive control for the transfer case and winch, and connect the hydraulic power steering oil radiator.

Close the engine hood, start the engine, and check the operation of all assemblies and accessories of the engine.

Parts dimensions

Cylinder sleeves. The geometric dimensions of the sleeves (Plate 4-89) may be measured without pressing them out of the cylinder block. The cylinder sleeves may also be measured after they are pressed out. The sleeves are measured in two mutually perpendicular directions, along the axis of the crankshaft and perpendicular to it, and also in two levels in height, at distances of 10-15 and 40-50 mm from the top surface of the cylinder block.

Maximum allowable wear of the cylinder sleeves is 0.4 mm. If wear in this amount is present, the sleeve should be pressed out of the cylinder block and sent into repair for regrinding to a repair dimension or to be replaced by a new one which is released by the factory as a set with the piston and rings.

Table 4-2 presents the dimensions of a sleeve (nominal and three repair). For providing selection of a piston according to the repair sleeve, the latter are divided into six groups within the limits of each repair dimension. Each group is designated by one or two letters. Corresponding pistons are designated by the same letters.

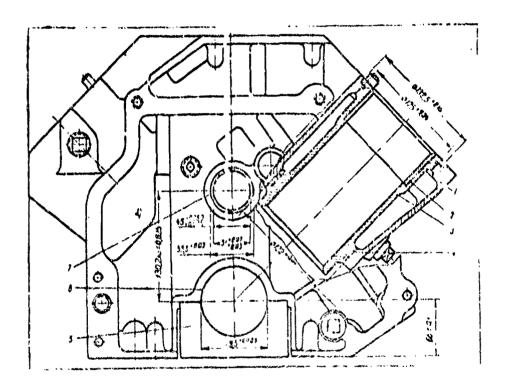


Plate 4-80. Fitting dimensions in a cylinder block for sleeves, interts, and camehaft bushings:

- 1) cylinder block 2) insert 3) cylinder sleeve 4) sleeve packing
- 5) rear main bearing cover 6) nest for insert 7) receptacle for camphaft bushing

All sieeves of a cylinder block must have a dimension within the limits of one repair dimension. The maximum ovality or conicity of a sleeve is not allowed to be greater than 0.020 mm. The working surface of a sleeve must be

smooth and polished, with a surface roughness of no less than 9th class.

Cylinder sleeves whose diameters are outside the limits of the maximum repair dimension by 101.56 mm are not repaired.

TABLE 4-2 Nominal and Repair Dimensions of Sleeves, mm

ل، مجيد سيد.		
P EREN	A B B	100,001—100,001 100,001—100,001 100,001—40,001 100,001—60,001
0,5	8 1 1 1 1 1 1	100,02 100,03 100,01 100,03 100,03 100,55 100,55 100,53
1,0	EEE XXXX	100.52 - 100.51 100.51 - 100.50 100.51 - 101.05 101.03 - 101.05
1,5	KK A GL CAA	101,02-101,01
		O,5 PT AAGE EE HO KK HIEL KK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK AAGE EK A

Koy: a) dimension

- e) nominal
- b) increase
- f) first repair
- c) group
- g) second repair
- d) sleeve diameter
- h) third repair

Regrinding of sleeves to repair dimensions in connection with the thin-walled sleeves and the presence of Ni-Resist [heat resistant iron alloy] inserts in them presents significant technological difficulties and must be conducted

in special shops which have the required equipment available.

The clutch housing. The surface of the clutch housing (see Piate 4-10) assembled with the cylinder block and with the transmission housing may not deviate more than 0.15 mm from perfect flatness.

The height of the support fingers of the housing must be within the limits of 70.00-69.26 mm. Near on the support fingers in height is allowed to 64 mm. The diameter of the holes for the rear motor mount bolts must be within the limits of 20.00-20.28 mm. If the holes are greatly worn, they are allowed to be reamed and have bushings inverted.

Holes for pressing in bushings for the clutch disengagement fork shaft are executed within the limits of 30.00-30.045 mm. Bronze bushings are pressed into these holes with an interference of 0.10 mm.

The internal dimension of the bushings is 25.06-25.13 mm. The maximum wear on the bushings is allowed within the limits of up to 0.7 mm. Worn out bushings must be pressed out and replaced with new ones which are pressed in.

After pressing them in, both bushings must be reamed simultaneously to assure their alignment. Nonalignment in the bushings is not allowed to be greater than 0.025 mm, and non-parallelness (in relation to the surface lying against the block) is not allowed to be greater than 0.1 mm on a length of 100 mm.

For a housing in the spare parts inventory, non-parallelness of the face surfaces assembled with the cylinder block and the transmission is not allowed to be greater than 0.05 mm on a length of 100 mm. Oscillation of the surface of the hole contering the transmission is not allowed to be greater than 0.15 mm, and this is checked by installing the housing on a device with locater holes on installing fingers, and simultaneously resting the housing on its surface, which is assembled against the cylinder block on the device base.

The designation of the piston group according to skirt diameter and dimension groups according to wrist pin holes in the front part of the piston are marked on their heads. Designations of piston markings of nominal and repair dimensions are shown in Plate 4-90.

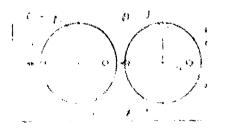


Plate 4-90. Piston markings of nominal and repair dimensions:

a) nominal dimension piston b) repair dimension piston 1 and 8) wrist pin ages 2 and 3) group designation according to piston skirt diameter 4) designation of repair dimension piston 5) designation of piston repair group 6 and 9) location of DTC stamp 7 and 10) designation of front part of piston

Piston dimensions are shown in Table 4-3. To provide individual selection of pistoms according to cylinders, each of the presented dimensions is divided into dimensional groups into which the pistons go according to skirt diameter, with increments of 0.01 mm. Piston skirt conicity must be within the limits of 0.035-0.050 mm. The difference between the maximum and minimum diameters of the skirt is 0.52 mm. The piston skirt surface must be smoothly polished, without dents or nicks, and must have a surface roughness of no less than 8th class. The pistons are manufactured according to weight to an accuracy of ±2 grams, and therefore they are not selected and marked according to weight.

TABLE 4-3 Piston Dimensions, mm

0		311	6 Marie	
Hotel		1	A	
i di pa		4.		
. 5.6 L.	•	1,6		
Fi	•	1.5	September 1	

Key: a) dimension

b) dismeter increase

c) group

- d) dimensions (in a plane permendicular to the wrist pin axis)
- e) nominal
- f) first repair
- g) second repair
- h) third repair

TABLE 4-4 Holes for Piston Wrist Pins. mm

Q.		farios :	in an ezin		
nng branch ly Ambbles	,	ij	144	tv	
21,963 G. 77,963	7,000	11,382	77 96 00	a (415	ì
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- Key: a) nominal dimension
 - b) dimension group
 - c) marking collar
 - d) blue
 - e) red
 - f) white
 - g) black

To ease individual selection of piston wrist pins, the pistons are divided according to diameter of their wrist pin holes into the four dimensional groups shown in Table 4-4. Marking of the dimensional group according to diameter of the wrist pin holes is done by putting paint on the wrist pin boss. Ovality or confeity of the wrist pin holes in the pisten is not allowed to be greater than 0.0025 mm.

Piston wrist pin dimensions are presented in Table 4-5. Roughness of the wrist pin surface must be no lower than 10b class. Surface hardness of the wrist pin is HPC 58-65. Depth of the hardened layer is 1.0-1.4 mm.

The wrist pins are fitted into the piston bosses with an interference of 0.0025-0.0075 was.

Piston wrist oin stop rings must fit into their grooves in the piston with some interference and must not rotate in them by hand. Rings which have lost their electicity are replaced. Dimensions of stop rings are shown in Plat 4-11.

Allowable noncylindricality of a wrist pin must not be greater than 0.0015

Compression and oil rings. Numbrial and repair dimensions for compression and oil rings along their exterior diameters, including those of the circular disk of a composite oil ring, are presented in Table 4-6. Clearances in the Fing fack and between the rings and the platon proover are presented in Isble 4.7. Piston ring hardness is his \$5-105.

For convenience in operation and repair, the factory produces a set of piston rings for one engine, which may consist of either case iron or conposite oil rings. Each set of piston rings for an engine has a number assigned to it: 130-1000101-A for those with cast iron oil rings; and 150-1000101 for those with composite of rings.

The connecting rod. During repair of the connecting rod small and (see Plate 4-15), dimensions for the bushing and for the wrist pin must correspond to the disensions show in Table 4-8.

For selection of piaton wrist pin-connecting rod pairs, the holes in the connecting red small and (along the bushing) are divided into dimensional groups every 0.0035 mm.

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Kay: 4) dimension

- b) dismoter increase
- c) designation of wrist pin dispater according to group
- d) designation of repair no: ensaid
- al noginal
- () first repair

- g) second repair
- h) color of warking
- i) green
- i) rose
- ki blue
- 1) red
- w) white
- n) black

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Table 4-6. Piston Ring Dimensions, me

a) dimension

- e) first repair
- b) increase
- f) second repair
- c) exterior ring g) third repair diameter
- d) nominal

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Table 4-7. Clearances in ring looks and between rings and pieton groves.

Kav:

- al piston rings
- b) classwhous
- c) in sing tack
- d) in height between kings and groove
- Atauaton E) abbar com-
- Diesagon
- h) cast iron oil
- i) composite steel circular disk oil

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Table 4-8. Connecting red small end

key: a) hominal disersion of connecting had small end hale for bushing

b) internal nominal disconsion of bushing for wrist pin according to group

- c) color arking
- d' blue
- 6) red
- f) white
- g) black

The crankshaft. Crankshaft journal dimensions are presented in Table 4-9. The factory is preparing a transfer to the use of inserts manufactured of steel-aluminum bands. In the transfer to the new band, main bearing journals will be decreased by 0.5 mm. The diameter of the connecting rod journals will not be changed. Longevity of the aluminum inserts is almost twice as high as that of the trimetallic ones. Shaft journal diameter is measured with a 50-100 meter micrometer. Shaft journals should be measured on no fewer than two respectively perpendicular places, and on two belts along the length of the journal.

Non-cylindricality in the journals of a new sheft or of a shaft which has undergone regrinding must not exceed 0.01 mm.

Main and connecting rod journal surface smoothness is assured by grinding and subsequent polishing and must not be lower than 9th class.

Crankshaft connecting rod journal length is 58.00-58.12 mm; main journal length is: 32.075-52.160 mm for the first journal, 31.00-31.17 mm for the second, third, and fourth journals, and 45.00-45.17 mm for the fifth journal.

The radii of the connecting rod and main journal fillets are 1.0-2.0 mm. The axes of the connecting rod journals must be parallel to the axes of the main journals, with non-parallelness not exceeding 0.01 mm.

Non-cylindricality of worn shaft journals is not allowed to be greater than 0.05 mm for connecting rod journals, and 0.07 mm for main journals. If the shaft journals are worn more than the allowable limits, the shaft is subjected to regrinding to repair dimensions.

Journal diameter beneath the small timing gear and beneath the crankshaft pulley is 45.950-45.975 mm. The internal diameter of the gear hole is 46.000-46.027 mm.

Oscillation of the journal beneath the gear must not exceed 0.03 mm on a length of 50 mm.

Facial webbling of the small timing gear installed on a mandrel must be no greater than 0.04 mm, measured on the side where the gear fits against the face of the main bearing.

Keyway width is 6.015-6.055 mm. Keyway repair by milling is allowed to a repair dimension of 6.445-6.090 mm.

Facial wobble of the shaft flange on which the flywheel is installed must not exceed 0.05 mm. Thickness of the flange is 11.57-12.2 mm. The diameter of the holes for the flywheel fastening bolts is 14.000-14.035 mm.

Bearing inserts. Insert dimensions are presented in Tuble 4-10. Bearing inserts which are decreased by 0.05 mm are used without regrinding the shaft journal. Markings of repair dimension inserts (0.05; 0.30; 0.60; 1.00; 1.25; 1.50; 2.00) are placed on the steel surface of the insert. Nominal dimension inserts have no markings.

Camshaft bearing journals. The diameter of the bearing journals on the camshaft, and also the amount of their allowable wear and journal repair dimensions are presented in Table 4-11.

Repair dimensions of the support flange (see Plate 4-55) of the camshaft are given in Table 4-12.

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							ı		1	

Table 4-9. Crankshaft journal dimensions, mm

- Key: a) dimension
- e) connecting rod
- b) diameter decrease
- f) nominal
- c) crankshaft journal dimensions
- g) first repair

- d) main
- * Dimensions are given for inserts manufactured of trimetallic bends.

The camshaft bearings are bored into the cylinder block parallel to the crankshaft bearings with a distance of 130.191-130.241 mm between the axes of these bearings (see Plate 4-89).

Diameters of the holes in the block for the camshaft bushings are 55.5-55.53 mm for the four front bearings and 49.5-49.53 mm for the rear bearing.

The camshaft bushings are thin-walled, stamped of a bimetallic band, and pressed into their receptacles with an interference of 0.120-0.210 mm. Dimensions of the camshaft bushings are given in Table 4-13.

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has a placement	10.00	1.70		1.83	2,012		
2-6	0,30	2,60	2,307 2,580	1,70	2,137 2,130		
3-6	0.50	2,15	2,537	1,80	2,287		
44 .	1,00	2,30	2,73/	2,08 1,96	2,487		
84	1,25	2,45 2,33	2,662	WHAT APPE	2,603		
6.0	1,80	2,53	2,947	2,30	2,737 2,730		
7-0	3,00	2,80 2,60	3,237	2,60	3,967		

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Table 4-10. Dimensions of main and connecting rod inserts, mm

key: a) dimension

- b) dimension decrease
- c) main bearing insert dimensions
- d) connecting rod bearing insert dimensions
- e) band thickness
- f) overall insert thickness
- g) nominal
- h) first repair
- * Dimensions are given for inserts manufactured of trimetallic bands.

Allowable non-alignment of the interior diameters of bushings which are pressed in and fitted according to the diameter of the shaft journal must not exceed 0.03 mm. Allowable wear of camshaft bushings is no greater than 0.05 mm.

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Table 4-11. Diameters of camshaft bearing journals, mm

Key: a) dimension

- b) diameter decrease
- c) journal dimensions
- d) nominal or repair
- e) allowable without repair
- f) nominal
- g) first repair
- h) second repair
- i) third repair
- j) fourth repair

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Table 4-12. Support flange repair dimensions, mm

Key: a) dimension

- b) flange thickness decrease
- c) flange thickness dimensions
- d) initia!
- e) allowable without repair
- f) nominal g) first repair

Camshaft gears. The internal dismeter of the small timing gear (see Plate 4-21) is 46.000-46.027 mm. The width of the keyway is 6.015-6.065 mm. Facial wobble of the small timing gear hub on the side lying against the face of the main journal is not allowed to be greater than 0.04 mm relative to the fitting hole on the gear. Wobble is checked with an indicator. The internal diameter of the camshaft gear is 30.000-30.023 mm. The width of the keyway is 6.015-6.065 mm. If the keyway is worn, a new one may be cut at an angle of 90° from the old one. The limiting width of the gear keyway allowable without repair is no greater than 6.1 mm. If the gear keyway is moved, the mark on the gear must also be moved. Facial wobble on the large timing gear on the side lying against the support flange is not allowed to be greater than 0.04 mm. Wobble on the remaining surfaces is no greater than 0.15 mm. Wobble is checked with an indicator (see Plate 3-86). The valve guides are cast iron. The dismeter of the holes in the cylinder head for the valve guides is 19.00-19.035 mm. The valve guides are pressed in with an interference of 0.014-0.065 mm. The internal diameter of the guides is presented in Table 4-14.

The valve springs are manufactured of 5.0 mm diameter wire. The total number of coils is $6.3/4 \pm 1/8$, of which 4.3/4 are working coils.

The exterior diameter of the coil is 39.5-40.0 mm.

The height of the spring is 58 mm in a free condition, 48.25 mm under a load of 26.8-30.8 kg, 38 mm under a load of 60-68 kg, and no more than 32.5 mm with the coils compressed together. After the spring is freed from load, it must not have any residual deformation. Springs which do not respond to these requirements are discarded.

Spring height and elasticity are checked on an instrument (see Plats 3-105). The amount of load on a spring is set according to a manometer.

Dimensions of the receptacles in the cylinder head for inserted seats, and dimensions of the valve seats are presented in Table 4-15.

Tappet holes. The diameters of holes are divided into two dimensional groups; 25.011-25.000 and 25.023-25.011 mm. The designation of the groups is marked on the bosses on the cylinder block in line with the holes.

If wear (ovality or conicity) appears in the tappet guide holes, it is recommended that their geometry be corrected using a reamer, bringing them to the repair dimensions presented in Table 4-16.

Tappets. Nominal and repair dimensions of tappets are presented in Table 4-17. Non-cylindricality in tappets is not allowed to be greater than 0.007 mm.

Wear on the spherical surface of a tappet must not exceed 0.10 mm, and wear on the tappet cuff in diameter must be no greater than 0.04 mm.

The rocker arm spacing spring (see Plate 4-26) is wound of 2.5 mm diameter wire. The full number of coils is 9 ± 1/4, of which 7 are working coils. The internal diameter of the spring is 23.0-23.52 mm.

The height of the spacing spring must be 69 mm in a free condition and 36 mm under a load of 10-12 kg. After freeing the spring from the load, it must not have any residual deformation. Springs with residual deformation are replaced.

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Table 4-13. Camshaft bushing dimensions, III Ø

- Key: a) dimension
 - b) diameter increase
 - _) internal bushing diameter
 - d) nominal
 - e) first repair
 - f) second repair
 - g) third repair

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« Рочантный (+0.38)	11,25011,277

Table 4-14. Internal diameter of "alve guides, was

Key: a) dimension

c) mominal

b) internal diameter d) repair (+0.25)

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№ Вынускного ихамана но- минильного диаметра Ф: Вынускного ихана-на	48,000-48,027
ремонтного диематра (+Q3) ф.Енуонне гнеся	48,300—48,327 9,00—4,10
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Ј. Дан внусиного илвин-	}
К.Нарумный номинила- ный диаметр	52,670-50, 7 00
1. Неружный ремонт (40,3)	56,970-57,000
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MB.	
ф Неружный номиналь: ный дивиату	40,175-46,200
очівружный ременті (+0.3)	48,475-40,500
₩ Плирина рабочей фас-	1.4
Біўгон рабочей фаски	45
Lincole causa nasna-	#,909,00

Table 4-15. Dimensions of inserted valve seats and receptacles in the cylinder heads for pressing them in, mm

Key: a) parameters

- b) dimension
- c) receptacle in cylinder head for valve seat
- d) nominal diameter intake valve
- e) repair diameter intake valve (+0.3)
- f) nominal diameter exhaust valve
- g) repair diameter exhaust valve (+0.3)
- h) receptacle depth
- i) valve seats
- j) for exhaust valve:

- k) exterior nominal diameter
- 1) exterior repair diameter (+0.3)
- m) working face width
- n) working face angle
- o) for exhaust valve:
- p) nominal exterior diameter
- q) repair exterior diameter (+0.3)
- r) working face width
- s) working face angle
- t) valve seat height

TABLE 4-16 Dimensions of Tappet Holes, mm

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2.6	+0,2	#. ED	25,24

Key: a) dimension

- b) dimension increase
- c) repair dimension d) allowable without repair
- e) nominal
- f) first ropair
- g) second repair

TABLE 4-17 Dimensions of Tappets, mm

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Kany	The same of	113	
Ноинивания .		54,678 24 54,682	,070
1-4 34NOMTHM 4	0,1	25,079 25,072	, 070
3.	0.2	23, 176 23, 100	. 170

Key: a) dimension

- b) tappet diameter increase
- c) dimension value
- d) nominal or repair
- e) allowable without repair
- f) nominal
- g) first repair
- h) second repair

The oil pump. The spring in the reduction gear of the oil pump upper section must have the following dimensions: 62.0-65.2 mm in a free condition, and 50 mm under a load of 6.10-7.30 kg. The diameter of the wire is 1.74-1.80 mm (65 G steel). A spring with residual deformation should be replaced.

The spring of the by-pass valve of the lower section of the pump must have the dimensions of: length in a free condition, 35 mm, and length under a load of 1.7-2.1 kg, 22 mm.

The diameter of the hole in the body (Plate 4-91) of the oil pump for the driving shaft of the pump must be within the limits of 15.03-15.06 mm. If the hole diameter is increased to 15.10 mm and more, the body must be exchanged on the hole repaired. Depth of the cavity for the gear is 37.950-38.000 mm, and if this depth is increased to 38.1 mm, the body is subjected to replacement or repair. The diameter of the cavity for the gear in the body and the cover must be 42.225-42.275 mm, and if this diameter is increased to 42.4 mm, the body or the lower cover is replaced or repaired.

The nominal dimension of the hele for the driven gear shaft in the body and in the lower cover of the pump wast be within the limits of 15.030-15.060 mm. If this hole diameter is increased to 15.10 mm, the body and lower section are discarded.

Depth of the hole for the gear in the lower section of the pump must be 16.965-17.000 mm, and if this depth is increased to 17.1 mm, the cover must be replaced or repaired.

Diameter of the drive shaft 1 (Plate 4-92) of the oil pump must be 14.982-15.000 mm. If this shaft diameter is increased to 14.960 mm and smaller, it should be replaced. Shaft curvature is not allowed to be greater than 0.025 mm.

Width of the keyway in the shaft must be within the limits of 2.950-2.900 mm. Keyway width is allowed to increase to a dimension of 3.040 mm without being repaired, with a corresponding increase in key size.

The nominal dimension of the shaft (Plate 4-93) of the drive gear must be within the limits of 15.070-15.082 mm. If the shaft is worn equally, the diameter is allowed to be decreased to 15.042 mm. One-sided wear of a shaft is not allowed. A worn out shaft should be pressed out and replaced with a new one. The nominal dimension of the holes in the driven gear for their shafts must be within the limits of 15.100-15.127 mm. If this gear hole dimension is increased to a diameter of 15.170 mm and more, the gear should be replaced or repaired by installing a bushing.

The nominal exterior diameter of the drive gears 2 and 3 (see Plate 4-92) of the lower and upper sections of the pump is equal to 42.100-42.125 mm, and if the diameter is decreased to 42.0 mm, the gear should be discarded.

Tooth length on the drive and driven gears of the upper section of the pump is equal to 37.975-38.000 mm, and with a decrease in this tooth length to 37.0 mm, the gears are discarded.

Tooth length of the drive and driven gears of the pump lower section is 16.975-17.000 am, and if this tooth length is decreased to 16.9 mm, the gear is discarded.

The assembly surface of the intermediate pump cover (Plate 3-94), which is assembled against the faces of the gears, must be parallel and flat. Non-parallelness is allowed to be 0.03 mm on a length of 50 km. Non-flatness of the cover surface or wear on it is allowed to be no greater than 0.04 km.

The surface of the lower pump cover (see Plate 4-91) which touches against the faces of the gears must be flat. Non-flatness of the cover surface or wear is not allowed to be greater than).04 mm, and non-parallelness is allowed to be 0.08 mm on a length of 100 mm.

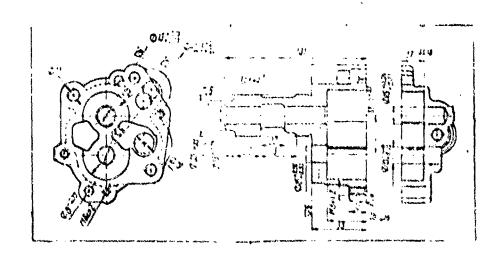


Plate 4-91. Oil pump body with cover

The partial flow filter for centrifugal oil cleaning. The nominal diameter of the shaft bushing hole (Plate 4-95, a) must be 10.500-10.527 mm for the upper section and 15.095-15.120 mm for the lower section.

The numine's dismeter of the shaft assembled with the bushings is 10.445-10.470 mm for the upper section and 15.040-15.065 mm for the lower section.

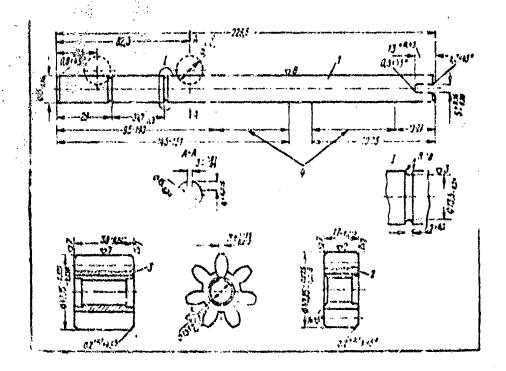


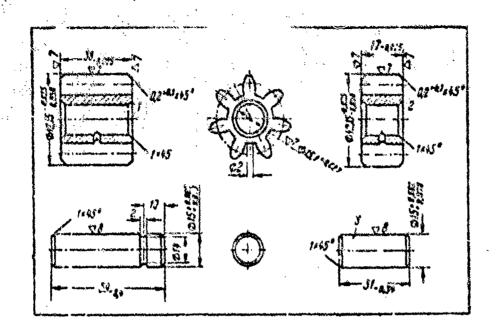
Plate 4-92. Oil pump drive shaft with gears;
1) shaft 3) lower section drive gear 3) upper section drive gear

The by-pass valve spring has 12 coils. The length of the spring in a free condition is 62 mm, and under a lead of 0.9-1.1 kg, it is 44 mm. Spring dismeter is 11.5 mm. The spring material is "V" hardness spring wire of group 1, 1.0 mm in dismeter (COCT 5047-49).

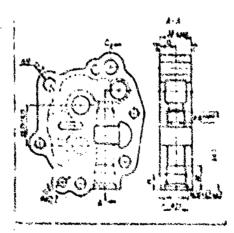
The full flow centrifugal oil steaming fixter. Plate 4-95, b, shows the body and shaft of the fitter and their basic dimensions. The nominal dimension of the shaft bushing hole is 14,000-14.027 mm for the upper bushing and 17.000-17.035 mm for the lower bushing. The nominal dimension of the shaft assembled with the bushings is 13.935-13.970 mm on the upper journal and 16.945-15.970 mm on the lower journal.

The water pump. In the water pump, the nominal dimension of the hole for the front bearing in 61.990-62.020 mm, and for the rear bearing, it is 46.992-47.018 mm. If the front hole dimmeter is increased to more than 62.04 mm, and the rear one is greater than 47.042 mm, the bearing body must be replaced.

The nominal dimension of the hole for the fan pulley hub bearing is 39.980-80.607 mm. If this dismeter is increased to 40.077 mm, the pulley must be replaced.



- Plate 4-93. Oil pump shaft with driven gears:
 1) upper section driven gear 2) lower section driven gear
 3) lower section driven gear shaft 4) upper section driven gear shaft



Oil pump is ermediate cover

The geometric dimensions of the water pump bearing body are shown in Plate 4-96.

Dimensions of the pump impelior body are shown in Plate 4-97. Non-flatness of the flange surface assembled against the bearing body is not allowed to be greater than 0.1 mm. The plane lying against the cylinder block must be parallel to the flange surface connected with the bearing body. Non-parallelness of these planes is not allowed to be greater than 0.2 mm. If non-parallelness and non-flatness are greater than these, the pump body must be replaced.

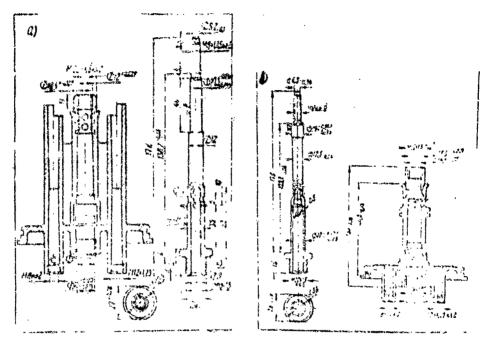


Plate 4-95. Oil filter body and shaft:

- a) partial flow
- b) full flow

The water pump shaft from a ZIL-13C engine (Plate 4-98) has a diameter of 15.588-17.000 mm. The water pump shaft of a ZIL-131 engine differs from the pump shaft of a ZIL-13O engine in the position of its keyway. If the shaft is worn to a diameter of less than 16.976 mm, it must be replaced with a new one. Shaft curvature is not allowed to be greater than 0.03 mm. The width of the keyway must be 3.945-4.045 mm, and if the keyway is worn to a dimension of greater than 4.08 mm, the shaft must be replaced.

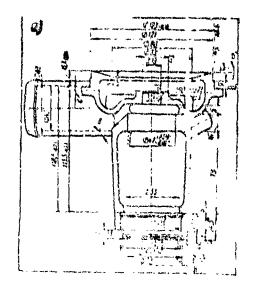
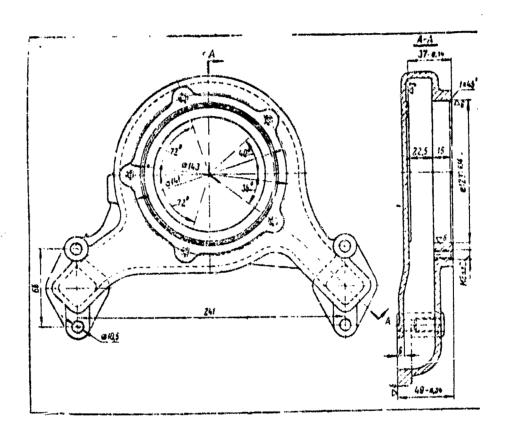




Plate --96. Water pump body of the:
a) LIL-130 engine
b) ZIL-131 engine



Place 4-97. Water pump impellar body

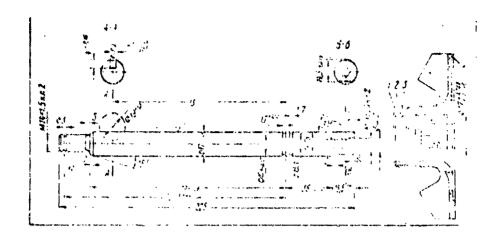


Plate 4-98. Water pump shaft with impeller of the ZIL-130:
1) band 2) textolite packing washer 3) collar 4) impeller

Chapter 5. The Engine Fuel System

Arrangement

The schematic of operation of the fuel systems of all ZIL engines are principally identical (Plate S-1, 5-2, 5-3). Fuel tanks are welded and stamped of lead treated short. Fuel feed from the tanks is forced by a diaphragm type fuel pump. All carburetors are vertical, downdraft, with one or two throats. The air filtures are of the oil-inertia type. All engines are equipped with crankshaft revolution speed governors.

For information on the intake and exhaust manifolds of in-line engines, see Chapter 3, and for information on V-shaped engines, see Chapter 4.

During disassembly, all small parts of the assemblies should be collected in special boxes or in boxes which have compartments in them. Calibrated holes (jets and valves) of the carburetors and pumps must not be cleaned with metal rods, since this operation may change the dimensions of the holes, leading to their unusalility.

Fuel tanks. Depending on the purpose of the motor vehicle on which the fuel tanks are mounted, they vary in volume. Table 5-1 shows the volume and number of tanks.

Fuel pumps. Disphragm fuel fpumps of the following types are installed on ZIL engines: on the ZIL-157K ongine, B-9B (Plate 5-4) or B-10B; on the ZIL-130 engine, B-9 (Plate 5-5) or B-10; on the ZIL-131, B-10 (Plate 5-6).

Characteristics of the fuel jumps are presented in Table 5-2.

The B-10B fuel pump differs from the B-10 pump only by its plunger arm. The pressure of all pumps at zero feed is no greater than 0.296 kg/cm².

The efficiency of a fuel pump is determined by its productivity (liters per hour) and maximum pressure (mm in a column of mercury or kg/cm²), which are determined on special installations or directly on the ergine. The listed parameters on installations are usually measured at 1300-1400 crankshaft rpm of the engine activating the fuel pump, with the fuel sucking and pumping height of 0.5 mm, fuel lines with an interior diameter of 6 mm, and zero fuel feed into the carburetor float chamber.

Автоми-биль	ist garders.	Eunicia Cana, a
ЗИЛ-157К	2	150; 65
3H/I-157KE, 3H/I-157KB	2	150, 150
311Л-130 и ЗИЛ-130Г	1	170
341/1430/11	1	125
307-1308;	2	125; 125
3117-1319	2	170; 170
SMJ = ZIL, B.V, F=G.	Д=D,	'A=L

Table 5-1. Number and volume of fuel tanks installed on motor vehicles

Key: a) motor vehicle

- b) number of tanks
- c) tank volume, liters

Тип настся	Харантеристика	Проняводи- тельн сть при 1000— 1400 об/мим распроле- лительн го вела, 4/4
6-9C	Насос е двумя	
B-9 H-10	ипускивани клапанами То жа Насос с тремя внуск-	140
B-10B	ными и треля выпуск- ными клапонами То же	180 180
8:8	1	

Table 5-2. Pump characteristics

Key: a) pump type

- b) characteristics
- c) productivity at 1300-1400 crankshaft rpv, liters/hr
- d; pump with two inlet valves
- e) same
- f) pump with three inlet and three outlet valves

Varying (nonuniform) quantities of fuel in volume are automatically fed by the fuel pump for various working rates of the engine depending on its fuel consumption. This takes place in the following manner.

A change in fuel consumption causes a variation in its level in the carburetor float chamber, consequently changing the blocking force of the fuel feed needle valve. Therefore, a fuel back pressure which has a changing value is created in the fuel line connecting the fuel pump to the carburetor. The less the needle valve is open, i.e., the less fuel the engine is consuming,

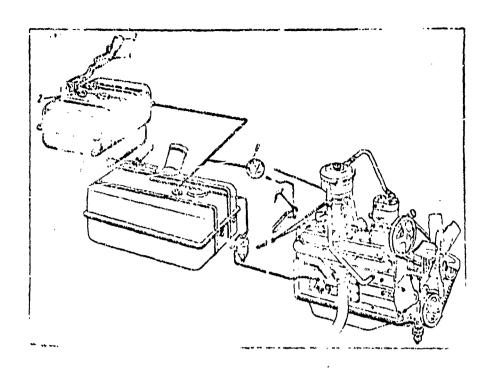
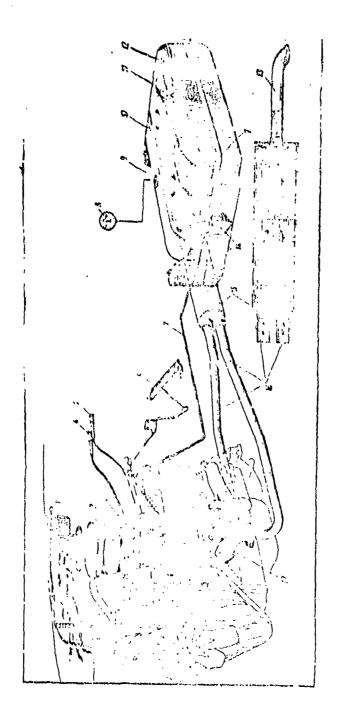


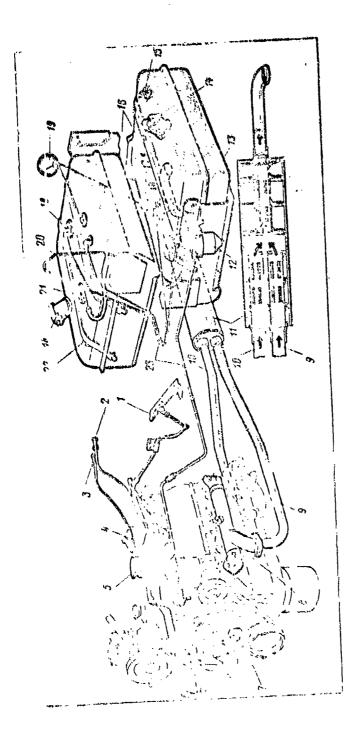
Plate 5-1. Fuel system layout of ZIL-157K engine:
1) auxiliary tank 2) fuel level sending switch 3) fuel filler cap 4) filler neck 5) fuel valve 6) fuel level indicator

the greater is the amount of this back pressure. As the result of this back pressure, the pump diaphragm does not move upward by a full stroke, but only partially, depending on fuel expenditure at the given moment of the engine's operation. When fuel in the carburetor float chamber reaches a set level (in correspondence with adjustment of the float) the needle valve closes, back pressure reaches its maximum value, and the pump stops feeding fuel. This phenomenon is called the zero fuel feed, during which pump pressure is measured with manometer installed on the outlet line (on the transfer) of the pump.

Carburetors. Downdraft carburetors with constant suction diffusers and balanced float chambers are installed on the ZIL trucks. The necessary composition of the mixture in the carburetors is attained as the result of pneumatic restriction of the fuel lead and the use of two economizer valves (with mechanical and pneumatic drives).



manual choke control manual lever control chrottle 6) accelerator pedal 7) fuel lines 8) fuel level 9) fuel lavel sending switch 10) fuel tank 11) fuel filler cap 12) fuel valve 13) muffler tail pipe 14) filter and sediment bowl 15) muffler 16) extaust pipes 17) exhaust past manifold 18) fuel pump Plate 5-2. Fuel system layout of the ZIL-130 engine:
1) passage supplying air to air filter 2) air filter 3) carburetor indicator



governor sending switch 8) exhasut manifold 9 and 10) exhaust pipes 11) muffler governor sending switch 8) fuel shut-off valve 14) fuel filler cap 15 and 18) angle connectors 16) fuel tanks 17) fuel level sending switch 19) fuel level indicator 20) fuel connectors 16) fuel tanks 17) fuel level sending switch 19) fuel level indicator 20) fuel 1) accelerator pedal 2) magnal throttle control handle 3) manual choke control handle tank air vemt 21) valve box 22) steel tank fastening strap 25) fuel lines Fuel system layout of the ZIL-131 engine: 5) carburetor 6) fuel pump

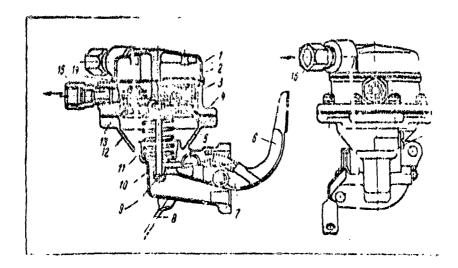


Plate 5-4. B-9B fuel pump:

1) cover 2) screen filter 3) inlet valve 4) head

5) diaphragm 6) rocker arm 7) rocker arm spring

8) handle fer manual fuel pumping 9) support washer

10) red 11) diaphragm rod spring 12) body 13) outlet

valve 14) gasket 15) fitting for fuel outlet 16) fit
ting for fuel inlet 17) control hole plug

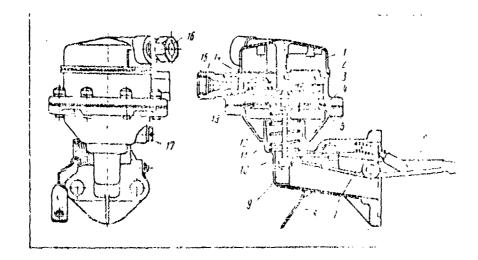


Plate 5-5. 8-9 fuel pump (see Plate 5-4 for nomenclature)

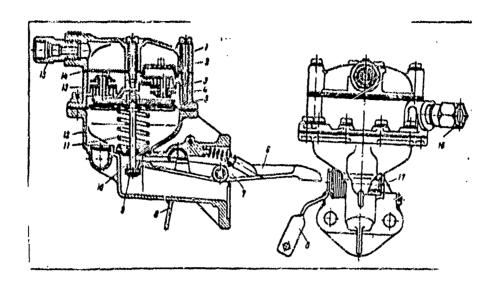


Plate 5-6. B-10 fuel pump (see Plate 5-4 for nomenclature)

The carburetors have an idling system with feed from the main fuel passage for each throat. The carburetors have accelerator pumps with machanical drive to enrich the mixture.

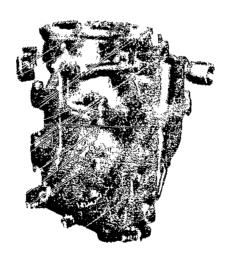


Plate 5-7, K-84M carburetor

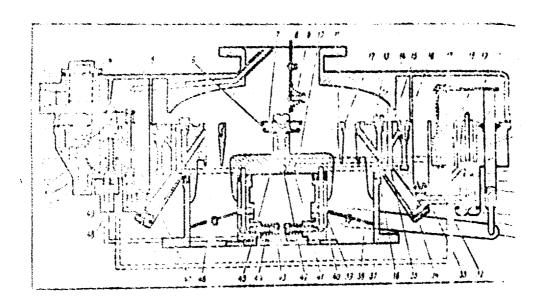


Plate 5-8. Layout of K-84M carburetor

1) cover 2) float chamber needle valve 3) screened filter

4) filter plug 5) balancing passage 6) air chamber 7) accelerator pump spray nozzle 8) choke plate 9) air valve 10) float chamber body 11) small diffuser 12) circular gap 13) air jet

14) high speed jet 15 and 25) holes 16) idle jet 17 and 21) rods

18, 28, 44, and 50) springs 19 and 52) pistons 20) bar 22) inlet vlave 23 and 36) gaske's 24) plunger 26) seat 27) mechanical drive economizer valve 29 and 34) plugs 30) drawbar 31) lever

32) fuel passage 33) main jet 35) valve 37) mixing chamber body

38) throttle 39) idle system upper holes 40) idle system holes

41) accelerator pump passage 42) needle valve 43) idle system adjusting screw 45) central screw 46) pneumatic drive economizer valve piston gasket 53) float

The float chamber, accelerator pump, economizers, and choke are common to all the carburetors.

To increase reliability and longevity, beginning in 1966, K-88A carburetors, differing from the K-88 carburetors by the absence of the pneumatic drive economizer valve, were installed on the V-shaped engines. In construction of the K-88A carburetors, the float lever was strengthened with a non-corroding contact plate. The accelerator pump drive unit was improved and strengthened by the introduction of heat treamment of its parts and metal-ceramic bushings, the dismeter of the throttle shaft was increased, and the construction of its fastening was strengthened, and gasoline-resistant shaft bearing lubrication was introduced. Additional cross pieces formed immediately on the casting were introduced into the diffusion portion of the carburetor. This improves even feeding of the engine cylinders with fuel by about 5% and provides an increase in the engine's torque moment in the area of low revolutions by by 2 kg m.

	Char	Moror	
Carburetor K-84M	Carburetor	Revolution governor	vehicle engine
	Two-throat. Each throat has two diffusers and a separate idle system with an accelerator pump and economizers.	Pneumatic type with two throttles, non-symmetric ally installed with a separate body.	ZIL-157K
K-88 and K-88A	Two-throat, with diaphragm operation of the revolution governor mechanism. Each carburetor throat has two diffusers and a separate idle system with an accelerator pump and economizers.	the revolution consisting of a centrifug smism. Each switch which receives rot tons from the timing ges a separate mechanism and has a diaph ith an accel- drive which acts on the	

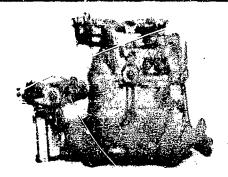


Plate 5-9. The K-88 (K-88A) carburetor

Carburetor types (Plates 5-7, 5-8, 5-9, 5-10) and their characteristics are presented in Table 5-3

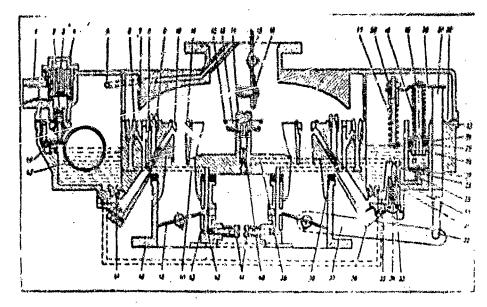
Basic data on carburstors and their adjustment parameters are presented in Table 5-4.

The schematic of drive control for the K-84M carburetor is shown in Plate S-11, and that for the K-88 and K-88A carburetors is presented in Plate S-12.

The control cables must not be sharply bent at any angle. There must be no traces of corrosion on the cables

The cable jacket must not have gaps or breaks. All threaded and articulated connections must be in proper working order.

The return spring must not have residual deformation.



Place 5-10. Layout of the K-88A carburetor:

1) cover 2) flow charber needle valve 3) screen filter 4) filter plug 5) belancing passage 6; idle jet 7) holer 8) high speed jet 9) air jet 10) small diffuser 11) circular gap 12) accelerator pump spray nousie 13) air charber 14) central screw 15) cheke place 16) air valve 17, 19, and 21) rods 18) spring 21) bar 22) circular passage 23) float diamber body 24) collar 25) collar soring 26) valuabling 27) holes 28) intermediate pluncer 29) inlet bail valve 30) seat 31) ball valve 32) draw bar 33 and 36) plugs 34) spring 35) fuel passage 37) lever 38) gasket 39) accelerator pump passage 40) needle valve 41) idle system adjusting screw 42) idle system upper hole 45; idle system lower hole 44) passage 45) throttle 46) mixing charber cody 47) main jet 48) float 49) float spring 50) nut

Air filters. The following types of air filters are installed on the ZIL engines: VN-15A on the ZIL-157k engine: VN-16 on the ZIL-130 engine, and VPM-3 on the ZIL-131 angine.

The VM-15A and VM-16 filters are of the dilineral type, with two-stage air cleaning and a special pipe for supplying air to the coapressor. The filtering element of the VM-15A filter is caprose (polycaprolactan resin and fiber).

The VF-16 air filter (Plats 5-13) works in the fallowing mender. One to action of the suction created by the engine, dust-less air moves through the pipe in the fence into the inlet circular gap 13 and, soving doseward along it, comes into contact with the oil, in which the first inertial cleaning of the largest dust particles from the air takes place

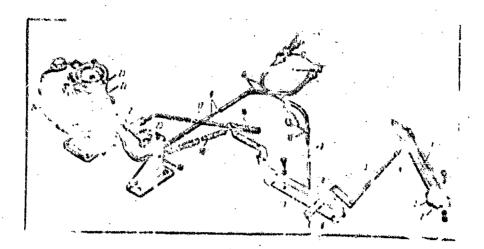


Plate 5-11. Control apparatus of the K-84M carbureter

1) pedal 2) pedal pin 3) pedal bracket 4) pedal rod nut

5) pedal rod 6 and 24) cable clamp acrews 7) throttle control apparatus stationary bracket 3) thruttle control apparatus moving bracket 9) cables 10 and 22) cable jacket clamps

11) choke control handle 12) manual throttle control handle

(3) pressure rings (4) pressure nuts (5) cut le jackets

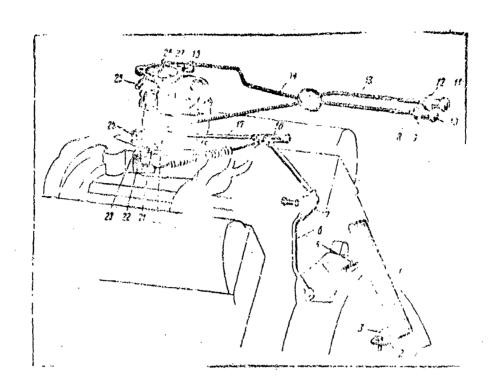
16) compensator spring 17) intermodiate rod 18) return spring

19) bracket 20) rossing crank 21) throttle crank rod
23) carburetor

Tegether with the sir stream, oil from the space 16, located beneath the deflector 3, is partially splanhed into the filtering element 6, lubricating it, as the result of which cleaning offectiveness is increased. Excess oil flows through the circular openings 14 in the inclined plane of the deflector 3 into oil bath 3. In this remove, oil is circulated along the inclined surface of the deflector and washes fallen dust particles from it. Washed-off dust particles settle to the bottom of the oil bath.

Air is supplied to the filter through air passage 1 (Plate 5-14) in the engine hood, which is connected to the sir filter with a corrugated pipe. Either fresh air or heated air free the space beneath the head may be fed into the passage, depending on the position of plate 5 located in the sir passage. During the rold time of year, the hole supplying the passage with exterior air should be reversed, and on a opened during operations under difficult read conditions.

Buring the ware time of year, it is notestary to open the holes supplying the passage with exterior air. The use of exterior air whose temperature is lower than the temperature of the air in the space because the head allows an increase in filling the cylinders, and greater angine power will be received.





Pince 3-13. VM-16 air filter

F and 11) duets 2) oil bath

5 deflector 6.5, and 10) sealing gaskets 6) filtering element

7) immion scrow 8) wing nut

9) thumb scrow 12) gir outlet

ine to compressor 13) circular

gap 14) circular passage

13) filter body 161 space

Operation of the engine without the filter or with no oil in the filter is not allowed!

It should be remembered that the service life of an engine depends to a significant degree on the proper operation of the air filter, and consequently, on its timely cleaning and servicing.

The VPM-3 air filter (Plate S-15) is of the foam oil and inertial type, with three-stage air cleaning and a special pipe for supplying air to the compressor. The air filter works in the following manner.

Dust-laden air is drawn into the central pipe 7 due to the action of the suction created by the engine and, moving downward, comes into contact with the oil; the largest dust particles are cleaned from the air during this first cleaning. Under action of the air pressure, oil moves from the center of the deflector 15 to the holes 3 and partially moves into the throttling chamber 12 and the feam oil retaining packing 9, while part of the oil flows through holes 3 into the space 20 of the oil bath 16.

In its turn, oil spouts from the space 20 through the central hole 18, due to the difference in oil levels in space 20 and area 1 above the deflector, and, moving along the deflector 15, cleans the dust from it.

Oil arriving in the throttling case 12 and in the foam oil retaining packing 9 is strongly feamed. Foamed oil and the filtering packing clean the saullar dust particles from the air.

The air stream holds the oil in the packing 9 and casette 12. Since the oil constantly moves into the foam oil retaining packing, its excess flows downward along the walls of the packing. Part of the oil flowing along the exterior walls of the packing reaches holes 3, through which it moves into the oil both space.

During travel of the air above the deflector in area 2, a suction is created, as the result of which a layer of oil flowing slong the internal walls of the packing and slots 5 in the ejector 19 is sucked up and hold by the air stream, forming an oil mist which reaches the deflector 15, through which air flows, partially carrying the oil into the packing 9 and casette 12.

The accumulating dirty oil remains in the oil bath 10, where dust settles out into a sediment. Feed and return of oil into the packing, oil movement along the deflector, and the work of the ejector provide oil circulation. Considering that the engine does not work for an extended period of time at one rate, out changes it, the working rate of the oil filter is also changed correspondingly.

In this case, oil arrives at varying heights in the packing, i.e., sometimes rising to the maximum height, and then flowing into the oil bath, providing additional washing of the packing.

Air is Supplied to the filter the same way as in the ZIL-130 motor vehicle.

It should be remembered that the service life of the engine, especially that of one working off the road, depends to a significant degree on the proper operation of the air filter and on its timely cleaning and servicing.

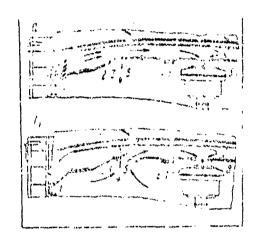


Plate 5-14. Diagram of air supply to the air filter:

- a) through hood louvres b) from the under-hood space
- 1) hood louvres 2) air passage in the hood 3) valve spring 4) valve shaft (handle) 5) valve 6) plug in hole for installation of an air filter used on the motor vehicles 7) air filter 8) bulkhead

The engine crankshaft revolution speed governor is shown in Plates 5-16 and 5-17. In the ZIL trucks, fuel passes through the two-stage cleaning through a sediment filter (Plate 5-18) and a fine cleaning fuel filter

(Plate 5-19).

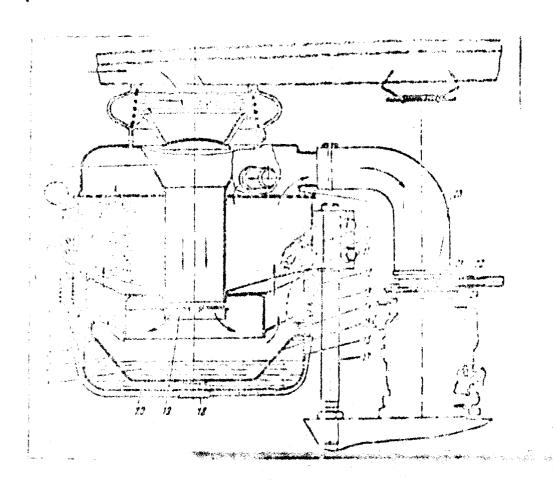


Plate 5-15. VPM-3 air filter:

1) area above the deflector 2) area above the oil level 3) holes
4) cable 5) slot d) lever 7) central pipe 8) body 9) foam oil retaining packing 10) bracket 11) stand for fastening bolt
12) throt:ling casette 13) rubber washer 14) spring 15) deflector
16) oil bath 17) stand 18) central hole 19) ejector 20) oil bath space 21) inlet tube for distributor ventilation 22) rubber hose
23) outlet tube for distributor ventilation 24) carburetor

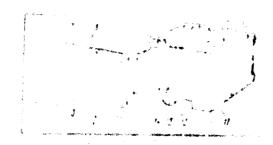


Plate 5-16. Revolution governor for k-84M carburetor:

- i) formed pawi 2) rod 3) spring
- 4) fine adjustment adjusting nut
- 5) coarse adjustment adjusting screw
- 6) small cover 7) piston 8) rod
- 9) pass ge connecting sleeve
- 10) passage connecting the governor vacuum mechanism with the carburetor air space 11) governor body 12) governor throttle 13) carburetor throttle shaft 14) needle bearing

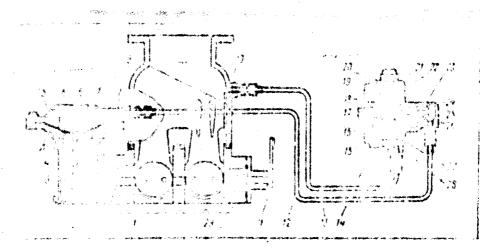


Plate 5-17. Schematic of connecting the centrifugal revolution governor switch to the diaphragm mechanism of a K-88 (K-88A) carburetor:

A-8) spaces 1) throttle 2 and 3) jets 4) diaphragm mechanism spring 5) diaphragm mechanism cover 6) diaphragm 7) rod 8) lever 9 and 10) holes 11) throttle drive lever 12 and 13) lines 14; centrifugal switch spring 15) washer 16) seat gasket 17) slot in rotor shaft for connecting with camshaft 18) seal 19) cover 20) spring tension adjusting screw 21) plug 22) rotor 23) filter 24) metal-ceramic bushing 25) switch hody 26) passage 27) valve 28) valve seat hole 29) forked joint

Table 5-4. Basic parameters of carturetors

aramoters	K-84M	Carburetors K-88	K-88A
Diffuser diameter, mm:			
1. small	8.5	8.5	8.5
2. large	26.0	29.0	29.0
dixing chamber diameter, mm	32.0	32.0	36.0
ir threat diameter, mm	56.0	56.0	60.0
distance from fuel level in			
float chamber to the top			
assembly surface of the			
body, sun	18-19	18-19	18-19
		18.7-19.7	19.2-20.2
arburetor height, mm	156		153.5
assage capability of motor-	150	40010	20070
ing elements when checked			
with water under a pressure	4		
of 1000 ± 2 mm in a water	•		
column and a temperature of	ç		
+20°C, cm ³ /min:	•		
1. main jet	24725%	370.5-359.5	311-319
2. high speed jet (in	247-233	a. v.a. v.a.	011-010
sprayer)			
3. high speed jet (separate)	2 980 2 180	330,5-369.5	1125-1175
4. valve jet in economizer		300,000,0	1145 1175
with preumatic drive		ቁምሳ <u>ዜ 1</u> 77 ፎ	
5. valve jet in sconomizer		3/2.3-3///3	
with mechanical drive			212-218
		103.5-106.5	2.14-2.26
6. air jet Diameter of idle jet, mm	103.3-100.3	103.3-100.4	2.14-2.20
1. fuel hole	0.60.0.66	0.60-0.645	0.60-0.66
2. air hole		1.80-1.92	1,6-1.72
acuum at the moment of	1.00-1.52	1.00-1.54	1.8-1.92
			1.0~1.54
pneumatically driven	with		
economizer valve opening, and a column of mercury		125-135	
Distance between the edge of		125-155	
the throttle and the wall of the mixing chamber at the	J Ľ		
••			
moment of mechanical drive	nm (1.7)	0 0 0 7	9.0-9.3
oconomizer valve opening, a	nun 9.0	9,0-9.3	3.K.n.a
full opening of the throttle,	a st		
(distance between the edge			
the throttle and the wall of		C 19 B 14 B	14 5 13 6
the mixing chamber), mm		S 13.8-14.8	14.5-14.8
roductivity of the accelerate			
pump for ten full strokes	ot		
the piston at a rate of 20 pumps per minute, cm ³	17, no 1	055 15-20	15-20
	17 1	nea 15 70	1 5 . 213

Technical servicing

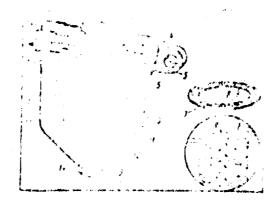
Garing daily service, the fuel level in the tank should be checked and in should be filled if necessary. Visually inspect the tightness of the line approactions and, in case fuel is leaking, tighten the nuts.

During TS-1, check the connection of the rods to the throttle control lover and choke, the action of the controls, and the full travel of closing and opening of the throttle and choke.

Check the condition of the rubber pipe connecting the engine air filter to the hood.

Check the condition of the fuel accessories.

The filter-sediment bowl. The plug should be periodically unscrewed, and sediment from the sediment filter body allowed to drain out.



Place 5-18. Filter-sediment bowl:

1) filter cover 2) bolt 3, 5, 13,
and 17) gaskets 4) fuel flow passage
6) filtering element washer 7) filtering element plate 8) holes in
plates for passage of fuel 9) projections
on plates 10) filtering element ring
11) rod 12) spring 14) plug 15) filter body 16) filtering element 18) fuel
outlet passage

The filtering element of the fuel filter, should be washed out during the TS-2. For washing the filtering element, it is necessary to close the fuel tank valve, unscrew bolt 2 (see Plate 5-18), fastening the filter cover, and disconnect the body 15 of the filter-sediment bowl, together with the

filtering element.

If ethyl gasoline is being used, unscrew the plug beforehand, and drain the gasoline, not allowing it to fall on the hands and clothing.

During disassembly of the filter-sediment bowl, attention should be paid to protecting the gaskets providing the seal between the body and cover. Having removed the body, wash it out with clean gasoline and inspect the parts.

The plates 7 on the filtering element must not be damaged.

After washing, checking, and assembly of the filter-sediment bowl, install it in place and tighten the bolt on the cover.

The fire cleaning fuel filter. For disassembly of the filter, it is necessary to loosen the nut (see Plate 5-19), move bracket 6 away, remove cup 5 in assembly with the filter, and pull the cup gasket from the body. Pull screen filter 3 with spring 4 from the cup.

After disassemply, wash the parts in account or clean gasoline. Blow the parts and fixer body passages out with compressed air.

After washing and checking the filter, assemble it and install it in place. During disassembly, washing, and assembly of the filter, it is necessary to handle the acreened filter very carefully.

On some engines, the screened filter has been replaced with a ceramic filter 9.

Checking and adjusting the carburetor on the motor vehicle. If an insufficient supply of fuel is reaching the carburetor, it is necessary to check:

The proper installation of intake manifild gaskets and the absence of air leaks into the manifold and carburetor;

The proper operation of the fuel pump (checking by means of pumping with the manual pumping lever with the fuel line disconnected from the carburetor);

The proper opening of the throttle (if the throttle does not open fully, it is necessary to adjust the throttle linkage).

The foot drive of the K-84M carburetor is adjusted with the two threaded ends on rod 21 (see Plate S-11) and on rod 17, as well as with the threaded rod 5 on the pedal.

The foot feed of the K-88 and K-88A carbureters is adjusted with the thresded fork 23 (see Plate S-12) and rod 4.

Adjustment for full opening of the throttle must be accomplished so that the throttle control pedal does not reach the floor of the cab by 3-5 mm. After completing the adjustment, it is necessary to tighten the rods with stop nuts.

Manual throttle control is adjusted by the clamps which are installed on the ends of the control cables to that with the handle 11 fully moved out, there is a clearance of 2-3 mm between the bracket and the clamp fastened on the cable.

During adjustment of the choke, it is necessary to set handle 10 of the manual control so that it does not reach the support screen of the cab by 2-3 mm. In this position, with r fully open choke, connect cable 27 of the control with lever 26 of the choke, and fasten it with a screw.

In a case of a properly working fuel pump and the absence of air lesks through the gaskets, it is necessary to look for the reason for poor fuel supply in the carburetor itself, for which it is necessary to unscrew and check the screened filter and, if it is not clogged, check the passage in the fuel feed valve unit.

For inspection and cleaning of the fuel feed valve passage, remove the air filter, disconnect the choke cable, remove the carburetor cover, check the condition of the passages, wash them out with clean gasoline, and blow them out with compressed air.

If the needle valve passages are cleaned, the reason for poor fuel feed might be clogging of the carburetor jets. For checking and cleaning the jets, the carburetor should be removed.

For cleaning the passages and blowing out the jets, unscrew the plugs from the high speed jet passages and from the mechanical economizer passage. Then blow out the jets and carburetor passages with compressed air.

Blowing out the assembled carburetor (through the fuel supply holes, balancing pipe, or other) with compressed air is not allowed, since it may lead to crumpling of the float.

After checking and cleaning the passages and jets, assemble the carburetor, install it on the engine, and check its fuel feed during the engine's operation at various rates.

In case of : treased fuel consumption, the full opening of the choke should first be checked, and the fuel level in the carburetor should be checked in the following manner: unscrew the control plug from the float chamber body, and with the engine running at idle, check the fuel level, which must be visible through the hole. If fuel runs out of the hole, the condition of the float or the fuel feed valve unit should be checked.

To eliminate these deficiencies, the carburetor cover should be removed and the fiel feed valve unit checked. If the needle valve does not fit tightly in its seat, blow out the valve unit with compressed air and remove fuel residue.

If the cone and seat of the needle valve are worn, the valve will sit in its seat too late. As a result of this, the fuel level in the float chamber will rise. To eliminate this deficiency, it is necessary to bend the float lever or adjust the setting of the valve body.

Before adjusting the carburetor, it is necessary to warm the engine and check to see that the ignition accessories are operating properly. Special attention must be directed toward the proper operation of the spark plugs and the proper clearance between their electrodes. For adjusting the qualitative composition of fuel during operation at an idling rate, start the engine, set the throttle at the minimum opening with which the engine will run reliably and without missing, with the stop screw 2 (Plates 5-20, 5-21). Then check the qualitative adjustment.

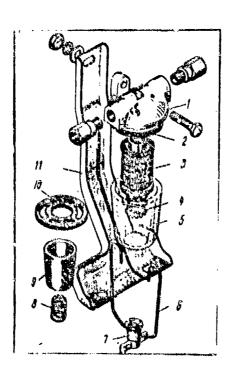


Plate 5-19. Fine cleaning filter:
1) bod/ 2) screened filter packing
gasket 3) screened filter 4) spring
5) filter cup 6) bracket 7) tension
nut 8) cersuic filter spring 9) ceramic
filter 10) ceramic filter packing
gasket 11) bracket



Plate 5-20. Adjusting the idle on a K-84M carburetor:

1) mixture quality screw 2) mixture quantity screw

The two-throat K-84M, K-88, and K-88A carburetors each have two screws 1 and require separate adjustment for each throat. The screws for qualitative adjustment are located underneath and are screwed into the fuel passage. When this screw is unscrewed, the mixture is enriched, and when it is screwed in, the mixture is leaned.

having adjusted the composition of the mixture, it is necessary to attempt to decrease the number of revolutions at idle by unscrewing the throttle stop screw.

A properly adjusted carburetor must provide steady operation of the engine at an idle speed of 400-500 rpm.

For checking the proper adjustment of the engine's id!, the throttle pedal should be depressed and immediately released. If the engine steps working after this, the idle arred must be increased by moving the carryretor step acres.

The sir filter is serviced simultaneously with changing the engine oil. Before servicing the sir filter, it is necessary to disessemble all the parts, clean the dirt from them, and carefully wash them out in pasoline or kerosene.

After washing, the filtering element is bathod in engine oil, and before installation of the element into place, the oil must drain down. Oil is poured into the filter bath to the bittom edge of the arrow stamped on the bath fil. Besides the arrow, the words "oil level" appear on the bath wall. If the oil level in the filter bath is higher than a set norm, excess oil will be carried into the engine by the air stream, leading to increased deposit formation and coking of the rings.

Disassembly and assembly

Fuel tanks. If leaks in the fuel tanks are discovered, the tanks must be repaired. Before repairing the fuel tanks, they must have dirt and corrosion products cleaned off their outsides, and they must be washed. The internal space of the tank is washed with a hot solution of caustic sods and water. During this process, the tank not only has the dirt cleaned from it, but gasoline fumes are also eliminated from it. After it is washed, the tank is checked for tightness. For this, all holes in the tank are closed with plugs, an air hose is connected to the drain valve nipple, and the tank is loaded into a water bath. Checking is conducted at a pressure of 0.3-0.4 kg/cm². The location of escaping air bubbles will indicate the location of a leak.

Small cracks are eliminated by soldering with soft solder. Larger cracks or perforations are repaired by laying on a patch. The ends of the cracks are drilled and the patch is soldered on with heavy solder or welded by gas welding.

Cracks in the fuel tank may also be welded by gas or electric welding. To prevent the possibility of the tank exploding from the accumulation of garoline fumes in it during welding, it is recommended that the tank be washed ent with a hot solution of caustic soda and water before welding it. For more of a protection from the possibility of the tank exploding during welding, exhaust gases of a carbureted engine are often used, filling the tank with them from a hose and spark arrester before welding the crack.

If the tank has large cracks or holes in it, it should be replaced. To remove the fuel tank from a two-axle ZIL-130 truck, it is necessary to: unscrew the coupling nuts fastening the fuel lines running from the fuel tank to the filter-sediment bowl and remove the lines, disconnect the lead from the fuel level indicator switch, unscrew the stop nuts and nuts fastening the two steel bands to the tank brackets, and remove the top steel bands and the fuel tank.

For removal of the filter-rediment bowl, it is necessary to: unscrew the coupling nuts fastening the line running to the fuel tank and the line running to the tank valve, and remove them; unscrew the nuts fastening the filter and remove the filter-rediment bowl.

For removal of the fuel tanks from a saddle trailer truck, it is eddlittenally necessary to disconnect the line connecting the two fuel tanks, unserse the two coupling note, and also disconnect the fuel level indicator switch line from the second tank.

Installation of fuel tanks on two-axis motor vehicles takes place in the reverse sequence.

Removal of the main fuel tank and filter-sediment how! from three-axle movor vehicles is the same as for two axle motor vehicles.

To remove the nutility fuel tank from the ZIL-157K motor vehicle, it is necessary to: unserew the nuts on the bridges fastening the bed to the frame and remove the bridges; unserew the nut. fastening the front and center brackets of the bed to the right frame rail; set jacks under the rear part of the bed, or connect a hoist to it, and raise the bed far enough so that it is possible to pull out the fuel tank through the gap formed between the bed and the frame. Disconnect the filler nack hose and the air vent, loosen the clamp tension screws with a screw driver, remove the fuel line running to the fuel tank, disconnect the electric line from the fuel lovel indicator switch, and then unscrew the nuts fastening the steel bands of the tank, remove the bands, and pull out the fuel tank.

For removal of the auxiliary tank filler neck, it is necessary to unscrew the nut fastening the neck bracket and remove the tank filler neck.

Installation of fuel tank, on the ZIL-137K motor vehicles takes place in the reverse sequence. On the ZIL-131 motor vehicle, the fastenings on the right and left tanks are identical.

If the valves in the fuel tank caps are damaged, the cap assembly must be replaced.

To replace defective fuel lines, besides using spares, the factory produces a pipe made of 196 tember from 1000-2000 mm long (the pipe is drawn with a diameter of 8 % 0.75, moft, (OST 617-53). Fuel lines of any dimensions for all motor vehicles can be fabricated of these pipes and the firtings for them (also produced by the factory for upara parts)

Replacement of the fuel level indicator switch. For removal of the fuel level indicator switch, it is necessary to unacrew the scrows fastening the switch, remove the switch in assembly with its float from the test, and resolve the sealing gasket.

If nucessary, unscrew the fuel valve and drain plus from the tank. A new fuel level indicator switch is installed in less receptacle in the tank with its packing gasket and fastened to it with acrows. Screw the fuel valve, angle fitting, or drain plug into the tank, and tighten with a wrench. Install the fuel filter in the tank filter nock, and close the filter neck cap, pressing it down by hand and rotating is to the right.

It is recommended that the B-9 and B-95 fuel purps be disassembled in the following sequence. If necessary, unserse the fittings: 1) the fuel supply fitting from the cover, and 2) the fuel obtiet fitting from the pump head. Unserew the screws fastening the head to the pump body and remove the head, carefully separating the pump disphragm.

Unscrew the two screws fastening the cover to the purp head, recover cover, cover packing pasket, and screened filter.

The filter may also be removed without removing the pump head.

For rest alof the valves, it is necessary to press out the valve rods (Piato 5-22, a), remove the band, valve, and valve spring. The valve unit should not be disassembled except in extreme necessity.

For resoval of the diaphragm with its pull rod, it is necessary to pressout the pump arm shrft, withdraw the pump arm from the body, and remove its return spring from it. Pull the diaphragm in assembly with its rod and diaphragm spring out of the body.

To extract the manual pump drive shaft, it is necessary to free the manual pumping handle from its spring and withdraw the shaft together with the spring.



Plate 5-21 Adjusting the idle on a K-88 and K-88A carburetor (for position designations, see Flate 5-20).

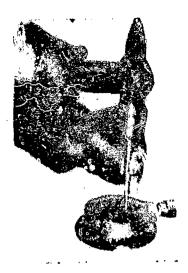




Plate 5-22. Disassembly of the fuel pump units:

a) pressing out the valve rod

b) unscrewing the draphrogm fastening nuc

For disassembling the pump diaphragm, it is necessary to fasten the diaphragm rod in a vise (a hand vise can be used) with soft inserts, unscrew the nut fastening the diaphragm to the rod (Plate 5-22, b), remove the spring washer, the upper compression washer, the diaphragm, the lower diaphragm washer, and the pull rod washer.

The two support washers of the pump arm which are fitted onto the pull rod and fastened by clenching the end of the rod are removed only when they are to be replaced.

Assembly of the B-10 and B-10B pumps is similar to the assembly of the B-9 and B-9B pumps.

Checking the fuel pump parts. After disassembly, the parts of the fuel pump should be checked for usability. There must be no burrs, holes, dents, cracks, or corrosion on the body, head, or parts of the pump.

The diaphragm linen must not be torn or damaged.

Wear on the working surface of the lever which rubs against the camshaft eccentric is not allowed to be greater than 0.2 mm, and wear on the lever in contact with the diaphragm pull arm must be no greater than 0.5 mm. If wear is greater on these surfaces, the lever must be replaced.

The pump diaphragm spring is tested for elasticity on a CARO model 357 device (Plate 5-25). The spring being tested is mounted on the stock of the

device, and its height is measured along a scale without a load and with a load. The scale indications must correspond to the characteristic presented in Table 5-5.

In checking the outlet valves of the B-9 and B-9B pumps of the first series, it is necessary to remove the head from the pump body, and then remove the head cover. When checking the outlet valves of the B-10 pump, only the head cover is removed, without removing the head from the pump body.

Fuel pump assembly. Assembly of all fuel pumps is identical. During assembly, it is necessary to assemble the dior ragm, for which: a washer, lower pressure washer, diaphragm plates (have lighted their holes), and upper washer are mounted on the pull rod, the with the pull rod gripped in a vise (see Plate 5-22, b), the diaphragment is identical. During assembly, it is necessary to assemble the dior ragm, for which: a washer, washer, and upper washer are mounted on the pull rod, the diaphragment is identical. During assembly, it is necessary to assemble the dior ragm, for which: a washer, and upper washer are mounted on the pull rod, the diaphragment is identical.

Insert the diaphragm spring in the pump body and install the diaphragm in assembly with its push rod. Then insert the manual drive shaft in the hole in the body, install the spring on the shaft and fasten it.

Install the pump arm in the bady, connect its forked end with the diaphragm pull rod, install the return spring, and fasten the pump arm by its shaft, pressing it into the hole in the body.

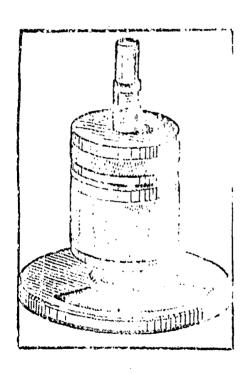
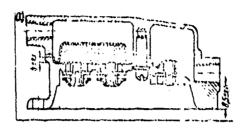
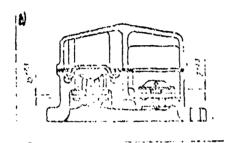


Plate 5-23. GARO model 357 device for checking diaphregm springs





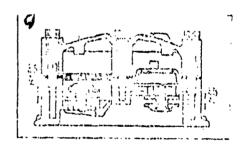
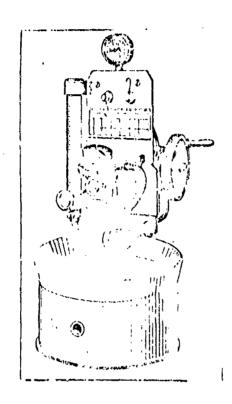


Plate S-24. Installation of fuel pump valves:

- a) B-9B
- b) B-9
- c) B-10 and B-10B

Assemble the head body, for which the inlet and outlet valves are installed, fastening them with rings. For the outlet valve of the B-9B fuel pump, the distance from the face of the band rod to the surface of the head body must be within the limits of 8.4-8.6 mm (Plate 5-24, 4). For the inlet valves of the B-9B pump, distance from the face of the band rod to the assembly surface of the pump cover body must be within the limits of 3.9-4.1 mm.

For the B-9, B-10, and B-10B fuel pumps during installation of the valves, the distance between the valve and ring is measured and must be within the limits of:1 1.5-1.8 km for the inlet valves of the B-9 pump, 2.0-7.3 km for the outlet valves of that pump (Plate 5-24, b); 0.65-1.45 km for the inlet valves of the B-10 and B-10B pumps, and 1.15-1.95 km for the outlet valves of that pump (Place 5-24, c).



Place 5-25. GARO model 374 device for checking fuel pumps

Install the screened filter on the injet valves and fasten the cover with its gasket. The assembled head is installed on the body, the fastening bolts are screwed in by hand, and the diaphragm is dropped downward by moving the lever (arm). Tighten the head in this position.

Screw in the fittings in the head and cover, and screw the threaded plug with its gasket into the control aperture in the body if the plug was unscrewed during disassembly.

It is recommended that fuel pumps be tested on a GARO model 374 device (Plate 5-25). Pressure developed by the pump and its capacity are checked on the device (data is presented in Table 5-2 and in the text).

Disassembly of the K-84M carburetor. Unscrew the screws fastening the cover, unscrew the central screw with a screwdriver, remove it together with the fiber washer, and remove the cover (Plate 3-26, a).

Пружина	. Восота пржини		Числувита в пружния		Anonesp	
	бе і нагрузки	с илгоузкой	AC&bii	[ब र्क स्थल ४	пружины	праводуки
⁶ Пружинг дилфрагмы ¹ насосов Б-9 и Б-9 Б	48-49	28,5 (apa narpyake	5,5-0,5	3,54,5	24	1,8
Пружина диафрамы пасосов В 10 и Б-10Б	50 51	26,5	67	4-5	24~	
^{зв} Пружина каппана ⁹	911	9,5-10,3 κΓ)	,5-8.5	5,5-6,5	7,3-7,7	0,4

Key:

a) spring

c) without load

d) with load

- e) number of spring coils
- b) spring height f) total

 - g) working h) diameter

- i) spring
- j) wire
- k) B-9 and B-9B pump diaphragm spring1
- 1) B-10 and B-10B pump diaphragm spring
- m) valve spring2
- n) (with a load of 5-5.6 kg)
- o) (with a load of 9.5-10.3 kg)

1 Diaphraga manufactured of lacquered fabric.

2 After compression to 4.5 mm, the spring must have no residual deformation.

When the central screw is being withdrawn from its receptacle and the cover is being removed, it is necessary to remember that the accelerator pump needle valve is not fastened and may fall from its receptacle.

To extract the needle valve from its receptacle, it is necessary to tilt the body and, placing the hand against the receptacle, remove the valve, as shown in Plate 5-26, b.

Disassembly of the cover. Carefully grasp the cover in a vise with soft jaws, unscrew the fuel feed fitting, unscrew the fuel food valve filter plug, remove it together with its gasket, and remove the screened filter from the valve space. Unscrew the fuel feed valve body (Piato 5-26, c) and remove it in assembly with the valve, packing, and adjusting gaskets (the valve in assembly with the needle and sent is pressed into the valve body and is not disessembled).

Remove the choke drive spring with a screwdriver. Unscrew the screws fastening the choke to its shaft, remove the choke in assembly with the reverse valve, withdraw the choke drive shaft from the body in assembly with its pressure screw and drive cable clump.

Unscrew the bolt fastening the caple clamp bracket and remove the bracket in assembly with the cable clamp.

Disassembly of the float chamber body. Remove the gasket from the body, carefully separating it from the corburetor body wurface with a screwdriver.

Unpin the accelerator pump red, disconnect the red from the drive lever, pull the bracket out of the hole for the lever and pump red, and remove the assembled accelerator pump body from its cavity..

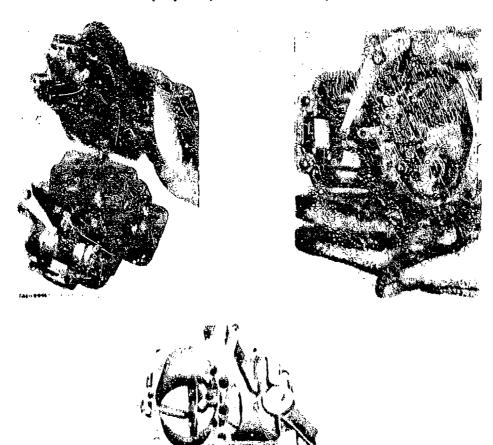
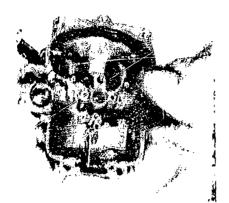


Plate 5-26. Removal and disassembly of the K-84M carburetor cover:

a) cover removal b) extracting the accelerator pump needle valve c) unscrewing the fuel feed valve body



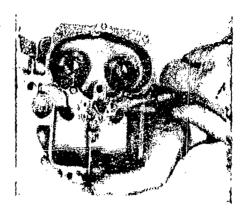




Plate 5-27. Removal of the K-84M carburetor jets: a) removal of the main jet b) removal of the idle jet c) removal of the air jet

Remove the float and its shaft, the mechanical economizer valve rod, the pneumatic economizer, the economizer piston spring, and if necessary, extract the packing gasket of the piston.

With a screwdriver, unscrew the two main jets Plate 5-27, a), the two idle jets (Plate 5-27, b), and the valve body of the economizer with pneumatic drive. Unscrew the two air jets (Plate 5-27, c) with a wrench. In case of extreme necessity, remove the lock ring with a screwdriver and pliers, and take out the accelerator pump injet ball valve.

Unscrew the plug (Piate 5-28, a) from the valve passage of the economizer with mechanical drive, unscrew the economizer valve assembly (Plate 5-28, b), and if necessary remove the packing gasket. The valve seat is pressed into the body inwhich the spring and mechanical economizer valve are located, and therefore this unit is not disassembled.

Unscrew the plugs from the passages in the body, then the high speed jets. For separation of the float chamber body from the lower part of the carburetor, it is necessary to loosen the fastening bolts with a wrench and then unscrew them with a screwdriver. Remove the mixing chamber body (Plate 5-29, a), lightly tapping on it with a wooden hammer, and then remove the insulating gasket, separating it from the body with a screwdriver (Plate 5-29, b).

Disassembly of the accelerator pump. Remove the stop ring fastening the piston rod to the drive rod plate with a screwdriver, disconnect the lever with the drive rod from the pump piston rod, and then remove the spring and spring support washer from the piston rod, after which the piston (rubber cuff) and piston compression spring are removed from the rod.

Disassembly of the mixing chamber. Unscrew the fitting from the vacuum regulator pipe and the two idle adjusting screws.

For removal of the throttle plate shaft, it is necessary to unscrew the screws fastening the plate and remove the shaft in assembly with its drive lever

After disassembling the carburetor parts, wash them in acetone, a solution based on acetone, or in clean gasoline, and the passages, jets, and all parts and units of the carburetor are blown out with compressed air. The painted surface of the mixing chamber body must be washed only in gasoline, since acetone will dissolve the paint protecting the body from corrosion.

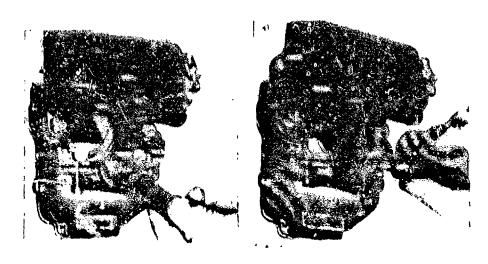
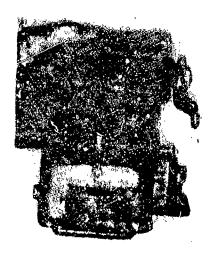


Plate 5-28. Removal of the economizer valve of the K-84M carburetor:

a) unscrowing the valve plug of the economizer with mechanical drive b) unscrowing the valve of the economizer with mechanical drive



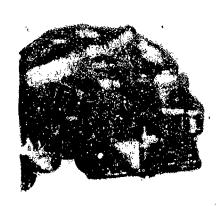


Plate 5-29. Removing the lower part of the carburetor:
a) removing the lower part of the carburetor b) removing the insulating gasket

Checking float tightness. Before setting about checking and adjusting the fuel level in the carburetor float chamber, it is necessary to insure the proper condition of all the float mechanism parts.

Tightness of the float is checked by immersing it in hot water at a temperature of 60-80°C and holding it there for a period of no less than 0.5 minutes. If the float seal is destroyed (escaping air bubbles appear on it), it must be soldered, after first removing all the fuel from it. After soldering, the float should again be checked for tightness and weight.

The weight of the float in assembly with its lever must correspond to the data presented in Table 5-4. If, after soldering, the weight of the float exceeds that allowable, it is necessary to remove excess solder and bring the weight of the float to the required amount in this way, without destroying its hereatic state.

The floar chamber needle valve is to check for tightness on θ special installation (Plate 5-30).

Creating a suction of 1000 mm in a water column from the water level in tank 1, and, having closed valve 7, check the rightness of the valve.

The allowable amount of water drop in the column over a period of 0.5 minutes must be no greater than 10 mm on scale 3. Lapping the needle into its seat is allowed to obtain the seal. If tightness is not achieved by these means, the needle valve unit must be replaced.

Installation of the valve on the cover of the carburetor is checked with a template (Plate 3-51, a). The distance from the upper point of the needle valve rod sphere to the surface c? the carburetor cover must be equal to 13.2-13.8 mm for the K-84M, and 13.5-13.8 mm for the K-88 and k-38A (Plate 5-31, b). If necessary, adjunt the installation of the valve with gaskets.

Checking the passage capability of the carburetor metering elements. Plate 5-37 shows one of the possible layouts of a device for checking the passage capability of the metering elements (jets, atomizers) for a period of time by means of the absolute usage of water.

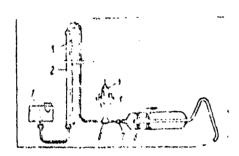


Plate 5-30. E agram of installation for checking float chamber needle valve tightness:
1) tank 2) glass tube
3) graduated scale 4) needle valve 5) body 6) tee
7) valve 8) piston

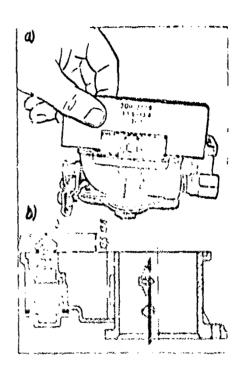


Plate 5-31. Checking installation of the float chamber valve: a) checking valve installation with a template b) installation dimensions of the fuel feed valve 1) upper body of the carburetor 2) valve body 3) gasket

Passage capability, $cm^3/\sin ute$, of the metering elements, in checked by determining the time for a flow of water through it at a temperature of 19-11°C at a pressure equal to 1000 + 2 mm in a column of water.

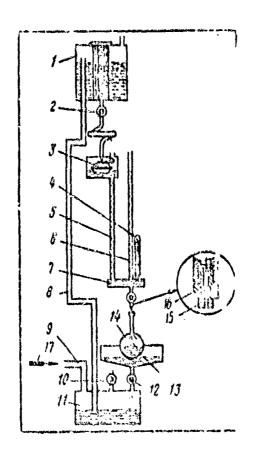


Plate 5-32. Diagram of device for checking passage capability of carbureter metering elements:

- 1) upper tank 2, 10, 12) valves 3) float chamber 4) thermometer 5, 6, 8, and 9) pipes
- 7) body 11) lower tank 13) trough (4) measuring
- flusk 15) metering element 16) holder 17) direction of compressed air feed

Water flows from the upper tank I through valve 2 into the float chamber 3, in which a constant water level is maintained. From float chamber 3, water flows through tube 5 into body 7, which is raised along glass tube 6 to a determined height, and simultaneously flows through the tested metering element 15, which is fastened into helder 16.

Water flowing through the tested metering element flows into trough 13, and from there through value 12 into the lower tank 11. Mater can flow as needed from the lower tank to the upper tank 1 along pip. 3 under the force of compressed air incroduced through pipe 9, during which values 10 and 12 must be closed. After the upper tank 1 is filled, values 10 and 12 must be

open. The water column must be equal to 100 mm.

Temperature of the water flowing out is checked by thermometer 4.

After the measuring vessel 14 (usually a measuring flask with a high small diameter neck) has been set beneath the strasm of water flowing out, and the time of its filling has been measured in seconds, it is possible to determine the passage capability of one or another metering element at a given water pressure. For this, it is necessary to divide the quantity of water in the measuring vessel (in cm³) by the time elapsed to fill the vessel (in seconds), and multiply the result obtained by 60, to give the passage capability in cm³/minute.

The neminal passage capability of various metering elements of the carturetor are presented in Table 5-4.

for normal operation of the carburetor, it is also necessary to check the tightness of the valve of the economizer with mechanical drive. Checking may be conducted on the installation shown in Plate 5-30.

Assembly of the K-84M carburetor. Assembly of the carburetor takes place in the reverse sequence, fastening the units and parts with the same tools used during disassembly.

buring assembly, it is necessary to ensure that there is no hanging or wedging of the economizer valves, accelerator pump, choke, or throttle.

The clearance between the choke and the mixing chamber body must be no greater than $0.05~\text{mm}_{\odot}$

Checking and adjusting the moment of the mechanical drive economizer value opening. After installing the accelerator pump drive, it is necessary to check and possibly adjust the moment of opening of the mechanical drive economizer valve. The distance between the edge of the throttle and the wall of the mixing chamber at the moment that the economizer valve opens must be 9.0 mm for the K-84M carburetor. This distance may be measured by a template or a special measuring instrument. If there is a deviation from this value, adjustment must be conducted by means of bending the accelerator pump rod bar on the K-84M carburetor. The bar is bent only on a section of 30 mm (Plate 5-33).

Checking carburetor tightness. Tightness of the carburetor may be checked on a special GARO meddel 355 device (Plate 5-34) for checking carburetors. The carburetor being checked, 5, is installed on bracket 7 and is pressurized by means of supplying fuel to it at an excess pressure of 0.2 kg/cm² from tank 13 along pipe 3 and hose 2. Pressure in the system is created by pumping air into the tank of the device through reverse valve 12 by a hand pump or from a pneumatic power system. Maximum pressure in the tank is limited by

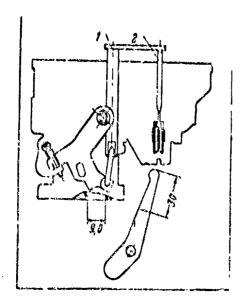


Plate 5-33. Diagram of adjusting the moment of the mechanical drive economizer valve opening: 1) bar 2) pull rod

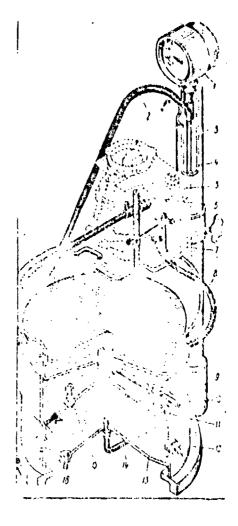


Plate 5-34. GAPO model 355 device for checking carburetors:

- 1) manometer 2 and 8) rubber hoses
- 3) fuel feed line 4) device stand
- 5) tested carburetor 6) control pipe 7) bracket 9) bath 10) valve handle
- 11) valve 12) roverse 13) tank
- 14) filler valve 15) safety valve 16) observation port

safety valve 15, which is adjusted to a pressure of 0.5 kg/cm2. The tank is filled with fuel shrough valve 14, during which it is necessary to lower air pressure in the tank beforehand, for which it is connected to the atmosphere through valve 11. Valves 14 and 11 are blocked together so that in the esignning, with the rotation of handle 10 by 90°, valve 11 opens and releases air from the tank, and then with a rotation of the handle by another 90°, valve 14 opens, connecting the tank with bath 9, intended for supplying fuel to the device tank. Fuel level in the tank is checked through observation port 16. Fuel level in an assembled carburetor may be checked on the same model 355 device. For this, the plug covering the machanical drive economizer valve passage is unscrewed, and a fitting with rubber hose 8 is screwed in its place. Rubber hose 8 ends with a glass tube 6 which has two tanks on it, indicating the limits of fuel level deviation. With the proper position of the float, the fuel level in the carburetor float chamber with an excess fuel pressure in front of the needle valve of 125-170 mm in a column of mercury must be 18-19 mm from the upper assembly plane of the carburetor.

To attain the proper value of fuel level in the float chamber, the float bracket may be bent.

Checking the accelerator pump mechanism. Using the fuel supply into the carburetor float chamber from the model 355 device, check the operation of the piston mechanism, which must work reliably and provide a capacity of no less than 17 cm³ for ten full strokes of the piston at a rate of 30 pumps per minute.

The throttle plate lever must be pumped from the fully closed to fully opened positions of the plate.

The quantity of fuel is determined by measuring it with a vessel.

Before star'ing resurement, stroke the pump several times to ensure that it works.

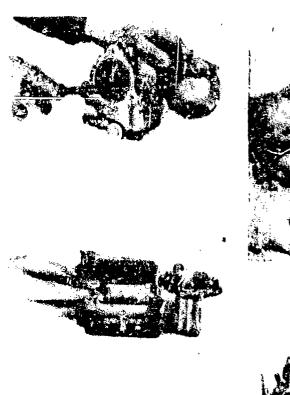
Disablembly order of the K-88 and K-88A carburetors is similar to the disassembly order for the K-84M carburetor, and therefore only the differing operations are presented below.

Plate 5-35, a, shows the unscrewing of the central hollow screw, removal of the upper body of the cover (Plate 5-35, b), gasket (Plate 5-35, c), and float (Plate 5-35, d) of the K-88 carburetor.

Plate 5-36, a, shows removal of the accelerator pump and pneumatic economizer mechanisms (Plate 5-36, b), as well as the removal of the mechanical economizer valve plunger (Plate 5-36, c) of the k-88 carburetor.

Piste 5-37, a, shows the unscrewing of the pneumatic drive economizer valve body, and Piste 5-37, b, c, and d, show unscrewing of the lets from the K-18 carburetor. The float chamber body and insulating gasket of the K-88 and K-88A carburetors are then removed from the mixing chamber body.

Removal and disassembly of the diaphragm mechanism. Unsersw the bolts (Plate 5-38, a) fastening the side cover of the lever mechanism, and remove the cover with its gasket. Remove spring 1 (Plate 5-36, b) from the lever pin 2 and pin body with a screwdriver, unpin red 4 of the diaphragm, separate it from the lever 2, unscrew fastening nut three on the throttle plate shaft, and remove the lever. Unscrew screws 5 fastening the body of the diaphragm



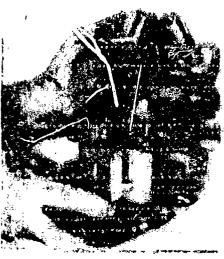




Plate 5-35. Removal of the cover and disassembly of the K-88 carburetor:

- a) unscrewing the central screw b) removing the cover
- c) removing the bedy gasket d) removing the float

mechanism to the body of the mixing chamber, disconnect the body and remove the body gusket, remove the compression spring of the collar and carefully pull the bearing collar from its receptacle.

For removal of the diaphragm, it is necessary to unserew the screws (Plate 3-58, c) fastoning the upper cover to the diaphragm mechanism body, remove the cover, and pull out the diaphragm assembled with the rod 4 from the bedy (see Plate 5-38, b).

The diaphragm unit is not disassembled, since the diaphragm is compressed between two washers and fitted on a rod whose end is crimped.

Assembly of the N-88 and K-88A carburetors. After checking the components and parts, assemble the c. source in the following order. Assembly of the mixing chamber body. Insert the shaft with the forked hinges throttle actuator into the actuator body. The shaft must rotate freely in the body bushing with a clearance of 0.035-0.143 mm.

Insert the ball bearings into their receptacles in the body and fasten one bearing from the side of the actuator with a locking ring. Insert the throtile shaft in the body and fasten both throttle plates onto the shaft with screws. Install the gasket and the ucluator body with the forked shaft and fasten it with screws. Install the connecting lever shaft and the throttle actuator lever on the end of the forked shaft with a support screw, and fasten them with a nut.

Screw the two idle adjusting screws and one support screw into the hody after mounting springs on them.

Assembly of the diaphragm mochanism. Insert the diaphragm with its rod into the mechanism body. Install the top cover and fasten it on with screws.

Screw the air and vacuum jets into the mechanism body. Insert the collar and spring into the bearing receptable. Install the diaphragm mechanism body with its gasket in the mixing chamber body and fasten it with screws. Install lever 2 (see Plate 5-58, b) of the diaphragm mechanism on the throttle plate shaft and fasten it ith a nut. Connect the lever with the rod 4 of the diaphragm and fasten the rod with a cotter key. Mount a spring on the lever pin and on the body pin.

Install the side cover of the lever mechanism with its gasket and fasten it with screens (see Plate S-38, $^{\circ}$).

Assembly of the float chamber body of the K-6P and K-88A carburetors (see Plate 5-35, 5-36, and 5-37), assembly, installation, and checking of the accelerator pump, connecting and fastening the float chamber body to the gixing chamber body, and assembly, installation, and fastening of the cover (see Plate 5-55, a, b) trke place the same as in the K-84M carburetor.

During installation of the acc levator pump and connecting rod to the linkage, it is necessary to connect the li kape rud, faston it with screws, and cinch the screws with stop plates.

After assembling the carburetor, install the rod connecting the choke and throttle plate levers.

The carburator is checked for tightness. The K-88 and K-80A carburators are checked for tightness on an instrument in same as that for the K-84M.

Disassembly of the engine revolution gormnor (K-84M carburetor). Remove the seal, unscrew the screws fastening the front and side covers, and remove them with their gaskets.

If necessary, carefully remove the two jets (upper air and lower vacuum) from the diaphragm mechanism body with a screwdriver.

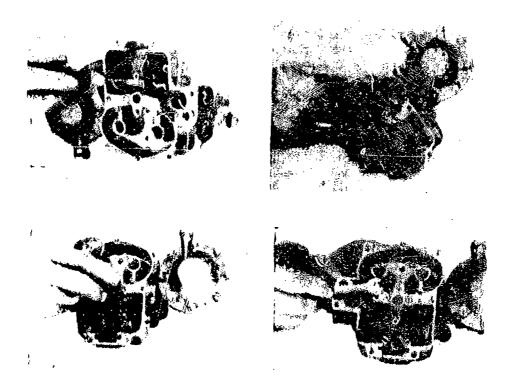
Disassembly of the mixing chamber. Unscrew the nut fastening the throttle drive lever and the connecting lever, and remove the levers. Unscrew the screws fastening the drive body and the bearing, remove the body together with the forked control shaft, and remove the shaft from the body.

To extract the throttle shaft, it is necessary to remove the stop ring of the bearing from the side of the control and press out the shaft. Extract the two ball bearings from the mixing chamber body by hooking them with a curved metal rod (the bearings six in their receptacles freely). If necessary, unserew the idling system adjusting screws and stop screw.



Plate 5-36. Removal of float chamber parts of the K-88 carburetor:

- a) extracting the accelerator pump and rod
- b) removing the pneumatic economizer mechanism
- c) removing the mechanical economizer plunger



Piato 5-37. Removal of jets from a K-88 carburetor:
a) unscrewing the preumatic drive economizer valve body b) unscrewing the main jet c) unscrewing the idle jet d) unscrewing the air jet

Checking the basic corponents of a carburetor. Before checking an assembly, all parts, assemblies, and passages of the carburetor are washed out in acetone or clean kerosene, and the throttle drive body is blown our with compressed air. If a bushing is worn so that its clearance is increased to a dimension of more than 0.143 mm, it is necessary to replace the drive body in assembly with the bushing or drill the worn bushing out of the body, renew the hole to its nominal dimension of 10.4-10.435 mm, and press in a new bronze bushing with the interference of 0.055-0.080 mm.

After the bushing has been pressed in, its interior diameter should be reamed out to a nominal dimension of 8.0-8.058 mm (nominal dimension of the shaft with the forked hinged throttle actuator is 7,915-7.965 mm).

Tightness of the float and the assembled float chamber needle valve and passage capability of the metering elements of the K-88 and K-88A carburetors are checked the same as the K-84M carburetor.

Assembly of the K-88 and K-88A carburetors. After checking the components and parts, assemble the carburetor in the following order. Assembly of the mixing chamber body. Insert the shaft with the forked hinges throttle actuator into the actuator body. The shaft must rotate freely in the body bushing with a clearance of 0.035-0.143 mm.

Insert the ball bearings into their receptacles in the body and fasten ene bearing from the side of the actuator with a locking ring. Insert the throttle shaft in the body and fasten both throttle plates onto the shaft with screws. Install the gasket and the actuator body with the forked shaft and fasten it with screws. Install the connecting lever shaft and the throttle actuator lever on the end of the forked shaft with a support screw, and fasten them with a nut.

Screw the two idle adjusting screws and one support screw into the body after mounting springs on them.

Assembly of the diaphragm mechanism. Insert the diaphragm with its rod into the mechanism body. Install the top cover and fasten it on with screws.

Screw the air and vacuum jets into the mechanism body. Insert the collar and spring into the bearing receptacle. Install the diaphragm mechanism body with its gasket in the mixing chamber body and fasten it with screws. Install lever 2 (see Plate 5-38, h) of the diaphragm mechanism on the throttle plate shaft and fasten it with a nut. Connect the lever with the rod 4 of the diaphragm and fasten the rod with a cotter key. Mount a spring on the lever pin and on the body pin.

Install the side cover of the lover mechanism with its gasket and fasten it with screws (see Plate 5-38, a).

Assembly of the float chamber body of the K-88 and K-88A carburetors (see Plate 5-35, 5-36, and 5-37), assembly, installation, and checking of the accelerator pump, connecting and fastening the float chamber body to the mixing chamber body, and assembly, installation, and fastening of the cover (see Plate 5-35, a, b) take place the same as in the K-84M carburetor.

During installation of the accelerator pump and connecting rod to the linkage, it is necessary to connect the linkage rod, fasten it with screws, and cinch the screws with stop plates.

After assembling the carburetor, install the red connecting the choke and throttle plate levers.

The carburetor is checked for tightness. The K-88 and K-88A carburetors are checked for tightness on an instrument the same as that for the K-84M.

Disassembly of the engine revolution governor (K-34M carburetor). Remove the seal, unscree the screws fastening the front and side covers, and remove them with their gaskets.

For removal of the regulating unit parts (adjusting screw and nut, and the spring and rod), it is necessary to partially unscrew the adjusting nut 4 (see Plate 5-16) so that rod 2 can be freely removed from the rod of the shaped lug 1. After this, the parts of the regulating unit are removed from the passage of the body in assembly.

To remove rod 8 with its piston 7, it is necessary to unscrew the screws fastening the throttle plates, withdraw the plate pin from the slot in the fod, remove the plate, and then pull the red and piston from the cylinder in body 11.

Pu'l shaft 13 with lug 1 and the meedle bearings 14 from their recess, and knock out (if necessary) the plug room the bearing receptacle.

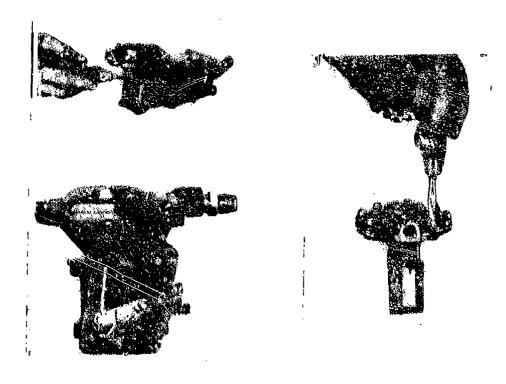


Plate 5-38. Disassembly of the engine revolution governor disphragm mechanism:

a) removing the lever mechanism cover b) diaphragm mechanism from lever mechanism side c) removal of diaphragm cover

1) spring 2) lever 3) nut 4) diaphragm rod 5) diaphragm mechanism body fastening screw

For removal of the regulating unit parts (adjusting screw and nut, and the spring and rod), it is necessary to partially unscrew the adjusting nut 4 (see Plate 5-16) so that rod 2 can be freely removed from the rod of the shaped lug 1. After this, the parts of the regulating unit are removed from the passage of the body in assembly.

To remove rod 8 with its piston 7, it is necessary to unscrew the screws fastening the throttle plates, withdraw the plate pin from the slot in the fed, remove the plate, and then pull the rod and piston from the cylinder in body 11.

Pull shaft 13 with lug 1 and the needle bearings 14 from their recess, and knock out (if necessary) the plug from the bearing receptacle.

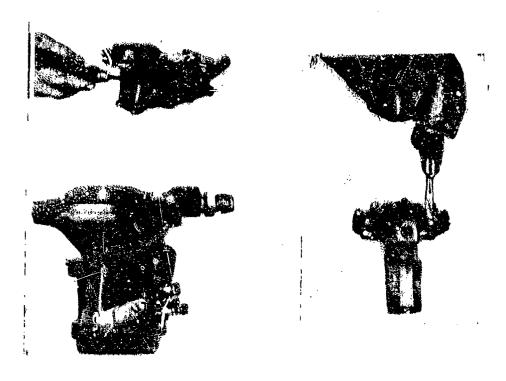


Plate 5-38. Disassembly of the engine revolution governor disphragm mechanism.

- a) removing the lever mechanism cover b) disphragm mechanism from lever mechanism side c) removal of disphragm cover
- 1) spring 2) lever 3) nut 4) disphragm red 5) disphragm mechanism body fastening screw

Assembly. Assembly should take place in the following order: lubricate the bearings with 1-13c grease, insert the shaft with its needle bearings and formed lug in its recess and press in the plug.

Install the piston and rod in their cylinder, set the plate with its pin on the shaft, connect the rod slot with the plug pin and fasten it on its shaft with scrows. Install the second plate on the shaft and fasten it with scrows.

Insort the regulating unit parts in the body passage with the bent end of the spring going into the slot in the body passage. After mounting the spring on the lug pin, connect the spring to the shaped lug. Having previously screwed in the adjusting nut, tighten the spring.

Install the side cover with its gasker on the body, and fasten it with screws. The front cover is installed and fastened after it has been checked and the governor adjusted.

The revolutions governer is checked and adjusted on the engine or on a special installation. During adjustment, it is necessary to remember that: the stronger the spring tension, the higher the number of engine revolutions at which the governor will trigger, and conversely, the lower the spring tension, the lower the number of engine revolutions at which the governor will trigger.

A properly adjusted governor must trigger at 2600-2750 engine crankshaft rpm.

Plate 5.39, a, shows a GARO model 419 device for checking the revolution governor adjustment, and Plate 5-39, b, shows the schematic of the device.

The revolution governor 2 is fastened onto the ascombly surface 9 and arrow 12, which has sma 10, is installed on place 8 of the governor.

After this, the movable scale body is retated so that the end of the arrow coincides with the zero degree division.

Elasticity of apring 3 of the governor is checked according to deviation of arrow 12 when load 11, weighing 100 grams, is hung at points 11 and 111 of arm 10. With this, the information received is compared with the data on plate 13, which is fastened onto the device.

The governor is adjusted by changing the tension on its spring with screw handle 7. Rotating the charse adjustment screw 5, a preliminary setting is achieved, and rotating hellow bodied screw handle 5 into nut 4, a fine adjustment is achieved, performing the final setting of the revolution governor.

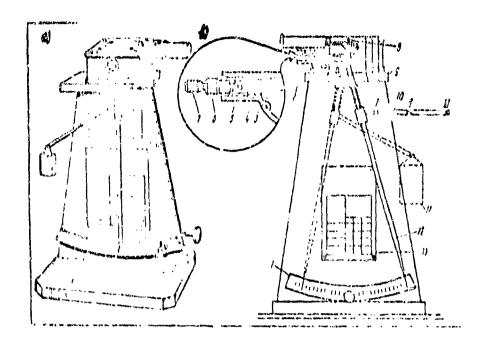


Plate 5-39. GARO model 419 device for checking a maximum revolution governor of an in-line engine:

- a) device in acsombly b) device schematic 1) scale
- 2) revolution governor 3) governor spring 4) governor fine adjusting nut 5) governor coarse adjusting screw 6) hollow bodied screw handle 7) screw handle 8) governor plate
- 9) device assembly surface 10) arrow arm 11) control weight
- 12) arrow 13) plate with adjusting data

The revolution governor of the k-88 and K-88A carburetors. The engine revolution governor consists of two mechanisms: the centrifugal switch installed on the cambhaft gear cover, and the diaphragm mechanism installed on the mixing chamber of the capturetor.

The contribugal switch is disassembled and assembled separately from the disphragm mechanism, but adjusted together with it.

Disassibly of the contribugal switch is not recommended unless it is needed. During repair, the contribugal switch must be disassembled in the following order.

the screw the acrews fastening cover 19 (ace Place 5-17), remove it from the best in assembly with seal 18, remove the seal from the cover, and if necessary remove the gasket.

Remove rotor 22 in assembly with its support washers from the body, and then remove the washers from the rotor.

For disassembly of the rotor, it is necessary to remove the stop ring fastening the valve seat with a scrowdriver, and then knock out seat 28 of the valve, lightly tapping the rotor on a wooden object. Then, if necessary, remove gasket 16 of the seat.

Rotating the adjusting screw handle 20 to the last, free spring 14 from the threaded screw (the end of the apring which is decreased in diameter is a thread for the adjusting screw). Unscrew velve 27 in associally with the spring (the adjusting screw does not apparate from the spring, since it is rolled into the body of the rotor) and separate the spring from the valve.

For disassembly of the writch body, it is necessary to unscrew plug 21 with its gasket from the hole for setting the switch spring, and then unscrew the lubrication fitting with its gasket and pull out wick 23 with a screw-driver or metal rod with a best and.

Unacrew the almove of the pipe connecting the diaphrage mechanism from the body and the sleeve from the pipe connecting the above-throttle space of the carbureter.

If necessary, press the metal-coramic bushing 24 of the rotor axis out of the body.

Checking. The switch valve must fit against its sent along its entire circumserence. Valve lapping is permitted. A lapped-in valve is checked for tightness with a vacuum of 1000-1100 mm in a water column for a period of one minute. With a valve wet in gasoline, a pressure drop is not allowed.

The internal aimension of the rotor shalt bushing must be 13.0-13.035 mm. The neminal dimension of the rotor shaft is 12.93-12.95 mm.

If wear is present, the bushing and shaft must be replaced. A new bushing is pressed in with an interference of 0.005-0.040 mm and is fitted according to the shaft diameter with a clearance of 0.055-0.105 mm.

The cover seal must be in good condition. The sharp edges of the seal rubber must not have signs of stretching. The threads in the holes for the sleeves must be in good condition.

Assembly of the centrifugal switch. Switch assembly takes place in the reverse order from disassembly.

Having installed the valve and spring, seet and gasket, and fastened them with a top ring in the rotor, assemble the rotor. The rotor valve must freely move in the guide.

Mount the spacing washer on the rotor, install it in the body, having guided the shaft into the rotor bushing, and meunt the support washer.

Insert the rubber casing seal in the cover, set the cover on the body with its gasket, and fasten it with screws.

Soak the felt wick in engine oil, with the excess oil being allowed to drain off.

Adjusting the centrifugal switch. In the process of operation, the centrifugal switch valve spring might lose its elasticity, and the governor will cut in at a lower number of engine revolutions, as a result of which the maximum speed of the motor vehicle will be decreased.

Therefore, the assembled contrifugal switch must be checked, and if necessary, adjusted so that it, in connection with the diaphragm mechanism, will cut in at the assigned maximum number of engine crankshaft revolutions.

Checking and adjusting the contribugal switch should be done during the process of testing the engine on the stand after overhaul.

For adjusting, the tessed contrifugal switch is installed on the engine and fastened with bolts. After starting the engine, with fully opened throatles, check the number of angine crankshaft ravolutions at which the centrifugal switch must cut in on the tachemeter. The switch must cut in at 3100 engine crankshaft rpm. If the switch cuts in at a higher or lower number of ravolutions, it is necessary to step the engine, and then, without removing the switch from the engine, unacrew plug 21 and adjust the rotor by turning the adjusting screw 20 with a screwdriver and changing the tension on spring 14.

When the screw is turned to the right, the switch rotor spring tension is increased, and when it is turned to the left, the spring tension is decreased respectively increasing or decreasing the number of engine crankshaft revolutions at which the switch begins to cut in.

After adjustment, the plug should be screwed into the hole in the switch body, the engine should be started, and the result of adjustment coacked.

Having finished adjustment, remove the contribugal switch from the stationary engine, seal it, and ship it for installation on a motor vehicle engine.

Section III. Transmissions

Gapter 6. The Clutch

Layout

The single-disk clutch of the ZIL-130, ZIE-157K, and ZIL-131 motor vehicles (Plate 6-1) provides transference of a twisting moment of up to 41 kg maters.

The pressure plate 8 in assembly with the cover 3 is fustaned to the flywhest with eight centering belts having a body diameter of 10.000-9.942 mm and a shoulder length of 12.5 mm. The twisting assent is transmitted from the clutch cover to the driven disk through pressure plate 8 by four pairs of spring plates 5.

Four levers 30 are fastened onto the pressure plate on brackets, and, resting on their center parts, rotate on pins 25, which are sounted on the support forks 27. The support forks are fastened to the cover 3 with adjusting nuts 28. To decrease friction, the lever pins and forks work on needle bearings 26, which are packet with grease during assembly of the clutch.

The pressure force of the clutch is created by 16 springs, which are installed between the clutch cover and the pressure plate. Insulating washers 9 are jaid beneath the pressure plate aide of the springs. The pressure plate and cover assembly are statically balanced to an accuracy of 90 gram cm.

The driven dist is heel, with riveted friction plates and hub 15, and has a friction type horque vibration damper consisting of eight springs with supporting plates and two damper disks. The driven disk assembly is statically balanced to an accuracy of 25 gram cm.

The clutch throwous bearing is of closed construction. It is packed with grouse only during its assembly at the factory.

During disengagement of the clutch, bearing 52 of the sleeve presses against the inner ends of the four levers 30, and the outer ends, transfering the force to the pressure aprings 10, withdraw the pressure plate 8 from flywheel 2.

A packing gasket is installed between the clutch housing and its cover on the ZIL-131 motor vehicle. A packing gasket is also installed beneath the flange of the clutch disengagement fork. Both gaskets are installed with sealing pasts (VTU MKRP 3336-52). The front and rear faces of the clutch housing are pasked with the same paste during assembly of the power unit. To seal the clutch disengagement forks, rubber rings are installed on their journals can both sides.

A special regimene shield is located on the lower part of the front face of the clutch housing and covers the opening in the clutch housing. The shield is fastened to the clutch housing with two bolts and is pressed against the lower surface of the cylinder block by a rejection on the front part of the clutch housing cover. During assembly, t is necessary to first screw in the holts fastening the shield to the point where the bolt heads touch the spring washers, and then, without finally tightening them, tighten the bolts fastening the clutch housing cover, and only after this, tighten the bolts fastening the shield. In all operations connected with disassembly of the clutch, it is necessary to use the sealing paste ('TU MKhP JJ36-52) in the points mentioned above during installation of the assemblies in their places. A tube of this paste is supplied with each TIL-130 motor vehicle. The basic data on the clutch are presented in Table 6-1.

The pressure plate is manufactured of SCh 18-36 cast iron (GOST 1412-54).

The clutch pressure plats lever is manufactured of 35 steel (COST 1050-60). The depth of the symmidized layer is 0.15-0.30 mm. Hardness is HRC 56-62. The number of levers is four.

The lever pins and support fork of the lever are manufactured of 15 steel (3557 1051-39). The depth of the cyanidized layer of the pins is 0.15-0.30 mm. Hardness is HRC 56-62.

The driven disk is manufactured of 50 steel (COST 3680-57, COST 914-56). Hardness is MSC 35-40. The disk is subjected to phosphatization. The driven disk hub to manufactured of 40kh steel (COST 4543-61). Hardness is MB 255-285. The disk is phosphatized and passivated in a solution of bichromate.

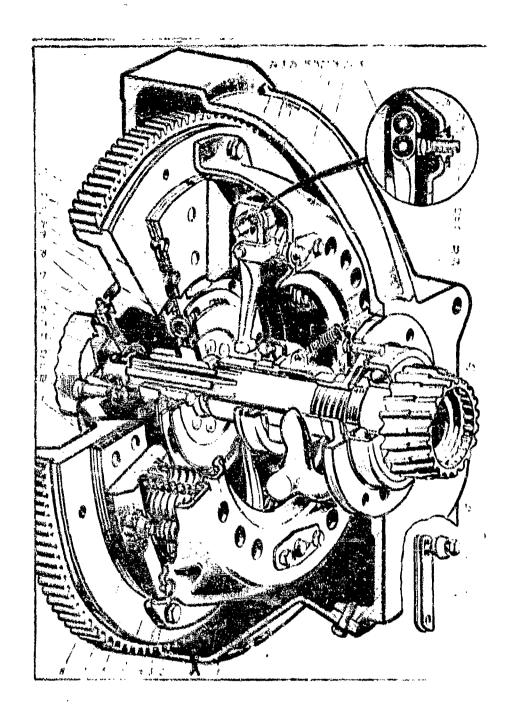


Plate 6-1. Single-disk clutch:

1) howing cover 2) flywheel 3) clutch cover 4 and 13) rivets 5) paired spring plates 6) bolt 7) formed bushing E) pressure plate 9) insulating washer 10) pressure spring 11) desper disk 12) damper plate 14 and 32) ball bearings 15) hub 16) crankshaft flange 17) damper intermediate disk 18) lubrication fitting 19) oil deflector 20) electic sleeve spring 21) sup-

[Plate 6-1, continued]

port plate 22) driven disk lining 23) steel driven disk 34) clutch housing 25) pins 26) needle bearings 27) support fork 28) adjusting nut 29) compression plate 30) pressure plate lever 31) guide sleeve 33) sleeve spring 34) throw out bearing sleeve 35) transmission input shaft 36) clutch disengagement fork

Table 6-1. Technical characteristics of the single-disk clutch

Parts and their parameters	ZIL-157K	ZIL-130 and ZIE-131			
Clutch assembly					
Number of driven disks		1			
Full clutch pedal travel, mm	1	160			
Pedal working travel, mm	130	0-150			
Pedal free travel, mm	30-45	35-50			
Number of friction linings		2			
Friction lining material	Asbestos composition				
Diameter of friction liners, mm:		•			
Exterior	341	l342			
Interior	186	5-187			
Friction liner thickness, mm	3,9	9-4.1			
Diameter of heles for rivets in liner, mm		0-4.3			
Diameter of holes in liners for					
rivet heads, mm	9.9	5-9.7			
Thickness of shoulder in friction	• , ,				
lining recess for rivet, mm	1.25	5-1.50			
Pressure springs					
Mumber of pressure springs	16				
Height of spring in free condition,					
mpa	61.7-63.0				
Control height of spring, mm		45			
Load with spring at control height,					
kg	64	64-72			
Minimum allowable load at control					
height, kg		60			
Elastic sleeve spring (damper)					
Number of springs		8			

Spring height in free condition, mm Spring control height, mm (no less)	24.35-24.65 22.5			
Load with spring at control height, kg Spring height under compression to)-65		
the point of coil touching, mm	21-22			
Clutch disengagement sleeve roturn spring				
Number of aprings	1			
Spring longth in free condition, mm				
(no greater)	36			
Spring control length, mm	56			
Load with spring at control length, kg	1.:	5-2.5		
Minimum allowable load with spring at control length, kg	1.2			
Clutch linkage spring				
Number of springs	1	1		
Height in free condition, mm	130	180		
Spring control height, mm	70	147		
Load with spring at control				
height, kg	23-28	9-12		
Minimum allowable load with		_		
spring at control height, kg	18	7		
Clutch pedal return spring				
Number of springs	1	1		
Spring length in free condition, mm	173	132		
Spring control length, mm	217	174		
Load with spring at control length, kg Minimum allowable load with spring	23-31	22-29		
at control length, kg	20	18		

The clutch disengaging sleeve is manufactured of SCh 15-32 cast iron (GOST 1412-54).

The clutch disengaging fork is manufactured of 45 steel (GOST 1050-60). Hardness of the tempered surface is HRC 52-62. Depth of the tempered layer is 1.0-4.0 mm.

The Flange of the clutch disengaging fork is manufactured of SCh 15-32 cast iron (GOST 1412-54). The bushing of the fork flange is manufactured of KCh 35-10 wrought iron (GOST 1215-59).

The clutch disengaging fork lever is manufactured of KCh 35-10 wrought iron (GOST 1215-59).

The clutch disengaging linkage is shown in Plate 6-2.

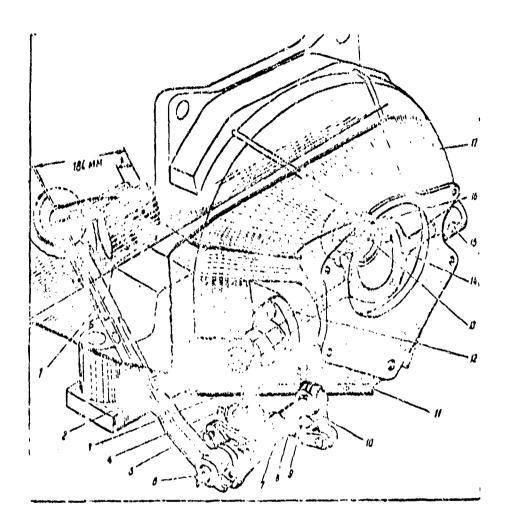


Plate 6-2. Clutch disengaging linkage of the ZIL-130 motor vehicle:

- 1) pedal 2) return spring 3 and 10) levers 4) stop nut
- 5) shaped adjusting nut 6, 11, and 15) lubricatinn fittings
- 7) pedal shaft 8) spacing spring 9) rod 12) flange
- 13) Sleeve spring 14) clutch disengaging fork 16) sleeve with bearing 17) clutch housing

Technical servicing

The single-disk clutch is not adjusted on the motor vehicle. If necessary, the clutch is removed and adjusted.

Care for the clutch includes cleaning the dirt from it and the timely tightening of bolts fastening the clutch housing to the cylinder block. These bolts are torqued (torque moment is 8-10 kg meters). The bolt heads are stopped with plates whose ears are bent up against a flat on the bolt head.

Care for the clutch linkage consists of adjusting the pedal free travel by means of changing the length of the rod. The clutch disengagement sleeve bearing does not require lubrication during operation. The clutch disengagement fork and pedal shafts are lubricated according to the lubrication chart (see Appendices 10 and 11--see Part II). For adjustment of the clutch disengaging linkage, see Plate 6-10.

Disassembly and assembly

1

During removal of the clutch, it is necessary to unscrew the bolts fastening the transmission to the clutch housing, disconnect the transmission from the housing, and remove it.

Unscrew the bolts fastening the clutch housing shield and ragova it.

Unscrew the bolts fastening the lower cover of the clutch housing and remove the cover.

Loosen the tension bolt fastening the lever on the fork shaft, remove the lever, and drive out the key.

Loosen the two bolts fastening the bushing flange and remove it.

Pull out the clutch disengagement fork, after previously moving it to the left and inclining it downward.

The clutch is dynamically balanced in assembly with the crankshaft at the plant. To maintain the balance, before removing the clutch from the flywheel, it is necessary to make marks on the flywheel and the pressure plate cover. This will allow them to be installed in their original position, not destroying the factory balancing.

inscrew the bolts fastening the pressure plate cover to the flywheel. While unscrewing the bolts, rotate the flywheel sequentially. The bolts must be unscrewed gradually and in sequence, in order to avoid deforming the cover.

Remove the pressure plate in assembly and remove the clutch driven disk.

Disassembling the pressure plate. Before beginning disassembly, mark the relative positions of all parts of the clutch. For disassembly of the pressure

plate, an auxiliary flywheel and steel disk 9.8 mm thick must be used in place of the driven disk. In place of the steel disk, any hard lining of the given dimensions can also be used. If necessary, various attachments with quick clips can be used for pressure plate disassembly, but with the mandatory installation of the pressure plate disk on eight centering study or bolts with the consequent pressure of the jacket on its feet.

For disassembly of the clutch pressure plate, it is necessary to set the flywheel on the bench, lay the disk on the working surface of the flywheel, set the pressure plate in assembly with its cover on it, and fasten it to the flywheel with lengthened bolts. The bolts must be 10-12 mm longer than the normal bolts used for fastening the cover.

It is recommended that disassembly of the pressure plate take place in the following order. Unpin the bolts fastening the support plates, unscrew them, and remove the plates from the clutch cover. Unscrew the adjusting nuts with a special wrench.

Unscrew the bolts fastening the paired spring plates, and remove the guiding bushings from the shaped holes in these plates. Then gradually unscrew all the bolts fastening the cover to the flywheel, until pressure is completely released from the pressure plate, and then screw out these bolts completely. Remove the cover, the pressure springs, and the insulation washers.

Mark the position of each clutch disengaging lever relative to the pressure plate, unpin and remove the pins connecting the levers with the pressure plate, remove the levers in assembly with the support forks, and extract the rollers from their receptacles in the levers. Unpin and drive out the pins connecting the levers with the support forks, remove the forks from the levers, and extract the rollers from their receptacles in the levers. Remove the pressure plate from the auxiliary flywheel.

If there are no additional bolts of extended length available, disassembly of the pressure plate may be conducted in the following manner.

Install the pressure plate in assembly on the flywheel, with the steel auxiliary disk 9.8 mm in thickness, and fasten them with normal bolts.

Unpin and a great the bolts fastening the support plates and remove the plates from the gover. Unscrew the bolts fastening the paired spring plates and drive the gauge bushings from their shaped holes in the plates. Preliminarily unscrew the adjusting nuts and leave them on the forks (on approximately half the height of the threaded portion of the nut); then unscrew all the normal bolts fastening the clutch cover on the flywheel, and after this, pressing on the cover by hand, finally unscrew the adjusting nuts, unscrewing them pair-wise on opposite sides of the cover until the springs are fully freed from pressure. After this, remove: the clutch cover, pressure springs, insulation washers, clutch disongaging levers, and pressure plate from the flywheel.

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Having disassembled the clutch, it is necessary to wash out all the parts in a degressing solution, check them for usability, and if necessary, replace unusable parts with new ones.

Assembly of the pressure plate. Ine pressure plate should be assembled in a sequence which is the reverse of that for disassembly on an auxiliary fly-wheel (used as a tool), placing a device (Plate 6-3) for regulating the position of the clutch disengaging levers beneath the pressure plate.

Allowable deviation in parallelness between the surfaces of the shoulders of the device must be no greater than 0.01 mm. In this, the plane of the surfaces of the shoulders must be parallel to surface three of the projection on which the control plate is installed. The allowable nonparallelness is no greater than 0.02 mm.

Set the flywheel on a metal working bench, lay the steel disk or adjusting device on it, and set the clutch pressure plate on them.

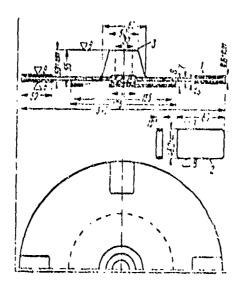


Plate 6-3. Device for regulating the position of clutch disengaging lavers:
1) device shoulders 2) control plate
3) device projection surface for installing the control plate

Assemble the needle bearings. For this, insert a technological ball which is 8.8-9.9 mm in diameter, and made of soft oil-resistant rubber in the hole in the lever, and then insert 19 rollers, lightly lubricated with oil, between the rubber ball and the wall of the hole in the lever. Insert 19 rollers into the second lever hole by the same method.

Align the holes on the support fork with the hole in the lever. In this, the spherical projection on the inside end of the lever must be directed the same way as the threaded end of the fork. After pushing out the rubber ball, insert the short pin in the aligned holes. Place cotter keys in the pon.

If a rubber ball is not available, the rollers may be assembled by placing a layer of grease on the surface of the hole, and the needle rollers are placed in the second hole after assembly of the lever with the fork.

Observing the marks made during disassembly, install the lever in the slot in the pressure plate bracket, after aligning the holes in the lever and in the bracket. After driving out the rubber ball, insert the long pin in the aligned holes. Insert cotter keys in the pin.

Install the remaining levers by a similar method. During this, the heads of identical pins must be in the same positions relative to the pressure plate.

Install the insulating washers on the pressure plate, and set the pressure springs on the washers. Align the marks made during disassembly for maintaining balance on the cover and plate, and set the clutch cover on the springs, guiding them ento the projections of the inner surface of the cover. In this, the threaded ends of the support forks must go into the holes in the cover.

Lightly pressing on the cover, screw the adjusting nuts onto the threaded ends of the fork by one or two turns.

Align the holes in the support feet of the cover with the threaded holes in the auxiliary flywheel, insert the lengthened centering bolts, and draw the cover feet to the flywheel, screwing in all the bolts gradually and in sequence.

Install the bushings into the formed holes in the paired spring plates, screw in the bolts fastening these plates, tighten the bolts. (torque moment is 1.0-1.5 kg meters), and then lock them by driving the thin edge of the bushing onto a flat of the bolt head.

Screw in the adjusting nuts with a wrench (Plate 6-4) until the face of the nut coincides with the face of the threaded end of the fork.

Install the support pressure plates on the adjusting nuts, screw in the bolts fastening these nuts, and tighten them preliminarily until the ends of the plates touch the jacket.

Adjusting the clutch disengaging levers. Without removing the assembled pressure plate of the clutch from the auxiliary flywheel (used as a tool), it is necessary to adjust the positions of the levers relative to the working surface of the pressure plate.

Rotating the adjusting nuts with a wrench (Plate 6-5, a), set all the levers in such a position that the distance from the working surface of the

pressure plate to the top of the spherical projections on the inner ends of the levers is within the limits of 39.7-40.7 mm. With this, the ends of the levers must lie in the same plane, parallel to the working surface of the pressure plate with inaccuracy of no more than 0.5 mm.

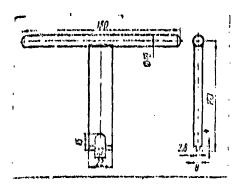
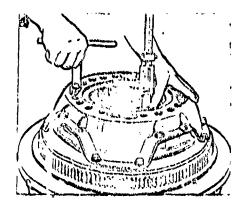


Plate 6-4. Wrench for adjusting the clutch



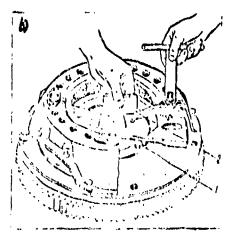


Plate 6-5. Clutch adjustment:
a) adjusting and checking the position
of the levers with a bar depth gauge;
b) adjusting and checking the positions
of the levers with the device and control
plate; 1) device 2) control plate

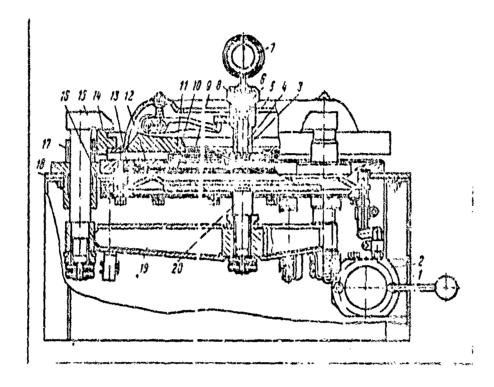


Plate 6-6. Device for adjusting the clutch:
1) body 2) valve 3 and 20) rods 4) measuring installation
body 5) measuring bushing 6) spring 7) indicator 8) mevable
ring 9) disk 10 and 11) studs 12) disphrage 13) cover
14) pressure ring 15) lever 16) busing 17) limiting bushing
18) plate 19) spider

In case the pressure plate of the clutch is assembled on a device for adjustment (see Plate 6-3), she levers should be installed with the control plate as shown in Plate 6-5, b. In this, the apherical projections of the levers must touch the control plate 2, which is installed on the projection of the device 1.

Disassembly, assembly, and adjustment of the clutch may to consucted on a GARO model R-20? device [Plate 6-6]. The clutch springs are compressed by three turning levers 15 through compression ring 14. The levers are brought into their working position with the help of a pneumatic chamber with a central rod 20 and spider 19.

The necessary mutual position of the working planes of the clutch pressure plate and the support plane of the clutch housing is provided by disk 9 with calibrating support studs 10.

The measuring device is installed on rod 3, which is fastaned in the center of cover 13.

With the assembled clutch on the R-207 device, the clutch disengaging levers are set by rotating the adjusting nuts with a wrench in such a position that the distance from the working surface of the pressure plate to the top of the spherical projections or the inner ends of the levers is within the limits of 39.7-40.7 mm.

In this, the ends of the lever: must be located in the same plane, parallel to the working surface of the pressure plate, with inaccuracy of no greater than 0.5 mm, which is checked by indicator 7.

Having finished clutch adjustment, tighten the bolts fastening the support plates (torque moment is 1.0-1.5 kg meters). Then pin the bolts (as a set of eight) with lightly annealed steel wire, 1 mm in diameter.

Punch the threaded connection of the adjusting nut with the threaded end of the fork on one point.

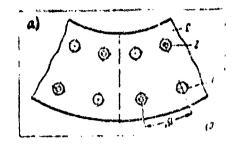
Unscrew the bolts fastening the cover to the auxiliary flywheel and remove the pressure plate in assembly with the cover. During this, all the bolts are unscrewed gradually and sequentially to avoid deformation of the clutch cover.

Changing the friction liners. The liners on the driven disk are changed if they are scored, peeled, or if the friction liners are worn down to the heads of the rivets. The liners are replaced in the following manner Lay the driven disk on backing blocks set so that there is a gap wide enough for passage of the rivet heads between them. This position of the blocks is necessary to prevent deformation of the seed disk.

Knoc. out the rivets with a punch and remove the wern-out friction liner. The diameter of the working end of the punch must be 2.0 km. The rivets should be knocked out from the side where they are rolled in. Remove the second friction liner in the same magner.

If the new friction liners do not have holes for eight rivers, they must be drilled, using the steel driven disk as a guide.

The diagram for drilling holes in the new liners for the rivet heads and heles for rolling the rivets out is shown in Piste 6-7, a. The liners must be fastened to the driven disk with brass rivets whose dimensions are given in Piste 6-7, b.



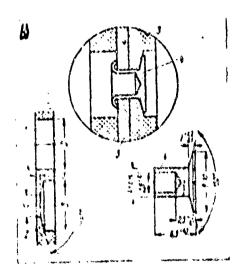
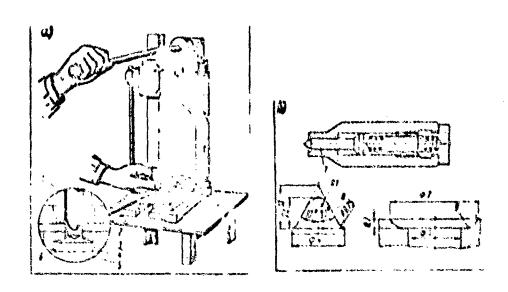


Plate 6-7. Fastening the friction liners of the clutch driven disk with rivets:

a) diagram of hole positions for rivets b) riveted connection 1) through hole for rolling the rivet 2) receptable for rivet head 3) driven disk friction liner 4) rivet 5) steel disk

for fastening the friction liners, it is necessary to lay the steel driven disk on the friction liner and align the hole: In the liner and the disk using a rod which is 4 mm in dismeter. Insert the rivet into its receptable in the liner so that its tubular portion projects shove the steel disk. Rest the head of the rivet on the cylindrical insert 4 (Plate 6-8) which is 9 mm in dismeter and installed on the table of a bench press (backing plates assuring the horizontal position of the driven disk sust be placed on the diametrically opposite side beneath the insert).

Sot the projecting end of the working part 8 of the plunger on the rivot and roll it, pressing of the mandrel of the plunger 7 with a press, as shown in Place 6-8, a. After pressing, the rivet must have a circular bead, on which one or two radial breaks are allowable. There must be no clearance between the steel disk and the circular bead. The rolled-out rivot must not rotate or move in an axial direction. The second rivet is clinched on the diametrically opposite side of the disk. The remaining rivets are rolled in an arbitrary order. The friction liner on the other side of the steel disk is clinched on in a similar order. There must be no cracks in the linings after rolling the rivets.



Place 6-8. Rolling the rivet fastening the driven disk friction liner:

- a) rolling the rivets with a press b) mandrel 1) punch
- 2) Priction liner 3) rivet 4) insert 5) plate 6) steel disk
- 7) man. trol plunger 8) plunger working part 9) mandrel working part

The driven disk may become warped during exchange of the friction linews. Therefore, the driven disk with its newly riveted liners should be checked for the absence of warping. The mathod of checking is shown in Plate 6-9. Oscillation of the driven disk is not allowed to be greater than 0.8 mm, and non-flatness is not allowed to be greater than 0.5 mm. If oscillation exceeds a given amount, the driven disk should be corrected with a special clamping device as shown in the illustration.

If the rivets fastening the hub loosen, they must be tightened or replaced. If the springs in the elastic sloeve (damper) of the driven disk are broken, they should be replaced.

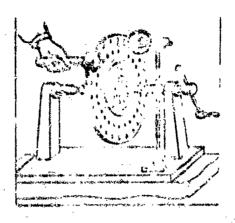


Plate 0-9. Checking and correcting the clutch driven disk

Installation of the clutch in the motor vehicle. Install the driven disk, directly the projecting part of the disk has toward the flywheel install the pressure place and cover assembly on the flywheel, eligning the marks made on the cover and flywheel during disabsembly, and lighten the cover on the flywheel by preliminarily acreming in several of the fastoning beits by head.

Canger the driven disk relative to the flywhool with a greeved mendrel or musilisty transmission input whaft, instrting it into the grooved hele in the driven disk hub and in the bar ing in the crankshort flence. Serew in the yerriskly formened botto and time! tighten the cover to the flywhool, thereof appling wanters beseath the head botto beforehand. All the before must be tightened gradually and sequentially.

Remove the mulitary shade from the grooved hote. Install the clutch disorgagement fork and the fork flange and fasten is with being and spring without.

Then, install the key is the took chaft keyway, count the fork lover, and tighter the lover stop ecres.

leaded the transmission on the gins in the circum assering and connect the fark by the state exercise out bearing elseve. Tighten the note fortuning the transmission to the clutch housing.

Install the housing cover and shield and fasten'them with bolts.

The clutch linkage in all ZIL trucks has identical construction, and therefore all operations connected with disassembly, assembly, and adjusting of the linkage are the same for all of the trucks.

During disessembly of the clutch disengaging linkage, it is necessary to remove the return spring 2 (see Plate 6-2) of the clutch pedal 1. Unscrew stop mut 4 and the spherical adjusting nut 5 of the pedal rod. Take rod 9 out of the holes in the fork of lever 3 and remove the support washer and spacing spring 8. Remove the cotter key from the pin connecting rod 9 and lever 10 of the pedal shaft, remove the washer, withdraw the pin, and remove the rod (in motor vehicles with in-line engines, remove the pin connecting the support ring and pedal shaft, and then remove the support ring and clutch pedal from the shaft. Loosen the fastening tension screw of lever 10 and remove it 1.0m the shaft. Loosen the fastening tension bolt of the pedal and remove the pedal from the shaft. Pull the pedal shaft from its bracket. Unscrew the nuts fastening the pedal shaft bracket and remove the bracket from the longitudinal frame rail.

After disassembly, all parts of the linkage should be washed out and inspected, and daugeble parts should be replaced with new ones if necessary.

If the hole for the axis (shaft) of the clutch pedal is worn more than the allowable amount, it is recommended that the hole be drilled out and a repair bushing be installed.

Worn-out faces of the bosses (hubs) of the pedal are renewed by wolding atth subsequent machining.

If the pedal is best, it is recommended that it be atraightened.

Assembly. Align the holes in the breaket of pedul shaft I with the holes in the longitudinal frame rail, insert the bolts with their heads outside, and screw nuts onto them, with spring washers inserted behavath the nuts. Insert the shaft in the bracket, mount the clutch pedal on the shaft, with its fluted surface upward, and tighten its tansion bolt (in motor vehicles with in-line engines, mount the support ring, and after oligning the holes in it with the holes in the axis, insert a cotter key and bend out its ende).

Hount lever 10 on shaft 7 and tighten its tension bolt.

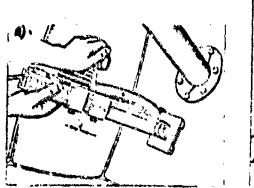
Align the holes of the forked end of rod 9 with the holes in lever 10 of the podal, insert the connecting pin with its head toward the side of the longitudinal frame rell, and fasten it with a cotter key.

Mount spring 9 and its washer on rod 9, insert the end of the rod in the holes in lever 3 of the fork, and screw on the spherical adjusting nut 5 (with its spherical side toward the fork lever), and then screw on the stop nut by hand.

Install the return spring 2 and fasten its pins at the pedal and the bracket on the frame cross member.

After assembly of the linkage, clutch pedal free travel must be adjusted with the engine installed in the motor vehicle with the help of a measuring device.

Adjustment. Install the measuring device (Plate 6-10, a) on the inclined floor of the cab, and then, rocking the pedal by hand, determine the free play A of the pedal (see Table 6-2).



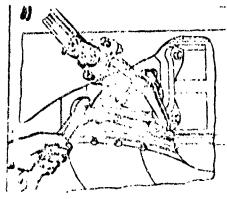


Plate 6-10. Adjustment of the clutch pedal free play:

- a) measurement of the pedal free play with a device
- b) adjustment of the padal free play A = amount of clutch padal free play

With proper adjustment, the free play of the clutch pedal must provide a clearance between the ends of the levers and the throw out bearing within the limits of 5.0-4.9 mm.

If the assumt of pedal free play does not correspond to the indicated d'mension, the linkage should be adjusted. For this, it is necessary to unscrew the stop nut on the clutch disengaging rod by several turns, after which, turning the adjusting spherical nut with a wrench (Plate 6-10, b), edjust the amount of pedal free play. In this operation, pedal travel is decreased by turning the nut to the right, and increased by turning the nut to the left. After adjustment, the stop nut is tightened, without allowing rotation of the spherical adjusting nut during tightening of the stop nut.

After adjustment, start the engine and check the proper operation of the clutch.

Dimensions of parts

The pressure plate. Thickness of the pressure plate, measured along the bosses for fastening the paired spring plates, is 25.72-26.00 mm. With overhaul of the pressure plate, the working surface is allowed to be ground down to a dimension of no less than 24.7 mm.

Non-flatness of a new disk or one which has been repaired is not allowed to be greater than 0.1 mm. Warping of a pressure plate is not allowed to be greater than 0.8 mm without being repaired.

Pressure plate levers. The diameter of the holes for the needle bearings in the pressure plate levers is 11.42-11.47 mm. Allowable dimension of the hole in a lever without being repaired is 11.49 mm.

The number of rollers in one joint of the lever is 19. Roller diameter is 1.59-1.60 mm. The diameter of the pins for the fork and lever is 8.17-8.20 mm. The allowable dimension of the pin without being repaired is 8.15 mm. The diameter of the hole in the support fork of the lever and in the pressure plate bracket for the lever pin is 8.2000-8.258 mm.

The allowable dimension of these holes without repair is 8.3 mm.

If the pins or holes in the lever, fork, and bracket of the pressure plate are worn more than the allowable amounts, they should be replaced.

The driven disk. The diameter of the driven disk is 342 mm. Thickness of the steel disk is 1.8 mm. Thickness of the disk in as embly with its friction liners is 9.44-10.16 mm. The limiting allowable thickness of a disk before replacement of the friction lining is 6.4 mm.

The nominal width of a slotted groove in the hub is 5.89-5.94 mm.

The allowable width of a slotted groove without repair is 6.05 mm. If the slotted groove is worn more than the allowable value, the hub is replaced.

Non-flatness of the working surface of the driven steel disk must be no greater than 0.3 mm. Non-flatness of the disk in assembly with its friction liners is not allowed to be greater than $0.5~\rm mm$.

Oscillation of the working surface of the driven disk in assembly with its friction liners with the hub installed on a grooved mandrel is not allowed to be greater than 0.8 mm.

If the rivets fastening the friction liners are loose or the liners are worn more than the allowable values, they should be replaced.

The clutch disengagement sleeve. The distance between the faces of the clutch disengagement sleeve and the clutch disengagement fork is 85.54-85.77 mm. The length of the face at the fork is 11 mm. The allowable dimension before being overhauled is 12.0 mm.

The diameter of the hole in the sleeve for the race of the transmission input shaft bearing is 47.60-47.65 mm. The allowable dimension before overhaul is 47.9 mm.

If the hole in the sleeve for the face of the bearing race is worn, the sleeve should be replaced.

The diameter of the face of the sleeve for the outside ring of the clutch throw out bearing is 55.002-55.032 mm.

The clutch disengaging fork. The diameter of the support faces of the clutch disengaging fork is 24.955-25.000 mm. The allowable dimension of the fork faces without being repaired is 24.92 mm. If the support faces of the clutch disengaging fork are worn more than the allowable amount, the fork should be replaced.

The distance between the ends (faces) of the fork is 86.00-86.23 mm. The allowable dimension between the ends of the fork without being repaired is 88.00 mm. It is recommended that the fork faces be repaired by welding and subsequent machining.

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Table 6-2. Dimensions of clutch linkage parts, mm.

Key:	a)	dimensions
	b)	nominal

- c) allowable
- without repair
 d) pedal shaft
- diameter
 e) diameter of
 shaft hole in
- pedal
 f) diameter of
 bushing in
 bracket for
 pedal shaft
- g) diameter of hole in pedal for rod pin

- h) diameter of hole in 1 i for connecting pin
- i) diameter of hole in pedal shaft lever for connecting pin
- j) diameter of connecting pin

Width of the keyway is 5.945-5.990 mm. The allowable dimension of the keyway without being repaired is 6.01 mm.

Oscillation of the support faces of the clutch disengagement fork is not allowed to be greater than 0.12 mm. If oscillation is greater than that allowable, the fork must be corrected.

Diameter of the hole for the fork flange bushing is 30.000-30.045 mm. The allowable dimension without being repaired is 30.07 mm. If the hole for the bushing in the flange is worn, it should be reamed out to a repair dimension of 30.250-30.259 mm.

The exterior diameter of the flange is 41.95-42.00 mm. The allowable dimension without being repaired is 41.90 mm. If the exterior diameter of the flange is worn to more than the allowable, the flange should be replaced.

The diameter of the hole in the flange bushing for the clutch disengaging fork is 25.060-25.130 mm. The allowable dimension without being repaired is 25.17 mm. If the hole in the bushing is worn to more than the allowable dimension, the bushing should be replaced.

The diameter of the hole in the lever for the clutch disengaging fork shaft is 25.977-25.010 mm. The allowable dimension of the hole for the fork shaft without being repaired is 25.3 mm.

The diameter of the hole for the clutch disengaging rod is 24 mm.

If the lever is bent, it should be straightened. If the threads in the holes for the fork lever fastening tension bolt are damaged, it is recommended that the hole be welded up, drilled out, and tapped with a M10 X 1.5 class 2 thread

The dimensions of parts for the clutch disongaging linkage are presented in Table 6-2.

Chapter 7. Transmissions

Layout

The plant began to produce the transmissions for the ZIL-130 motor vehicle in April of 1961. Transmissions for the ZIL-157K and ZIL-131 motor vehicles and their modernizations have some minor design differences from the transmissions of the ZIL-130 motor vehicles.

The transmission for the ZIL-130 motor vehicle is three-throw, five-speed, with all gears except low gear and reverse gear in constant engagement.

The transmission is equipped with two inertia type synchronizers for engagement of second and third, and fourth and fifth gears.

The transmission of the ZIL-130 motor vehicle is assembled with a drum type hand brake (Plate 7-1, a).

The transmission (Plate 7-1, b) without the hand brake and with changed cover and additional levers for controlling the transfer case and the front drive axle is intended for installation on the three-axle 27-157K and ZIL-131 motor vehicles. There is no speedometer drive in the transmissions for the three-axle motor vehicles, since it is installed in the transfer case.

Various modifications on the transmission (Plate 7-2) differ in gears 19 and 21 of the speedometer drive, which are calculated on the ** transmission ratio of the rear axis.

Since the third quarter of 1967, the front bearing of the trensmission input shaft has been installed with a separator instead of a needle bearing. In connection with this, the design of the input shaft journal for the bearing and the recoptacle for the bearing in the input shafe were changed, and the stop ring was eliminated.

To prevent water from falling into the transmission (Plate 7-3) when fording streams, the transmission gear selection lever of a ZIL-131 motor vehicle is sealed with a rubber boot and tension clamps. The transmission housing surface which fits against the clutch housing, the transmission cover, inspection hole cover, and bearing cover are also scaled with a special paste (VTU MKhP 3336-52). The internal space of the transmission is connected with the atmosphere through ventilating tube 17.

In all operations connected with opening and disassembling the transmission, assembly is conducted with the use of the noted sealing paste.

All transmissions have a factory sorial number which is stamped on the upper right boss of the transmission housing.

Technical Characteristics of the Transmission

Transmission type	Mechanical, with five speeds forward and one reverse
Synchronizers	Two inertia type for engagement of
•	second and third, and fourth and fifth
	goars
Transmission ratios:	•
First gear	7.44
Second gear	4.10
Third goar	2.29
Fourth gear	1.47
Fifth gear	1.0 (straight)
Roverse gear	7.09
Maximum torque moment	
transmitted by the	
transmission, kg meters	41

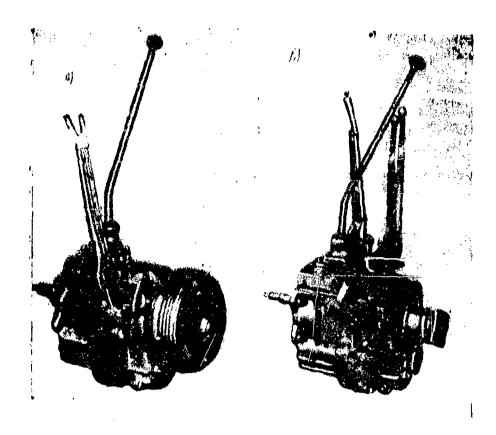


Plate 7-1. Overall view of transmissions:

a) for ZIL-130 motor vehicles
b) for 3-axle motor vehicles

Goar selection

Power take-off Maximum take-off power, hp Lever, installed on the transmission cover From the reverse gear cluster 30

The transmission housing is east of type SCh 18-36 iron, GOST 1412-54.

The input shaft (Plate 7-4) is manufactured of 25 KhGM steel. Depth of the hardened layer is 0.5-0.7 nm, hardness of the surface layer is HRC 60-65, and hardness of the core is HRC 35-45.

The input shaft goar and synchronizer carrier 10 (Plate 7-5) is manufactured of 25 KhGM steel, and the depth of the hardened layer is 0.5-0.7 mm. Hardness of the surface layer is HRC 57-60, and hardness of the core is

The input shaft (Plate 7-6) is manufactured of 25 KhGM steel; depth of the hardened layer is 0.8-1.1 mm, and hardness of the surface layer is HRC 60-65, and hardness of the core is HRC 35-45.

The intermediate shaft (Plate 7-7) is manufactured of 25 KhGM steel; depth of the hardened layer is 0.8-1.1mm, hardness of the surface layer is HRC 57-60, and hardness of the core is HRC 35-45.

The gear cluster is manufactured of 25 KhGM steel; depth of the hardened layer is 0.5-0.7 mm, hardness of the surface layer is HRC 57-60, and hardness of the core is HRC 35-45.

The reverse gear cluster shaft is manufactured of 25 KhGM steel; depth of the hardened layer is 0.5-0.8 mm, and hardness of the surface layer is HRC 60-65.

The goar selector lever unit is shown in Plate 7-8, and the transmission cover is shown in Plate 7-9.

Technical service

During TS-2, it is necessary to check the fastening of the transmission to the clutch housing, the fastening of the side and top covers, and to wash out the air passage in the vent, whose clogging causes increased pressure in the transmission housing and will lead to oil leaks. The magnetic plug in the drain hole should be cleaned when oil in the transmission housing is changed (every six TS-2).

Whenever changing or adding lubricant, it is necessary to clean dust and dirt off the transmission.

Lubricant should be measured immediately after stopping the motor vehicle, when the unit is still warm, and fresh oil should be poured in through the filler hole in the transmission housing up to the level of that hole. If there is a power take-off box on the transmission, oil must be poured in through the hole on the power take-off box housing.

The front bearing of the transmission input shaft is lubricated through the lubrication fitting 18 (see Plate 6-1), which is screwed into the passage in the crankshaft flywheel.

To lubricate the bearing, it is necessary to remove the clutch housing cover from beneath the automobile and rotate the crankshaft so that the lubrication fitting is directed downward. On the ZIL-130 and ZIL-131 motor vehicles, beginning in April 1967, a bearing was installed with a constant supply of lubricant (for the entire time of its operation). In this case, the passage is blocked with a plug.

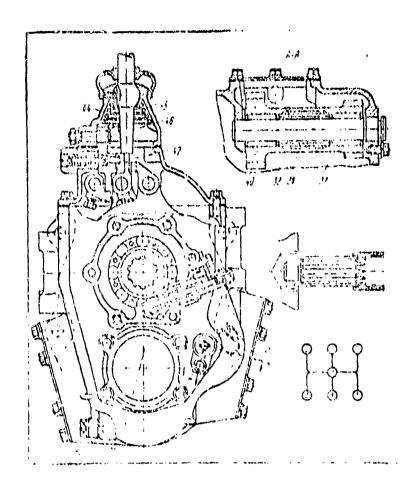
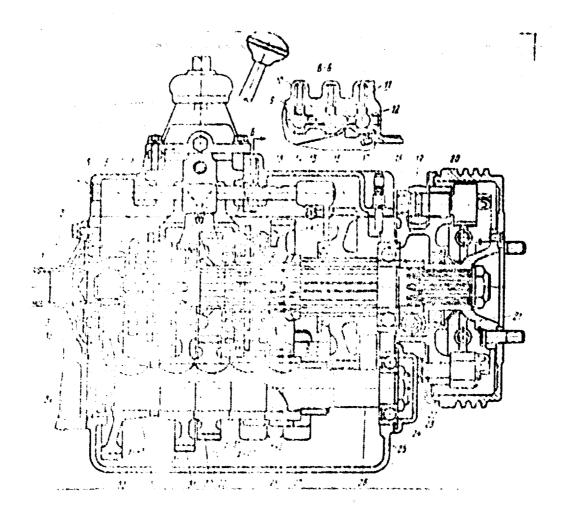


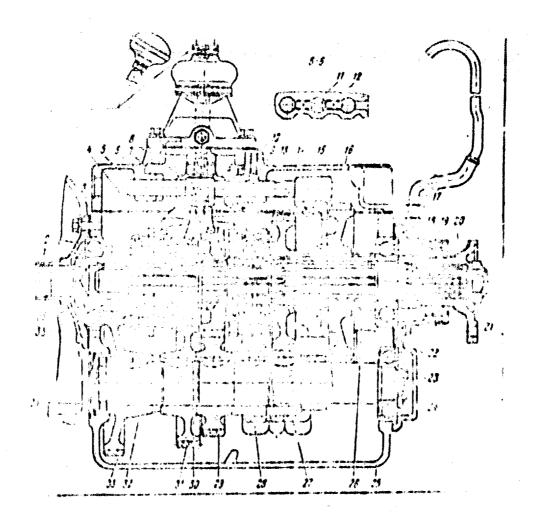
Plate 7-2. Transmission of ZIL-130 motor vehicle:

1) input snaft 2, 18, 24, 34, 35, and 37) bearings 3) input shaft bearing cover 4) fourth and fifth gear synchronizer 5 and 31) fourth speed gears 6 and 29) third speed gears 7) feurth and fifth speed changing fork

8) second and third speed changing fork 9) eatch lock ball 10) catch lock spring 11) lock pin 12) lock ball 13) second and third speed synchronizer 14 and 27) second speed gears 15) first and reverse gear changing fork 16) first and reverse gear 17) vont 19) speedometer drive gear 20) hand brake drum 21) speedometer driven gear 22) intermediate shaft bearing cover 23) bearing fastening nut 25) transmission housing 26) output shaft 28) reverse gear 30) fourth speed gear bushing 32) intermediate shaft 23) intermediate shaft constant engagement gear 36) input shaft bearing fastening nut 38) spacing bushing 39) reverse gear cluster shaft 40) reverse gear cluster 41) filler hole plug 42) drain hole plug 43) transmission cover 44) lever housing 45) lever spring 46) lever 47) protector support



[Plate 7-2, continued]



[Plate 7-3, continued]

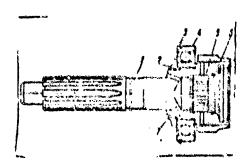


Plate 7-4. Transmission input shaft assembly: 1) shaft 2) nut 3 and 6) lock rings 4) bearing 5) needle bearing rollers 6) thin edge of nut pressing into shaft elot

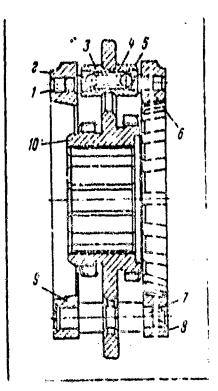


Plate 7-5. Synchronizer

1) catch lock support 2 and 3 conic ring 3) catch lock 4) catch lock spring 5) catch lock ball 6) profile of spiral passage on conic surface of ring (for rapid passage of oil from the cone surface at the moment of gear changing) 7) blocking finger 9) conic surface of ring 10) synchronizer

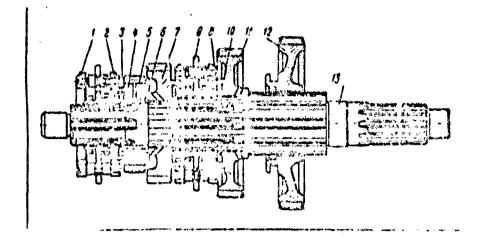


Plate 7-6. Transmission output shaft assembly:
1) fourth and fifth gear synchronizer 2 and 9) lock rings 3, 6, and 10) support washers 4) fourth speed gear 5) fourth speed gear bushing 7) third speed gear 8) second and third gear synchronizer 11) second speed gear 12) first speed gear 13) output shaft

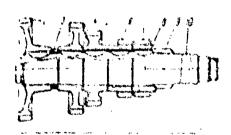


Plate 7-7. Transmission intermediate gear in assembly:
1) lock ring 2) constant engagement gear 3) spacing hushing
4) fourth speed gear 5) third speed gear 6) reverse gear
7) second speed gear 6) key
9) first speed toothed ring

10) snafe.

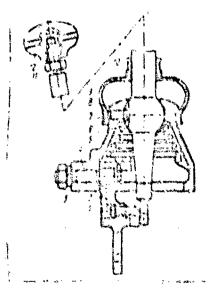


Plate 7-8. Coar changing lever unit in section.

1) protector 2) intermediate lever for selecting first and reverse gears

2) nut 4) intermediate lever axis

5) spring 6) ring 7) eatch local lever housing 9) protective sleeve 15) gear changing lever 1;) nut 1.) knob

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Recoval of the transmission from the motor vehicle. For removal of the transmission, it is necessary to unscrew the bolts fastening the inspection hole cover above the transmission in the cab and remove it, and unscrew the flange fastening the propellor shaft. On two-axis motor vehicles, disconnect the bracket of the intermediate support from the frame cross member, and free the propellor shafts.

Disconnect the clutch adjusting rad and return spring. Discomment the speedometer drive shaft. Remove the housing with the geer changing lever and the manual brake lever. This crew the second flange of the propellor shaft from the transfer case and remove the propellor shaft.

On these-axis motor vehicles, the levers installed on the transmission must be disconnected from their rods and removed.

If there is a winch on the motor validie, it is necessary to disconnect the propellor shaft from the power take-off box and remove the transmission together with the power take-off box.

Unscrew the builts featuring the transmission to the clutch housing with a bex and wrench. Disconnect the transmission from the clutch housing and except it (Plate >-10) with a model 444 hydraulic jack.

Resove the transmission from the motor vehicle. The housing with the transmission quatral lever and the brake lever may be left in place.

Disassembly Engage the transmission with a hanger (Plate 7-11, a), raise it with a haist, and set it on a decice (Plate 7-11, b) intended for disassembly art assembly of the tornamission.

takers discussibly, it is necessary, to drate the oli by unscreeting the plus, and clear and with the metalds of the transmission.

Removal of the hand brake (the operation) lates only to the IIL-130 motor vehicle), impores the nut factoring the flange on the output short, and remove the flat weeker and flange in assembly with the drum. Disconnect the spring of the shoet, and unseres and remove the boits and spring washers. Unpin and remove the rod connecting the drawber fork with the brake lever. Remove the hand irvin bracket in assembly with the brake shoes, protective disk, and seal from the tracketins ion. Astract the two installation bushings of the bracks from the holes in the housing with cliers.

for resident of the handrake drive lever from the transmission, it is necessary to unserse the two holts fastening the sector and the one holt factoning the lever, sector the lever place, brake drive lever assembly, the two apacing bushings, and the lever assertor.

Monoval and disassembly of the transmission selector lever housing.

Unsures the four holts fastening the lever housing and remove the housing with the lever in assembly and the housing gasket.

Fasten housing 8 (see Plate 7-8) of the lever in a vise with the lever down.

Holding the head of the intermediate lever shaft, unserew nut 3 festening the shaft, remove the spring washer and shaft 4 with the intermediate lever 2. Then remove the shaft from the hole in the lever and the protector 1. Extract spring 5 from the housing, remove support 6. The lever, remove lever 10 in assembly and the lever catch lock 7. For removal of the protective boot, it is necessary to loosen nut il and unscrew handle 12.

Beforedisassembling the transmission cover with the gear selector mechanism on a three-axle motor vehicle, it is necessary to remove the lever for engaging the transfer case and the front axle, and also the lever to hand brake drive.

Removal and disassembly of the transmission selector mechanism. Unscrew the bolts fastening the transmission cover, remove the cover in assembly with the gear selector mechanism, and remove the cover gasket. If the gasket is stuck, it is necessary to carefully separate it with a screwdriver or other tool.

The transmission selector mechanism is disassembled on a device (Plate 7-12) on which the cover is fastened in a position convenient for disassembly. If there is no device available, the cover is installed in a vise. Unpin the stop bolts fastening the forks and the protector heads on rods 9, 10, and 11 (see Plate 7-9), unscrew the stop acrews fastening the forks 3, 5, and 6, and the bolts fastening the rod heads. Move one of the gear selector rods with a pry, and press out the plug from its receptable. Moving the rod, remove the forb and, holding the catch lock balls by hand, remove the rod with the other hand. The two other gear selector rods are removed by similar means.

Removal and disassembly of the input shaft. Bisconnect the return spring from the clutch throw out bearing sleave, and remove the sleave and bearing in assembly. Unscrew the four bolts festening the input shaft front bearing cover, and remove the cover and its gasket.

In order to remove the input shaft from its recess in the transmission housing, it is necessary to press out the bearing with a 40P-5015 puller (Plate 7-13) and remove the shaft and bearing in assembly.

To withdraw the front input shaft bearing from the input shaft recess, it is necessary to fasten the shaft in a vise, remove the stop ring 6 with a screwdriver (see Plato 7-4), and remove the rollers 5 of the bearing.

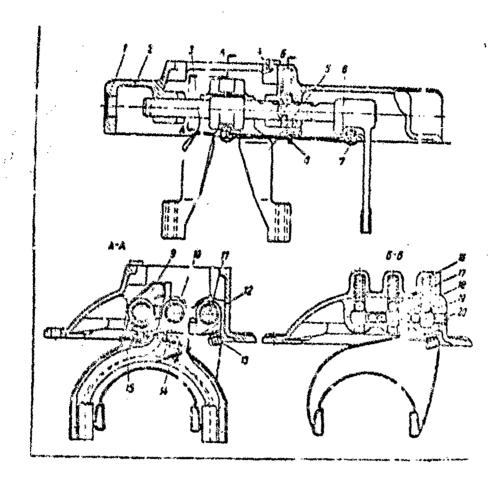


Plate 7-9. Transmission cover in assembly:
1 and 20) plugs 2) cover 3) fourth and fifth gear fork 4) installing bushing 5) second and third gear fork 6) first and reverse gear fork 7 and 13) stop boits 8, 14, and 15) tie wire 9) second and third gear selector rod 10) fourth and fifth gear selector rod 11) first and reverse gear selector rod 12) first and reverse gear rod head 16) catch lock apring 17) catch lock ball 18) lock pin 19) lock ball

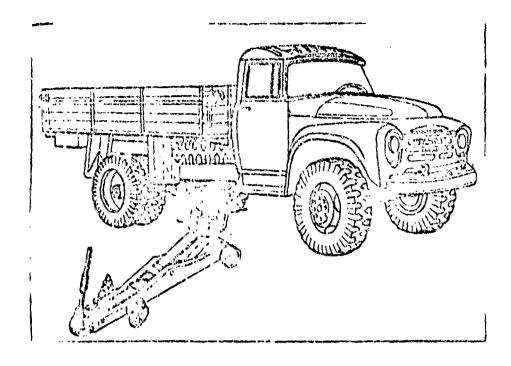
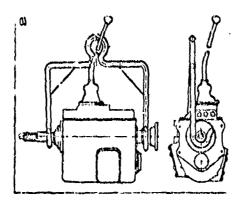


Plate 7-10. Removing the transmission from the motor vehicle

To unscrew the nut fastening the bearing 4, mount the shaft in the device shown in Plate 7-14, drive down the thin edge 7 (see Plate 7-4) of nut 2, unscrew the nut fastening the bearing, and press off bearing 4 with a device.

Removal and disassembly of the input shaft. Remove the speedometer drive gear from the end of the input shaft. Press the input shaft gear together with the shaft out of their recess in the transmission housing with a mandrel and hammer. Press the bearing off the shaft (Plate 7-15), and remove the input shaft in assembly with its gears and synchronizers from the transmission housing.

Remove synchronizer 1 (see Plate 7-6) for fourth and fifth gears and first speed gear 12 from the shaft. Remove the lock ring 2 (see Plate 7-6) fastening the fourth speed gear with two screwdrivers (Plate 7-16). Remove the support washer 3 together with fourth speed gear 4 and steel bushing 5 together with its stop. Remove support washer 6 and third speed gear 7, and remove second and third gear synchronizer 8. Remove the lock ring fastening the second speed gear with two screwdrivers. Remove support washer 10 and second speed gear 11. The synchronizers should not be disassembled unless necessary.



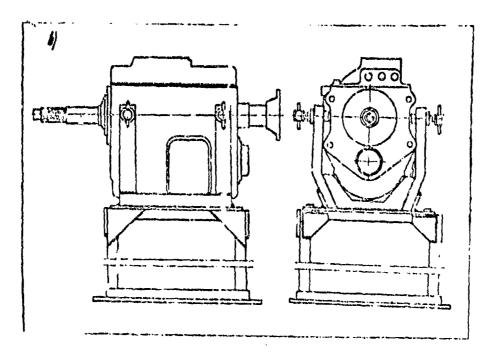


Plate 7-11. Device and sling for raising and moving the transmission:

- a) sling b) device

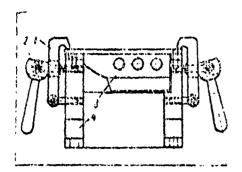


Plate 7-12. Device for disassembling and assembling the transmission cover: 1) pressure lever 2) pressure eccentric 3) cover 4) device frame

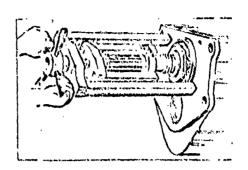


Plate 7-13. Pressing out the input shaft bearing with a 40P5019 device

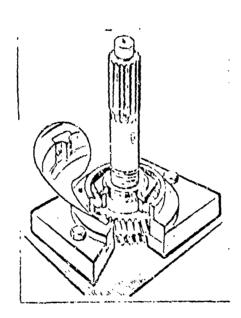


Plate 7-14. Disassembling the input shaft with the device

Removal and disassembly of the intermediate shaft and reverse gear cluster. Unscrew the bolt fastening the reverse gear cluster shaft stop, remove the stop, and remove the cluster shaft, the gear cluster, the two roller bearings, and the spacing bushing from the housing.

Unscrew the four bolts fastening the intermediate shaft rear bearing cover, remove the cover and gasket, drive down the thin edge of the nut, brace the intermediate shaft gear with a lever, and unscrew the nut fastening the rear bearing.

Press the rear bearing, togother with the intermediate shaft, out of the receptacle in the transmission housing, and move the shaft and gears along their axis toward the bearing. Press out the intermediate shaft rear bearing with a puller, the same way as the input shaft bearing was pressed out (see Plate 7-15). Remove the intermediate shaft with its gears in assembly from the housing.

Remove the intermediate shaft front bearing from its recess in the housing. If necessary, drive out the plug covering the front bearing with a mandrel and remove its stop ring.

For disassembly of the intermediate shaft, remove lock ring 1 (see Plate 7-7), press all the gears off the shaft, and pry keys 8 from the keyways. The gears may be pressed off with a device (Plate 7-17, a) or a support. Plate 7-17, a, shows a constant engagement gear being pressed off.

The last two gears, reverse gear and second gear 6 and 7 (see Plate 7-7) must be pressed off simultaneously. For removing the shaft 39 (see Plate 7-3) of the reverse gear cluster, a model 2489 puller is used (Plate 7-18).

Assembly of the transmission takes place in the following order. Assembly and installation of the intermediate shaft: install key 8 in its slot in the shaft (see Plate 7-7), and subsequently press onto the shaft the second speed gear (interference 0.005-0.055 mm), the reverse gear (fit from interference of 0.04 mm to clearance of 0.01 mm), the third and fourth speed gear (interference of 0.015-0.065 mm), which have been previously matched according to their journals. Install the spacing bushing, press the constant engagement gear (interference of 0.015-0.065 mm), and fasten it with a lock ring. The ring is installed with a screwdriver. All gears on the intermediate shaft must be pressed on until they are supported at their faces.

Install the transmission housing on the device (see Plate 7-11), check the condition of its shaft bearing surfaces, the absence of cracks and the amount of wear in the holes for bearings. Cracks and perforations in the transmission housing are not acceptable. If the holes for the bearings are worn more than the allowable dimensions, the transmission housing is subjected to removal by a method of pressing in repair bushings.

Damage to the threads in the housing holes is allowed within the limits of no greater than 2 turns.

Deviation of the front and rear faces of the housing relative to the axis of the hole for the input shaft bearing is allowable within the limits of 0.08-0.15 mm.

Non-parallelness of the axes of the intermediate and the input shaft, and deviation from the common plane passing through them, must not exceed 0.07-0.12 mm on the entire length of the housing.

Micalignment of the remaining shaft bearing planes in the transmission housing must be within the limits of 0.15-0.3 mm.

Install the ring of the front roller bearing of the intermediate shaft in its receptacle in the transmission housing (fit from an interference of 0.01 mm to a clearance of 0.033 mm). Mount the roller bearing on the front ring of the intermediate shaft (clearance of 0.015-0.047 mm). Install the intermediate shaft in assembly with its gears in the housing, first driving the rear end of the shaft into the recess for the ball bearing, and then installing the front end of the shaft with its roller bearing assembly into its external ring.

Press the ball bearing assembly with its lock ring on the rear end of the intermediate shaft (interference of 0.003-0.032 mm), direct it into the recess in the housing, and install the bearing together with the shaft in its recess in the heusing with a mandrel (fit from an interference of 0.012 mm to the clearance of 0.038 mm). Screw on the nut and tighten it. Torque moment is no less than 25 kg meters. Punch the nut, bending its thin edge into the slot in the shaft. Install the rear cover and gasket and fasten the cover with bolts and spring washers.

Install the stop ring in the receptacle in the housing for the front bearing, and fit it with a mendrel, insert the plug into its receptacle and press it in with a mandrel.

Deviation of the intermediate shaft journal relative to its axis are not allowed to be greater than 0.03 mm. Incorrect shaft journals may be repaired by chroming with subsequent machining to nominal dimensions.

Deviation of the transmission goar faces is not allowed to be greater than 0.05 mm. If cracks or great wear on the teeth or grooves are present on the gears, the gears should be replaced.

Small chips on the sides of the teeth should be smoothed off. Chips are not allowed on the working surfaces.

Small depressions of a fatigue character (pitting) on the working surface of a gear tooth are allowed on an area no greater than 15% of the entire surface. Sharp edges, small dents or burns on the gear teeth should be smoothed off.

Install the roller bearings in the holes of the reverse gear cluster, inserting the spacing bushing between them, install the gear cluster in the transmission housing, install the gear cluster shaft (with a fit of: large diameter shaft end--from an interference of 0.052 mm to a clearance of 0.004 mm, and small diameter shaft end--with a clearance of 0.007-0.06 mm). Install the stop plate in its depression and fasten the shaft with bolts and spring washers.

Assembly and installation of the output shaft and synchronizers. Install the shaft with its rear end down in a vise with soft inserts, and assemble the shaft parts in the following sequence. Mount first speed gear 12 (see Plate 7-6) on the groves, install second speed gear 11, mount the support washer 10 on the shaft, and fasten the gears with a lock ring by fitting it into the depression on the shaft with a special mandrel. Install second and third speed synchronizer 8 on grooves on the shaft and, after inserting support washer 6, install third speed gear 7 on the shaft journal. Install bushing 5 of the third speed gear, directing its catch lock groove into the groved slot in the shaft. Install fourth speed gear 4 on the bushing, mount support washer 3, and fasten the gear with lock ring 2, fitting it into the depression in the shaft with a hollow bodied mandrel. The ring must fit tightly in its groove. Install fourth and fifth gear synchronizer 1 on grooves on the shaft

Remove the shaft from the vise.

Oscillation of the output shaft journal relative to its axis is not allowed to be greater than 0.05 mm. Fetigue type chipping of the hardened layer on the journal surface is not permissible.

The requirements for the goars of the output shaft are the same as for the goars of the intermediate shaft.

If the parts of the synchronizer are worn or its springs lose their elasticity, the synchronizer assembly should be replaced.

Facial and radial oscillation for a new synchronizer relative to the housing is allowed to be up to 0.1 mm.

Guiding the rear end of the shaft into its recess in the transmission housing, install the output shaft assembly in the housing, mount the bearing in assembly with its lock ring on the end of the shaft and, guiding it into its recess in the housing, press in the bearing together with the shuft with a mandrel.

Assembly and installation of the input shaft. For assembly, the shaft is installed in a device (see Plate 7-14), and the bearing is pressed on (interference is 0.003-0.038 mm). Install lock ring 3 in its groove (see Plate 7-4), screw on nut 2 and tighten it. Tightening moment is no less than 20 kg meters. Then fasten the nut, driving its thin edge 7 into the slot in the shaft.

Remove the shaft from the device, fasten it in the vise, and install the rollers 5 of the needle bearing in their recess. The rollers must be in the same group according to dimensions. The rollers must be installed using grease. The last roller (the locking one) is installed from the face freely, without interference, and the rollers are fastened with lock ring 6, installing it in its groove on the shaft. After assembly, the rollers must rotate freely, without falling from their receptacle. Remove the shaft from the vise.

If the journals and grooves on the shaft are worn more than the dimensions admissible without being remained, the shaft should be replaced.

Worn-out shaft journals may be repaired by chroming with subsequent machining by grinding to nominal dimensions.

Oscillation of the input shaft journal at the bearing relative to its axis is not allowed to be greater than 0.025 mm. If the shaft is bent or twisted, it must be replaced.

Damage to the threads beneath the ball bearing fastening nut are not allowed to cover more than 1.5 of the thread turns.

The input shaft gear teeth must not have cracks. Small dents, burrs, and chips on the tooth faces should be smoothed off.

Small depressions of fatigue nature (pitting) are admissible on the worksing surfaces of the teeth, but must not cover more than 15% of the surface.

Install the input shaft with its bearing in assembly in the housing receptacle (bearing fit is from an interference of 0.012 mm to a clearance of 0.038 mm), and guide the end of the input shaft into its needle bearing. Install the input shaft bearing cover with its gasket, fasten them with bolts and spring washers, mount the sleeve and clutch throw out bearing on the cover guide, and install the return spring on the sleeve.

Assembly of the transmission cover is conducted in the reverse sequence as disassembly.

Cracks or chips are not admissible on the transmission cover, especially those passing through the edge of the flange and the bolt holes or passing through the holes for the gear changing rods.

If the aperture for the ball support of the gear changing lever is worn greater than the allowable dimensions, the cover should be replaced.

If the hales in the transmission housing cover for the gear changing rods are worn, the cover should be replaced or repaired by installing bushings.

Crookedness of the gear changing rods is not allowed to be greater than 0.1 mm. Bent rods may be repaired by straightening. Gear changing rods which are worn greater than the allowable dimensions should be replaced or renewed by chroming and machining.

Wear on the slots in the rods for the catch lock balls is admissible so long as the clearance between the formed template and the slot does not exceed 0.6 mm. If this margin is exceeded, the rod should be replaced.

If there are cracks or chips on the gear changing forks, heads, or lever, they should be replaced.

Bent gear changing forks and levers may be straightened.

If the fingers on the gear changing forks are worn more than the allowable dimension, the forks should be replaced.

If wear is present on the slot in the fork and head for the gear changing lever or the holes in the fork and head for the gear changing red, they should be replaced.

If the groove for the gear changing lever catch lock is worn, the lever should be replaced.

During assembly of the transmission cover, first insert rod 11 (see Plate 7-9) with the first and reverse gear changing fork, then rod 10 with the fourth and fifth gear changing fork, and finally rod 9 with the second and third gear changing fork. After the rods and forks have been installed, they should be fastened with stop belts 7 and 13, and tied off with wires 8, 14, and 15, wound through their ends.

Check the transmission and sof the first speed goar and the synchronizer carrier in the noutral position. Install the transmission cover with its gasket, driving the ends of the fork into the slot in he first speed goar and the slots in the fingers of the other forks onto the disks of the synchronizer carrier. Then fasten the cover with bolts and spring washers.

Assembly of the gear changing lever housing. Fasten the housing into a vise, insert catch lock 7 (see Plate 7-3) of the lever in holes in the housing, install gear changing lever 10 after coating its spherical surface with grease, mount support 6 of the spherical part of the lever onto its tail, install lever spring 5, turning its bent out end at shown in the illustration, and guide the spring up beneath the neck of the housing.

Assemble intermediate lever 2 ofter installing the protector 1 and shaft 4, lubricated with grease, in it. Install the lever together with the shaft in the housing, then fasten it to the housing with nut 3 and a spring washer. Remove the housing from the vise, install the protective boot 9, screw the round knob 12 onto the gear changing lever, and tighten it with nut 11.

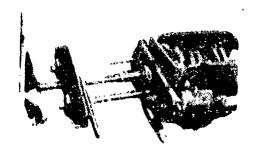


Plate 7-15. Pressing the rear bearing off the driven shaft

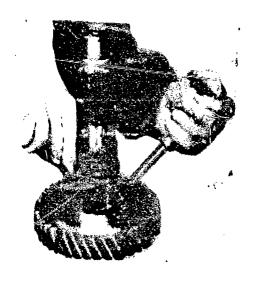


Plate 7-16. Removing the fourth goar locking ring from the driven shaft

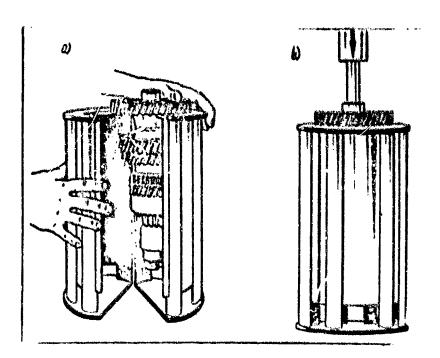


Plate 7-17. Disassembly of the intermediate shaft: a) installation of the intermediate shaft in a device b) pressing off the constant engagement gear

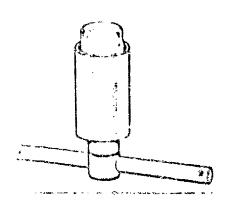


Plate 7-18. Puller for the reverse gear block shaft (model 2469)

Install lever housing 8 with its gasket guiding the end of the intermediate shaft into the hole in the first and reverse gear rod head, and the end of the gear changing lever into the slot in the gear changing fork. Fasten the lever housing with bolts and spring washers.

During assembly of the ZIL-130 motor vehicle transmission, it is necessary to install the speedometer drive warm gear on the end of the input shaft. Install the stationary part of the hand brake in assembly and fasten it with bolts and spring washers. House the brake shoe tension springs with a device, install the flange in assembly with the brake drum on the grooves, mount the support washer on the shaft, and screw on and tighten the nut. The tightening moment is no less than 30 kg meters. Lock the nut by driving its thin edge into the slot in the output shaft.

It is recommended that all cover gaskess is installed with No. 80 gress. After assembly, it is necessary to pour oil into the transmission up to the level of the control plug and check the transmission on a special stand. The transmission should be run in by an electric motor for a period of three to five minutes each for each of the gears.

During the process of running the transmission in, it is checked for normal ongagement of the gears, increased gear noise during engagement, and knocks, oil leaks at the seals and joints, and also for other deficiencies.

The properly working transmission is installed on the engine with a hydraulic jack or block and tackle, hand fastened to it on study with nuts and spring washers. The tightening moment of the nuts must be 12-15 kg meters.

The transmission housing is centered along the flange of the input shaft rear bearing cover (this cover simultaneously serves as the support for the clutch threw out sleeve).

Parts dimensions

Dimensions of transmission parts for the motor vehicles are presented in Table 7-1, 7-2, 7-3, 7-4, 7-5, 7-6, 7-7, 7-8, and 7-9.

Table 7-1. Dimonsions of holes for bearings in transmission housing,

Hole dismeter	Nominal	Allowable without repair
For input and output shaft bearings	109.986-110.023	110.05
For front intermediate shaft bearing	71 .96 12 .02	72.06

[Table 7-1, continued]

For front end of reverse gear cluster shark	29.967-30.020	30.50
For rear end of reverse goer cluster share	32.00)-32.039	32.06

Table 7-2. Basic dimensions of the input shaft, was

Dimension	Hominal	Allowable without repair
Tooth thickness on shaft		
groaved portion	5.14-5.64	5.00
Diameter of raller bearing	•	
receptrole	43.98-44.067	44.08
Diameter of shaft journal		
at ball bearing	60.003-60.023	59.98
Diameter of shaft end		
journal	24.96~24.98	₹4.94
Tooth langth (musber of		
teeth of the constant		
engagement gear 20)	26.0	***
Tooth thickness (measured		
at a height of 6.128 mm)	7.17-7.21	7.0
Tooth length (number of		
teeth in the first speed		
zear18)	7.0	
Slot width	4.63	4 . 8

Table 7-3. Dimensions of output shaft journals and grooves, am

Diagnsica	Nominal	Allowable without rapats
Clauster of the shaft front end journal for		
the roller bearing Dissoter of the journal	27.929-27.950	27 . (34)
for the ball bearing Disceter of the journal for the fourth speed constant engagement	50.003-20.020	49.97
gear bushing	46.491-47.009	46.97

[Table 7-5, continued]

Diameter of the journal for the second speed		
constant engagement	40. 00 40 DI	40.00
spiral goar	60.92-60.94	60,90
Tooth thickness of the		
shaft grooved portion		
for the synchronizor:		
Second and third speeds	8.88-8.94	8.78
Fourth and fifth speeds	10.90-10.95	10.80
Diameter of the journal for		
the peedometor drive		
2842	45.975-46.000	es to-
Tooth thickness of the		
shaft grooved portion		
for the first speed gear	10.88-10.94	10.78
Tooth thickness of the	22.2.	
shaft grooved portion		
for the flange	5.99-5.94	5.80
Ciameter of the journal		0.00
for the third speed		
constant engagement		
	51.92-51.94	E1 00
spical goar	31.94-31.94	51.90

Table 7-4.	Input shaft goar dim	ensions, ma
Dimensions	Nominal	Allowable without repair
	Pirst Speed Gear	
Number of teeth45; 25Nh0 of surface layerHRC 57-6		er depth0.5-0.7 mm; hardness 35-40.
Tooth length Tooth Width (measured at	29.86-30.0	27.0
a height of 1.2 mm) Groved portion slot	4,90-4.95	4.7
width	11.00-11.06	11.2
Width of those for gear changing fork	9.2-0.4	9.6

[Table 7-4, continued]

Second speed gear

Number of teeth--42; number of toothed sleeve teeth--24; 25kh@H steel; hardened layer depth--0.5-0.7 mm; surface layer hardness--HRC 60-65; core hardness--HRC 35-45.

Tooth length	29.0	**
Tooth width (measured at a height of 2.5 mm)	4.657-4.687	4.50
Sleeve tooth length	6.5	5.5
Sleeve tooth groove width	4.054	4.2
Second speed support washer thickness	3.952-4.00	3.930

Third speed gear

Number of teeth--33; number of toothed sleeve teeth--23; 25KhGM steel; hardened layer depth--0.5-0.7 mm; surface layer hardness--HRC 60-65; core hardness--HRC 35-45.

Tooth length	28.0	
Tooth width (measured at		
a height of 3.5 mm)	5.347-5.387	5.2
Sleeve tooth length	4.6	4.0
Sleeve tooth slot width	6.075	6.2
Dismeter of gear hole		
for shaft journal	52.000-52.018	52.04
Width of third speed		
gear support washer	3.952-4.00	3.930

Fourth speed gear

Number of teeth--26; number of toothed sleeve teeth--18; 25KhQM steel; hardened layer depth--0.5-0.7 mm; surface layer hardness--HRC 60-65; core hardness--HRC 35-45.

Tooth length	26	* *
Tooth width (measured at		
a height of 3.5 mg)	5,346-5,386	5.2
Sleeve tooth length	7.3	6.0
Sleeve tooth slot width	7.519	7.8
Diameter of gear hole External diameter of	\$5.00-\$5.018	55.02
pushing diameter or	54.92-54.94	54.90

[Table 7-4, continued]

Width of gear support washed

3.952-4.00

3.930

Specioneter drive worm gear

Number of threads--5; 20 steel, GOST 1050-60; hardened layer depth--0.15-0.20 mm; hardness--HRC 56-62.

Tooth thickness

1.76-1.81

1.70

Dismeter of hole in worm gear for output shaft

journal

46.000-46.039

--

Speedomuter drive driven gear

Number of teeth: on the ZIL-1.70 and ZIL-1306 meter vehicles--17; on the ZIL-130V1 and ZIL-MMZ-555--18; 00 steel (GOST 1050-60); depth of cyanated layer--0.15-0.30 mm; hardness--!NC 65-62.

Tooth thickness in the

ZIL-130 and ZIL-130G

motor vehicles

2,21-2,26

2.16

Tooth thickness in the

ZIL-130V1 and

ZIL-MMZ-555 motor

vehicles

1.76-1.81

1.70

Output shaft flange

Number of grooves: on the ZIL-130 and ZIL-130G motor vehicles--17; on the ZIL-130V1 and ZIL-MMZ-555 motor vehicles--18; 40 Kh steel (GOST 4543-57), hardened by heating with high frequency current; hardened layer--1-2.5 mm; hardness--HRC 56-62.

Diameter of flange journal for the seal	57.88-58.00	57,80
Diameter of the bolt holes		
for fastening the propellor shaft flange	14.24-14.36	15.00
Dimension of the flange grooved portion slots	6,00-6.05	6.2

Table 7-5. Basic dimensions of synchronizers, mm

Dimension

Nominal

Second and third speed carrier

Number of teeth: first ring (left) -- 23; second ring (right) -- 24.

Tooth length:	
First ring	7.7
Second ring	7.7
Full tooth width:	
First ring	6.02
Second ring	3.99
Decreased tooth width:	
First ring	5.42
Second ring	3,39
Synchronizer carrier groove	
width	9.00-9.09
Diameter in carrier hole for	
catch lock	14.00-14.07

Fourth and fifth speed carrier

Number of teeth: first ring (left) -- 18; second ring (right) -- 18.

Tooth length:	
First ring	7.7
Second ring	7.7
Full tooth width:	
First ring	4.567
Second ring	7.454
Decreased tooth width:	
First ring	3.93
Second ring	6.85
Synchronizer carrier groove	
width	11.00-11.05
Diameter in carrier hole for	
catch lock	14.00-14.07

Conic ring of the second and third, and fourth and fifth speed synchronizers

Brass LmTs KA 58 2-1-1; hardness no less than HB = 130.

Diameter of hole in synchronizer ring for catch lock support 6.00-6.025 Diameter of hole in syncaronizor ring for blocking finger

9.00-9.03

Synchronizor catch lock support

A12 steel (GOST 1414-54), hardened layer depth--0.15-0.30 mm; hardness--HRC 56-62.

Diameter of catch lock support journal for sonic ring hole

6.030-6.065

Synchronizer blocking finger

45 steel (GOST 1050-60); case hardened by heating with high frequency current; depth of case-hardened surface layer--1-1.25 mm; case hardened layer hardness--HRC 56-62.

Dismeter of finger journal for hole in synchronizer conic ring

9.035-9.100

Synchronizer spring

Number of coils--9; spring wire steel 0.8 mm in diameter (GOST 9580-60).

Spring diameter	5.57-5.60
Spring length in free condition	13.0
Spring length under a load of	
1.5-1.9 kg	9.5
Wire diameter	0.8

Table 7-6. Intermedians shaft journal dimensions, mm

Dimensions	Nominal	Allowable without repair
Shaft journal diameter		
for bail bearing	40.003-40.020	39.98
Shaft journal diameter		
for roller bearing	41.983-42.000	41,96
Shuft journal diameter		
for constant on- gagement goar	52.045-82.065	
Shaft journal diameter	1,210 43 " 32 10 0#	,, -
for spacing bushing	52.045-52.065	~~
Shaft journal diameter		
for fourth speed gear	54.045-54,065	••

[Table 7-6, continued]

Shaft	journal	di ame	ter
for	third	speed	gear
	journal		
for	second	speed	rasg

54.545-54.565

55.535-55.555

Table 7-7. Parameters of the intermediate shaft goars, m	Table	7-7.	Parameters	οf	tho	intermediate	shaft	gears. m
----------------------------------------------------------	-------	------	------------	----	-----	--------------	-------	----------

Πŧ	ma	***	4 6	1112	

Nominal

Allowable without repair

First speed goar

Number of teeth--13; material and heat treatment as in the intermediate shaft.

Tooth	length	
Tooth	thickness	(measured
_		·

33.38-34.00

32.00

at a height of 5.6 mm)

8.108-8.148

7.9

Second speed gear

Number of teeth--22; 25KhGT steel; hardened layer depth--0.5-0.7 mm; surface layer hardness--HRC 57-60, core hardness--HRC 35-45.

Tooth	1 or	igti	1			
Tooth	thi	cki	1055	(meas	ured
at	0 P	ioi	zh t	oí	4.6	nun)
Diamet	er	of	ho1	0	for	shaft
jou	l Pri i	1.1				

1.0

5.034-6.074

5.9

\$5.50-55.53

Reverse gear

Number of teeth--20; 25KhGT steel; hardened layer depth--0.5-0.7 mm; surface layer hardness--HRC 57-60; core hardness--HRC 35-45.

Tooth Tooth				(meat	ured
at	5 }	101	ght	of	4.7	man)
Diamor	. 6r	of	hol	ø	for	shaft
Jou	irn	16				

25.72-26.00

7.462-7.502

55.00-55.03

7.25

Third speed gear

Number of teeth--31; 25KhGT steel; hardened layer depth--0.5-0.7 mm; surface layer hardness--HRC 57-60; core hardness--HRC 35-45.

Tooth length Tooth shickness (measured 28.9

at a height of 3.3 mm)

5.347-5 387

5.14

[Table 7-7, continued]

Diameter of hole for shaft journal

54.50-54.53

--

pourth speed gear

Number of teeth--38; 25KhGT steel; hardened layer depth--0.5-9.7 mm; surface layer hardness--HRC 57-60; core hardness--HRC 35-45.

Tooth length	28.0	• •
Tooth width (measured at a height of 3.5 mm) Diameter of hole for	5.347-5.387	5.14
intermediate shaft		
journal	54.00-54.03	
Support washer thickness	3.952-4.00	3.90

Constant engagement gear

Number of teeth--43; 25KhGM steel; hardened layer depth--0.5-0.7 mm; surface layer hardness--HRC 57-60; core hardness--HRC 35-45.

Tooth length Tooth thickness (measured	25.0	
at a height of 2.974 mm) Diameter of hole for intermediate shaft	4.995-5 035	4.8
journal Longth of spacing bushing	52.00-52.03 9.97-10.00	9.80

Table 7-8. Dimensions of reverse goar cluster and shaft, man

Dimensions	Nominal	Allowable without repair
Diameter of hole in gear cluster for roller bearing	42.000-42.027	42.06
Diameter of gear cluster shaft Diameter of shaft thickened	29,96-29,98	:` 94
portion	32.035-32.052	32,025

Cluster large goar

Number of teeth--22

[Table 7-3, continued]

length thickness (measured	25.72-26.0	
a height of 2.1 mm)	5.576-5.616	5.45
	Cluster small goar	
	Number of teeth15	
length thickness (measured	25.48-26.00	
a height of 5.6 mm)	8.115-8.145	8.0

Table 7-9. Dimensions of the transmission housing cover, the lever cover, and gear changing mechanism parts, mm

Dimensions	Nominal	Allowable without repair
Tran	smission housing cover	
SCh 1532 cast from (GOST 1412	-54).	
Diameter of the holes for the gear changing rods	19.64-19.08	19.13
Gear	changing lever housing	
SCh 1532 cast iron (GOST 1412	-54).	
Diameter of the hole for the invermediate lover shaft	11.000-11.035	11.05
Ĺ	lear changing lever	
Steel 20 (GOST 1050-60).		
Diameter of the upper ball support of the lever Dimensions of the working surface of the lower	37,75-37,92	37.5
spherical and Dimensions of the slot	15.78-15.30	15.6
for the upper ball support lock	7 0-8.2	8.35

[Table 7-9, continued]

Intermediate lever for selection of first and reverse gears

25 LK-1 steel, precision cast (GOST 977-53).

Diameter of hole for intermediate		
lever shaft	14.000-14.035	14.05
Diameter of hole for protector		
lock	8.0-8.2	8.4
Dimension of the intermediate		
lever slot	16.0-16.3	16.5

Shaft of the intermediate lever for selecting first and reverse gears

A-12 steel (GOST 1414-54); hardened layer depth--0.3-0.3 mm; surface layer hardness--HRC 56-62.

Diameter of shaft journal for the hole in the gear changing lever housing Diameter of shaft journal	10.965-11.00	10.925
for the hole in the intermediate lever	13,93-13,98	13.8

Rods for changing fourth and fifth, second and third, and first and reverse gears

45 steel (GOST 1050-00), case hardened by heating with high frequency currease hardened layer depth--1-3 mm.

Rod diameter	18,979-19,000	15.95
Radius of detent for catch	6 4° 6 76	Claudonna ao mastar
lock	5.63-5.75	Clearance no greater

Fork for selecting second and third, and fourth and fifth goars

25 LK-1 steel, precision cast (GOST 977-53); hardened layer depth--0.3-0.5 mm; hardness--HRC 56-62.

changing rod	19.02-19.03	19.1
Dimension of slot for gear changing lever Width of slot for fork	16.00-16.24	16,5
fingers	6.8-7.0	7,4

Fork for selecting first and reverse gears

Type 20 steel (GOST 1050-57); hardened layer depth--0.3-0.5 mm; surface layer hardness--HRC 56-62.

Diameter of hole for gear

changing rod 19.02-19.05 19.1 Thickness of fork fingers 8.7-8.8 8.5

Head of rod for selecting first and reverse gears

25 LK-1 steel (GOST 977-53); hardened layer depth--0.3-0.5 mm; surface layer hardness--HRC 56-62.

Diameter of hole for gear

changing rod 19.02-19.05 19.1
Width of slot for gear
changing lever 16.00-16.30 16.0

Goar changing lever spring

Number of coils--4; spring wire, a mm in diameter (GOST 5047-49).

Diameter of the largest spring coil	69.3-70.5	• •
Diameter of the smallest spring coil	44.38-45.0	
Length of spring in free condition	39	~ ~
Length of spring under a load of 24-31 kg	26	* *
Wire diameter	5	* *

Spring of first and reverse year engagement protector

Number of coils--10; spring wire, class 1, 2.2 ma in diameter (COST 9389 60).

Spring diameter	13,07-13.	a ~
Spring length in free		
condition	41	
Spring length under a		
load of 14-17 kg	33	
Wire diameter	2.2	

First and reverse gear engagement protector lock

A-12 steel (GUST 1414-54); cyanated layer depths-0, 5.6.5 mm; surface layer hardness--HRC 56-62.

[Table 7-9, continued]

Protector lock diameter Lock length 7.85-7.95 26.22-26.50 7.75

Chapter 8. The Transfer Case

Layout

A single-throw, two-speed transfer case is installed in the ZIL-157K motor vehicle (Plate 8-1 and Table 8-1).

This case has three output shafts which turn on tapered roller bearings.

The ZIL-131 motor vehicle is equipped with a two-throw transfer case having two output shafts which turn on ball and cylindrical roller bearings. The advantage of these bearings is the fact that they do not require adjustment, either during assembly or during the process of operation of the motor vehicle, as do the tapered roller bearings in the transfer case of the ZIL-157K motor vehicle.

Both transfer cases have a mechanism preventing self-disengagement of the gears. In the transfer case of the ZIL-157K motor vehicle, it is formed on the input shaft 14 (Plate 8-1) and shaft 57 of the front axle drive in the form of grooves having a varied thickness and forming a step on which carrier 22 and sleeve 56 rest during self-disengagement. A diagram of gear positions in the various speeds and distribution of the torque moment during them is shown in Plate 8-2.

In the transfer case of the ZIL-131 motor vehicle (Plate 8-3), the installation preventing self-disengagement is formed an the grooves of both gears 25 and 32, located on shaft 3 of the front axle drive. This installation prevents the self-disengagement of low speed engagement carrier 31 and front axle drive engagement carrier 23. The construction which blocks disengagement of high gear has another arrangement. On the exterior ring of high gear engagement carrier 16 and assembled with the grooved hole of output shaft 19, there is a conic construction, i.e., tooth thickness and slot width along the length in the same diameter are changeable; they have a reverse cone which prevents self-disengagement.

To prevent simultaneous engagement of two speeds in the transfer case of the ZIL-131 motor vehicle, there is a blocking arrangement which consists of balls 46 betw. In rods 36 and 47. When one of the rods is moved, the balls move to the other and lock it.

Plate 8.4 shows the separate air-disphrage chamber for engagement of the front axle drive and the rod for this chamber in assembly.

Both transfer cases have openings for installation of power take-off boxes. The linkage for central of the transfer case in the ZIL-157K motor vehicle is shown in Plate 8-5, and that for the ZIL-131 motor vehicle is shown in Plate 8-6. Construction of the electro-pneumatic valve controlling the front axle drive of the ZIL-131 motor vehicle is shown in Plate 8-7. When it is not energized, the electro-pneumatic valve is closed by the force of spring 3, and the air-disphragm chamber 10 (see Plate 8-3) is connected through a vent to the atmosphere.

When current is fed to coil 13 (see Plate 8-7) of the electromagnet, core 12 pulls rod 17, overcoming the force of spring 3 and the resistance of compressed mir, and opens inlet valve 20.

When this happens, compressed air enters the space above the membrane in the air-diaphrage chamber, controlling the front axis drive.

Suspension of the transfer lase on the ZIL-157K motor vehicle (Plate 8-1,4-is realized by four study acrewed into the body of the transmission and passing through holes in the frame cross member. To provide clastic suspension of the transfer case, rubber cushions are installed on both sides of the cross member. The stud nuts are pinned.

Table 8-1. Technical characteristics of transfer cases

Parameters	ZIL-157K	211-131
Type	Nechanical, single-throw, with two speeds	Mechanical, two-throw, with two speeds
Transmission ratio: Low speed High speed	2.27	2.08 1.00
Speed selection	Single lever and rod	Single rocking lever and
Pront axle engagement	Positive, with a lever and mechanical sleeve	Automatic and positive. Automatic engagement is accomplished with an elec- trical awitch which is turned on during engagement of low speed. Positive en- gagement is accomplished electrical disongagement in any gear. With automatic or positive engagement, the slectro-passassic valve and and air-disphrage chamber awitch in.

[Table 8-1, continued]

Middle and rear axle drive

Accomplished from the transfer case shaft to the middle axle and from the transfer case to the roar axle through a single Cardan Cardan drive

Accomplished from the transfer case output shaft through shaft

Suspension of the transfer case in the ZIL-131 motor vehicle (Plate 8-6, b) is formed on two longitudinal rails which rest on the frame cross member. The rails on the frame cross member have elastic suspension, since they are fastened with bolts having rubber cushions installed on both sides of the support. The transfer case is suspended from the two longitudinal rails on four bolts passing through holes in the longitudinal rails. All nuts on the bolts fastening the longitudinal rails are pinned, as are those on the bolts fastening the transfer case.

Suspension of the transfer case on the ZIL-131 motor vehicle has a number of advantages over suspension of the transfer case on the ZIL-157K motor vehicle. First, the loading points of the supporting elements are spread. decreasing their load. Socond, the supporting elements need not be removed during removal of the transfer case, and it is sufficient to unscrew the nuts from the bolts fastening the transfer case to the auxiliary longitudinal rails. Third, when the bolts fastening the transfer case break, they are easily replaced. When the stude fastening the transfer case of a ZIL-157K mater vehicle break, they must, as a rule, be drilled out of the body.

Technical service

During DS, conduct cleaning operations and an external inspection of the transfer case.

huring TB-1, it is necessary to check the fastening of the transfer case. on the frame and tighten the holts.

During TS-2, shock the blocking of the transfer case control levers and tightness of the tapered hearings in the transfer case of the ZIL-157K motor vehicles. If necessary, adjust the tightness of the bearings.

During TB-2, check to control linkage of the transfer case of the 21L-131 motor vehicle and if necess by, eighten the stop nuts on the adjusting forks.

Adding and changing the oil in the transfer case must be done within the periods shown in the lubileation charts.

When checking the level of all in the housing, it is necessary to wash out the air passages in the vent, whose clogging may cause increased pressure in the transfer case housing and oil leakage through the scals.



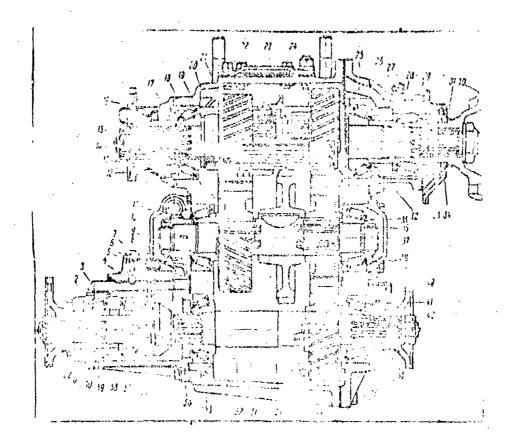


Plate 8-1. Transfer case of ZIL-157K motor vehicle: 1, 16, 30, and 40) flanges 2) oil deflecting washer 3) front axle engagement fork rod 4) catch lock bal. 5) stop screw 6) catch lock spring 7) catch lock spring plug 8) plug 9, 18, 24, 25, 29, 38, 41, 53, and 58) tapered roller bearings 10, 17, 37, 45, and 60) bearing covers 11) speedometer drive worm gear 12) input shaft bushing 13, 53, 44, and 61) seals 14) input shaft 15, 35, and 42) nuts 19) support washer 20) input shaft suching pin 21) drive gear 22) high and low speed engagement gear (carrier) 23; opening cover 26) bearing housing 27) bearing spacing bushing 28) adjusting washer 31) output shaft 32) output shaft gear 34) rear bearing cover (hend brake bracket) 35) lock washer 39) output gear intermediate shaft 43 and 62) dust covers 46) housing 47) housing 48) middle and rear axle drive gear 49) intermediate shaft low speed driven year 30) intermediate shaft 51) intermediate thatt constant engagement gear 52) middle axle drive shaft 54) front axle drive shaft bearing carrier 55) front axle engaging sleeve fork 55) sleeve 57) front axle drive shaft 59) adjusting gaskets

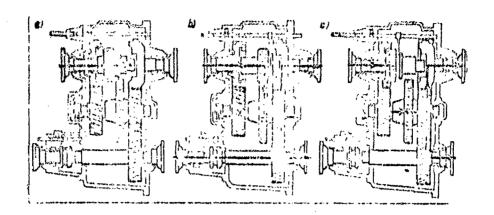


Plate 8-2. Diagram of various gear engagements of the transfer case of the ZIL-157K motor vehicle:

a) neutral position b) low speed and front axle engaged c) high speed engaged

Before changing or adding oil to the transfer case, dust and dirt should be classed from it.

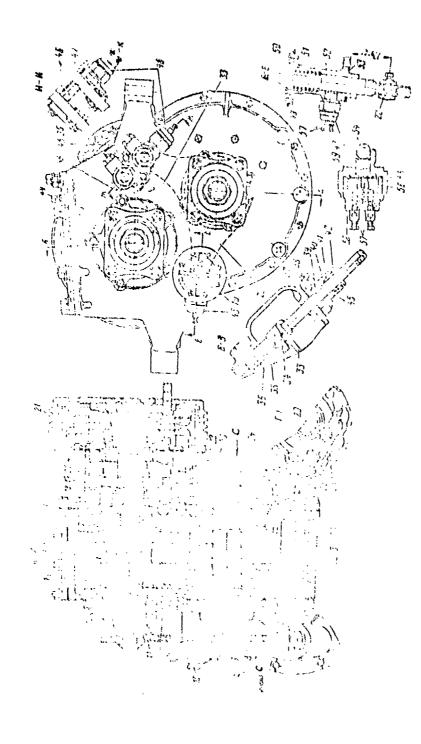
Then changing the oil, wash out the transfer case with low viscosity oil (industrial 12 or 20, GOST 1707-57), clean the magnetic plug of the drain hole, and wash out the air passages of the vent

Oil in the transfer case must be measured immediately after stopping the motor vehicle, while the unit is still warm. Oil must be filled to the level of the lower control hole in the transfer case. If a power take-off box is mounted on the transfer case, oil must be filled to the level of the upper control hole.

The transfer case control lever shaft must be jubricaled through the pressure lubrication ficting until fresh grease is pressed out.

Disassembly and assembly

The transfer case in the ZIL-157K motor vehicle should be removed with a carriago--the model 444 hydraulic jack (Plate 8-9), installed under its recess 4. Before removing the transfer case, drain the oil from it by unscrewing the drain hole plug. The sequence of operations in removing the transfer case is as follows.



6) oil deflecting ring 43) Switch for indicator 36) high speed engaging rod 37) catch luck spring plug 10) air-diaphragn chamber for engaging front 30) needle bearing 31) low speed engaging carrier 32) low speed gear 33) low speed engaging fork 28) holding plate 29) speedometer driven spection hole cover 18) housing side cover 19) output shaft with gear 20) speedometer worm gear 23) front axle drive engaging carrier 5 and 24) covers 42) seal nut Transfer case of ZIL-131 motor vehicle: stop bolt 35) high speed engaging fork 36) high speed engag spring 39) catch lock ball 40) tubber ring 41) felt ring 4) stop ring 22) front axle drive engaging fork 26) drain hole plug 27) speedometer collar 9) flange nut 3) front amle drive shaft 13) seal 14) drive gear 8 and 11) flanges Plate 8-3. drive 12) input shaft 7) filler hole plug speed gear 1) housing

[Caption for Plate 8-3, continued]

light signalling engagement of front axle 44) vent 45) catch lock body 46) blocking mechanism balls 47) low speed engaging rod 48) electromagnet switch of electropneumatic valve 49) air-diaphragm chamber body 50 and 50 and 55) diaphragms 51) return spring 52) rod 53) adjusting gaskets 54) switch ball 56) contacts 57) poles 58) pole insulation 59) switch body

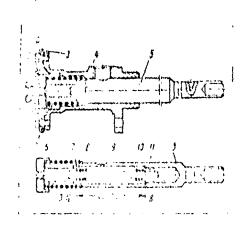


Plate 8-4. Air-diaphragm chamber for engaging front axle drive:

- a) chamber in assembly b) chamber rod in assembly
- 1) diaphragm 2) bolt 3) cover
- 4) chamber body 5) exterior rid of
- clamber 6) cup 7) stop ring 8) washer
- 9) internal rod 10) pressure spring
- 11) nut 12) rod flat 13) return spring

Park the motor vehicle on a level rurface. Set blocks beneath the wheels so that the motor vehicle does not roll forward or backward.

Relacio the handbrake.

Disconnect the Cardan shafts, transfer case control linkage rods, and handbrake control rod from the transfer case.

Roll the hydraulic jack underneath the motor vehicle and, turning handle 2, raise lever 3 so that the *ransfer case is located in receptable 4.

Unpin and unscrew the nuts fastening the transfer case with a box and wrench.

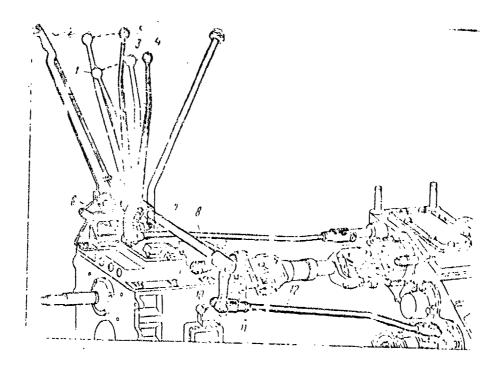


Plate 8-5. Control linkage for transfer case of ZIL-157K motor vehicle:

1) lever position during engagement of low speed 2) lever position during engagement of front axle 3) neutral position

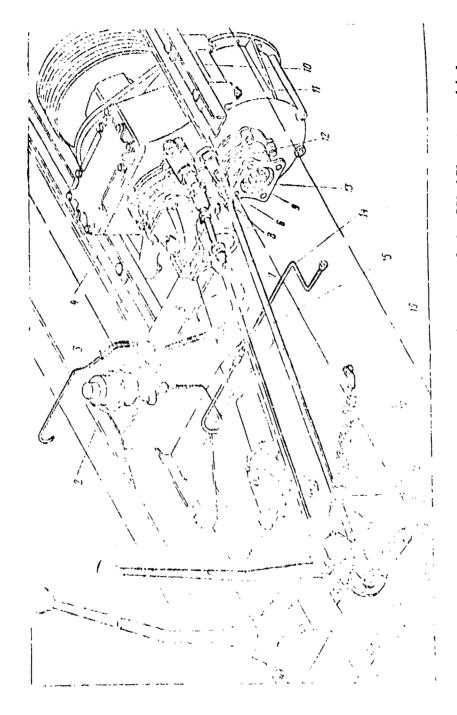
4) lever position during engagement of high speed 5) lever position during engagement of front azle 6) adjusting bolt 7) stop put 2) and characteristics.

7) stop nut 8) speed changing rod 9) control lever shaft 10) front axle engaging rod lever 11) fork 12) front axle engaging rod

Release the lever of the hydraulic jack together with the transfer case, and roll the hydraulic jack with the transfer case from beneath the motor vehicle.

Remove the suspension parts from the transfer case and from the frame of the motor vehicle.

Disassembly of the transfer case from a ZIL-157K motor vehicle. Before disassembling the transfer case, clean the dirt and oil from it, wash it off, and blow it off with compressed air, and remove the handbrake drum from the splined end of the transfer case output shaft. It is recommended that the transfer case be disassembled on a low bench or on a special device.



flange for 14) pipe for air supply to electromagnetic valve 11) transfer case fastening bolt 12) low speed speed engaging rod 16) high speed engaging rod 17) return spring 18) transmission Control linkage for the transfer case of the ZIL-131 motor vehicle: 8) stop nut 9) 4) transfer case air-diaphragm chamber 3) vent pipe 1) speed selecting lever 2) electro-pneumatic valve engaging shaft [3] high speed engaging shaft [5] low speed engaging shaft front axle drive shaft 10) longit dinal rail 6) rod fork hose to zir-diaphragm chamber Plate 8-6.

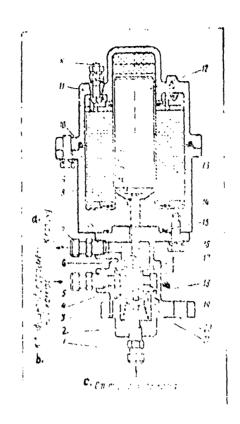


Plate 8-7. Electro-pneumatic valve: 1, 5, and 7) fittings 2) plug 3) valve spring 4) valve seat 6)out-let valve 8) electromagnet body 9 and 16) boits 10, 15, and 18) packing rings 11) cover 12) core
13) electromagnet core 14) spacing washer 17) rod 19) body 20)outlet
21) nut

Key: a) to vent
b) to air-diaphragm chamber
c) from brake valve

Removal of the flanges from the transfer case shafts. Before removing the flanges, it is necessary to remove the cover and gasket and block the gears so that the transfer case shafts cannot rotate. Unpin and unscrew the nuts fastening each flange in order, and remove them with a 20P-7968 puller (Plate 8-10).

There are a total of four flanges on the case. All the flanges are removed together with the dust guards fastened to them.

Disasserwily of the speed changing mechanism (Plate 8-11). For removal of rod 1, it is necessary to unscrew plug 4 of the catch lock and remove spring 5 and ball 3 from their recess. Unscrewing the catch lock plug is shown in Plate 8-12, a. Unpin the tension bolt 6 (see Plate 8-11), fastening gear changing fork 11, and unscrew the bolt with an angular socket wrench (see Plate 8-12, b). Insert metal rod 1 in the hole in rod 2 (Plate 8-13) and, rotating rod 2, unscrew it from the threaded hole in the fork, and then remove fork 7 from the rod (see Plate 8-11), and pull out the rod.

If the seal 2 of the rod is not in proper condition, it must be pressed out

Removal of the transfer case side cover. Unscrew the bolts fastening the side cover with a socket wrench. Lightly tapping with a hammer, separate the cover with a screwdriver, inserting it in the space opposite the catch lock. Remove the side cover together with the driven shaft.

Disassembly of the driven shaft and its bearing carriers. Unscrew the bolt fastening cover 34 (see Plate 8-1) of the rear driven shaft bearing, remove the cover in assembly with its sea and gaskets, and remove the supporting ring. Unscrew the bolts fastening carrier 26 of the bearings, and press out the driven shaft (Plate 8-14, a). With this, simultaneously press off the rear bearing of the driven shaft. After this, remove the adjusting washers and the spacing bushing.

Turn the side cover over, set it on blocks, press out the bearing carrier with a mandrel, and remove its gaskets. Press the outer race on the bearing from its recess in the side cover. This operation is accomplished with a hammer and mandrel.

During disassembly of the driven shaft, it is necessary to press the outer race of the rear input shaft bearing from its recess with a puller (Plate 8-14b).

Pross the innor race of the front bearing from the driven shaft with a puller (Plate 8-1% c).

The puller shown in Plate 8-14, b, should be used for pressing off the outer races (Plate 8-15) of the front 1 and rear 3 bearings of the driven shaft from the bearing recesses in the housing.

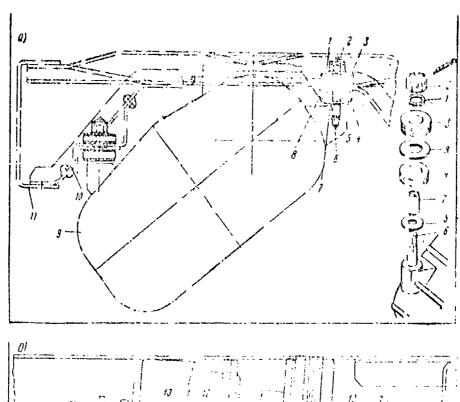


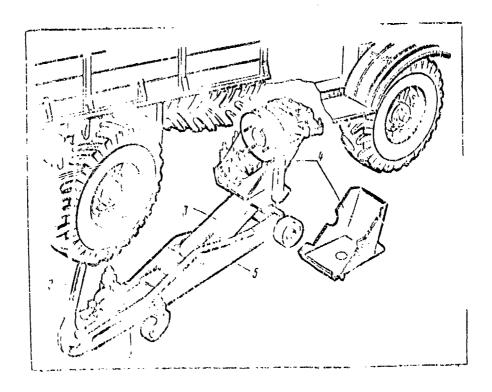


Plate 8-8. Transfer case suspension:

a) ZIL-15/K motor vehicle 5) ZIL-131 motor vehicle 1, 5, and 8) washers

2) nut 3 and 4) upper and lower bushings 6) stud 7) spacing bushing

9) transfer case 10 rail for fastenin, transfer case 11) frame 12) bolts



ARITH THINGS TOWNS . . .

Plate 8-9. Removing the transfer case from the ZIL-157K motor vehicle:

1) jack cylinder 2) handle 3) lever 4) receptable

1) jack cylinder 2) handle 3) lever 4) receptable
5) jack body

Removal and disassembly of the middle axle output shaft. Before removing the output shaft for the middle axle, it is necessary to unscrew the bolts fastening the bearing cover, remove the protector ring, the cover in assembly with the seal, the adjusting and packing gaskets, and the oil deflecting ring.

Pull the shaft 52 (see Plate 3-1) of the middle axle drive from the housing.

For pressing off the front bearing it is necessary to fasten the shaft in a vise in assembly with its gear and bearings, and press off the bearing with a 20P-7968 puller (Plate 8-16).

The rear hearing whould be pressed off together with the gear, with t^{-1} shaft set on supports (Plate 8-17).



Plate 8-10. Removal of the flange from the middle axle output shaft

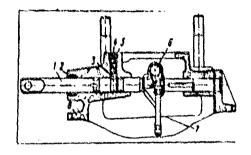


Plate 8-11. Goar changing mechanism: 1) rod 2) seat 3) catch lock ball

- 4) plug 5) spring 6) tension bolt
- 7) goar changing fork 8) transfer case housing

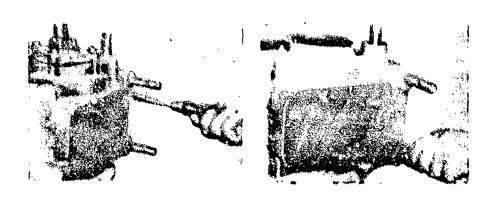


Plate 8-12. Disassembly of the transfor case gear changing mechanism:

a) unscrewing the catch lock plug b) unscrewing the fork tension boit

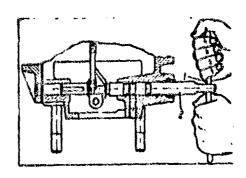


Plate 8-13. Removal of the gear changing mechanism rod:
1) metal handle 2) rod

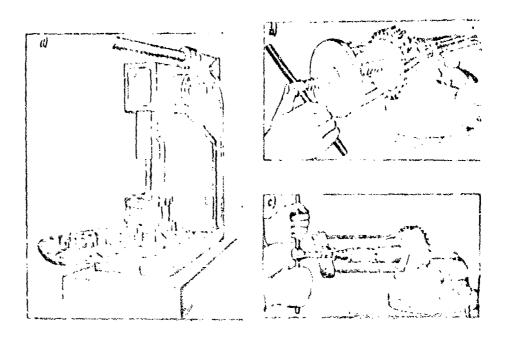


Plate 8-14. Disassembly of the driven shaft unit:
a) pressing out the driven shaft b) pressing the rear input shaft bearing outer race out of the recess in the goar
c) pressing the front bearing off the driven shaft

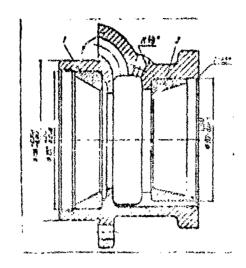


Plate 8-15. The driven shaft bearing carrier in assembly with the bearing races:

1 and 3) bearing outside races
2) bearing carrier

Removal and disassembly of the input shaft. Before removing the shaft, it is necessary to unscrew the bolts fastering the bearing cover, remove the cover in assembly with its seal, lightly tapping on them with a hammer, and remove the adjusting and packing gaskets.

Withdraw the shaft in assembly with the gears and hearings. Press off the bearing inner races with a 20P-7958 puller or with a press (Plate 8-18, a). Remove gear 22 (see Plate 8-1), support washer 19, gear 21, and steel bushing 12 from the shaft. If the bushing fits rightly on the shaft, it must be pressed off with a mandrel and hammer. If the bronze bushing is worn, it is pressed out of the ridge in the gear with a mandrel and hammer.

Removal and disassembly of the bearing carrier and front axle output shaft. For removal of the bearing carrier of the front axle output shaft, it is necessary to unscreware bolts fastening cover 50 (see Plate 8-1) of the bearing, remove the protective ring and cover in assembly with its seal.

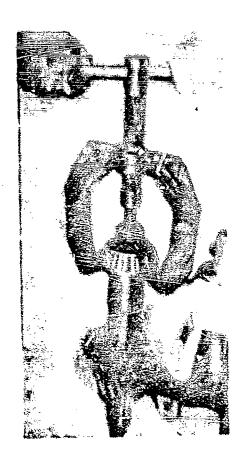
Remove the adjusting gaskets, the packing ring, and the oil deflecting ring.

Unscrew the bolts factoring shaft bearing carrier 54 and resove it by hand, lightly tapping on it with a harmon. Remove the bearing carrier gasket.

The bearing cerries of the front axie output shaft may be emoved from the transfer case is assembly with the bearing cover 60 and flange 1.

In this case, it is necessary to unsured the bolts fastening the bearing carrier and remove it in assembly with the shaft, hearings, and cover.

For disassembly of the Front aris output shaft bearing carrier, it is necessary to unscrew the nut fastening flange I and reserve the support washer and flange. Unscrew the bolts fastening the carrier cover, and reserve the dust cover 62, bearing cover 60, oil deflecting washer 2, the support washer, and the adjusting gaskets 59. If the seal 61 is not in proper condition, it should be pressed out of the cover.



Place 5-16. Pressing the front bearing off the middle axis output shaft

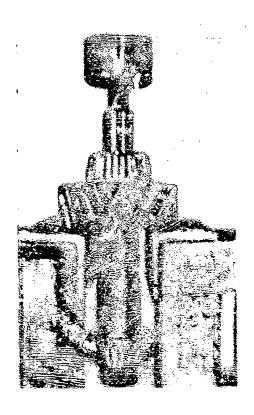


Plate 5-1". Pressing the gear and rear bearing off the middle asia out-

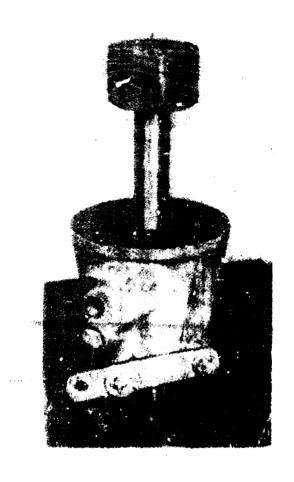


Plate 8-19. Pressing the front axle output shaft bearings from their carrier

For removal of the intermediate shaft rear bearing cover, it is necessary to unscrew the bolts and remove the cover and sealing and adjusting gaskets.

Remove the intermediate shaft in assembly from the housing.

For disassembly of the intermediate shaft, it is necessary to fasten it in a vise, bend down the ears of the lock washers (Plate 8-22,a), unscrew the number fastening the worm gear and bearings with a special wrench (Plate 8-22, b), and remove the lock washer and one support washer.

In ghtly tapping with a hammer, remove the speedometer worm gear from the shaft and drive the key from its keyway.

Press off the bearing together with the constant engagement gear with a press, using the device shown in Plate 8-23.

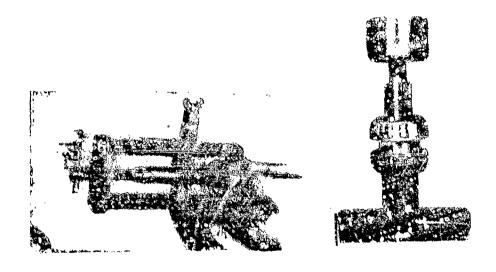
Press off the rear bearing and rear and middle axle drive gear with the same device.

Press off the low spee gear across the front end of the shaft, using the same device but without the angle irons.

If there are cracks in the cast iron parts of the transfer case, the parts should be replaced. If the bearing holes are worn more than the allowable dimensions, the transfer case housing should be renewed by pressing in repair bushings.

Damage to threads in the cast iron parts is not allowed to cover more than two turns.

Non-parallelness and deviation from the common plane of the nole axis for bearings in the carrier and cover is not allowed to be greater than 0.75 mm for a longth of 250 mm. The carrier and side cover of the transfer case are machined together and comprise a unit. If one of the parts of this unit fails, the two parts should be replaced simultaneously. Their installation with parts from other units is not admissible.

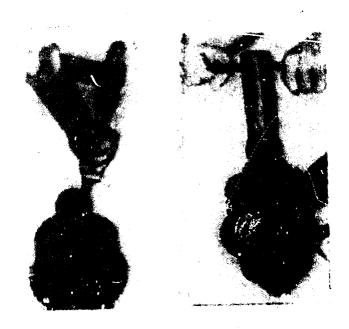


Place 8-20. Pressing the bearings from the front axle output shaft:

- a) with a puller
- b) with a press



Plate of the speedometer driven sear



Place 3-22. Disassembly of the intermediate shaft:

a) bending down the lock washer ears
b) enscrewing the nut fastening the worm gear and beaulugs

Non-parallelness of the flange faces and centering collar of the cover must be no greater than 0.05 mm. There must be no damaged on the splined assembly surfaces of the flange.

Nicks on the flange surfaces should be smoothed off.

Cracks on the flanges should be welled, or the flanges should be exchanged

Damaged threads on the flange fastening nuts are allowed to cover no more than 1-1.5 turns.

If the shaft journals and splines are worn more than the dimensions allowable without repair, or if bending or twisting are present, the shaft should be replaced.

If there are noticeable *races of wear, increased slack of chips in the bearings, or cracks in the races or chips and corrosion on a fifth of the working surfaces, the bearings should be replaced.

Oscillation on the exterior diameter of the input shaft steel bushing is not allowed to be greater than 0.03 mm. Oscillation on the bushing faces is not allowed to be greater than 0.08 mm.

Oscillation on the journals of the input, output, and intermediate shafts at the bearings is not allowed to be greater than 0.04 mm.

Oscillation of the faces on transfer case gears is no greater than 0.05 $\,\mathrm{mm}_\odot$ If there are cracks or great wear on the teeth or splines of the gears, they should be replaced.

Small chips on the faces of the teeth should be smoothed off.

Chips on the working surfaces are not allowed.

Small failure-type depressions (pitting) on the working surfaces of the gear teeth are allowed on an area no greater than 15% of the entire surface. Sharp edges, small chips, or burrs on the gear teeth should be smoothed off.

Oscillation of the face of the middle axle output shaft where it fits against the bearing is not allowed to be greater than 0.06 mm.

The speed engagement rod is not allowed to be bent more than 0.1 mm. Bent rods may be repaired by straightening.

If the surfaces of the rods are worn more than the allowable dimensions, they should be replaced or have their surfaces reneved by chroming and subsequent machining.

Wear on the passages in the rods for the catch lock balls is allowed as long as the clearance between the shaped template and the depression does not exceed 0.6 mm. If the wear is greater than this, the rods should be replaced.

If there are cracks, chips, or wear on the fingers of the goar engaging forks above the allowable dimensions, the forks should be replaced.

Bent forks may be repaired by straightening.

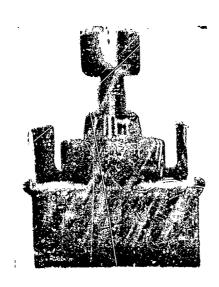


Plate 8-23. Pressing the front bearing off the intermediate shaft together with the gear

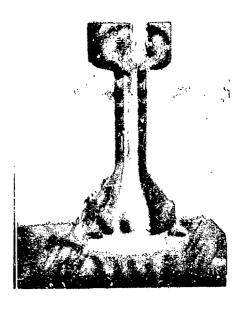
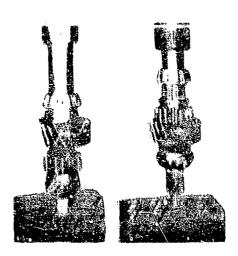


Plate 8-24. Pressing the seal into its recess in the front axle output shaft bearing cover



Place 8-25. Pressing the bearings onto the input shaft
a) front bearing
b) rear bearing

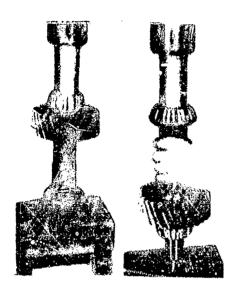


Plate 8-26. Pressing the bearings onto the middle axle output shaft a) rear bearing b) front bearing

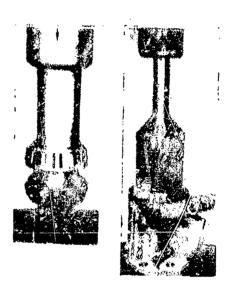


Plate 8-27. Assembling the front axle output shaft bearing carrier a) pressing the bearings onto the shaft journal b) pressing on the front shaft bearing outside race

Assembly of the transfer case of the 21L-157K motor vehicle. Assembly of the housing and bearing cover.

Using a press and mandrel, press the outside races of the middle axle output shaft, termediate, and input shaft hearings into their recesses. Screw the plugs into the drain, filler, and control holes.

If recessary, replace or serow in the transfer case suspension studs.

Press soals into all the bearing covers (Plate 8-24).

Ascembly of the input shaft. Press the bronze bus are the input gear 21 (see Plate 8-1) with an interference of 0.12-0.28 mm. The edges of the bushings are bent into the two slots in the gear hub. Install steel bushing 12 on the shaft, guiding its pin 20 into the slot in the shaft. In this operation, a mandrel and hammer should be used, fitting the bushing into place. The bushing fits on the shaft journal with a clearance of 0.024 mm or an interference of 0.02 mm. Install the drive gear with its bronze bushing in assembly on the steel bushing, mount the support washer 19 on the shaft, and press front bearing 18 on the shaft journal (with an interference of 0.003-0.020 mm). Install the

low and high range engaging gear 22 on the shaft, and press the rear hearing 24 on the shaft journal (interference is 0.018-0.035 mm). The method of pressing the hearings on is shown in Plate 8-25.

Assembly of the middle axle output shaft. Install the gear on the shaft splines and fit it into place with a hand press or mandrel (conic rate of the splined shaft connection is 1 : 8 on the length of the journal. Press on the front and rear bearings (interference is 0.018-0.035 mm for the front hearing and 0.009-0.027 mm for the rear bearings.

The method of pressing the bearings on is shown in Place 8-26.

Assembly of the front axle output shaft bearing carrier. Install the rear hearing, spacing ring, and front bearing on the front axle output saaft, pressing both bearings (with an interference of 0.009-0.027 mm) on the shaft journal simultaneously (Plate 8-27, a).

Press the shaft rear bearing outside sece into its recess in the housing (interference is no greater than 0.026 mm). Press the rod seal into its recess in the bearing carrier. Insert the rod in the hole in the bearing carrier and mount the changing fork on it. Connect the rod with the drive plate.

install the shaft with the bearings in assembly in the bearing carrier and press on the front bearing outer race (Plate 8-27, b) (interference no greater than 0.026 mm).

Mount the front axle engagement sleeve 56 on the splined end of the shaft (see Plate 8-1), and install engaging fork 55 in its slot. Fasten the fork by tightening stop screw 5 with a screwdriver, and screw plug 8 into the hole in the bearing carrier.

Install ball 4 of the catch lock with spring 6 in their recess in the carrier, and fasten them with plug 7.

Install the packing and adjusting gaskets on the bearing carrier, mount the support and oil deflecting rings, install the bearing cover with its protector ring, and fasten it with bolts. The front exle output shaft turns freely, without perceptible axial clearance. In cases where the shaft turns tightly or has an axial clearance, it is necessary to adjust the tension on the bearings with a selection of the required number of adjusting gaskets (Plate 8-28).

Install the flange on the splined end of the shaft and mount the support pasher. Screwing in the nut, seat the flange in place and pin the nut. The set of the flange on the splined end is a sliding one.

Assembly of the intermediate shaft. Press the driving gear 39 (see Plate 8-1) of the middle and rear axle drives on the shaft (conic rate of the splined connection of the shaft is 1:8 on the length of the journal). Press on rear bearing 38 (interference is 0.009-0.027 mm), install the support and

lock washers 35 on the shaft, and fasten the unit with nut 36. The nut is locked by bending ears on the lock washer up into slots in the nut. Install the key in its keyway in the shaft. The key fits with a clearance of 0.40 mm or an interference of 0.060 mm. Press on the low range gear (Plate 8-29).

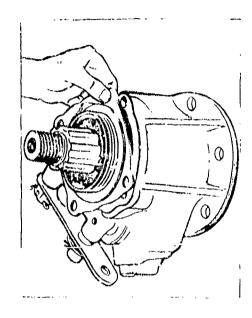


Plate 8-28. Adjustment of tension on the front axle power shaft bearings

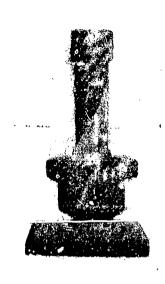


Plate 8-29 Pressing the low range gear onto the intermediate shaft

Press on constant engagement gear 51 (see Plate 8-1) and the front bearing 9.

The monic rate of the splined connection and the amount of interference on the loaring is the same as on the other end of the shaft. Install the key in keyway in the shaft, and mount the speedometer drive worm gear, fitting it into place with a mandrel and hammer. Install the lock washer and fasten the unit with a nut, locking it by bending up the ears on the lock washer into the slots in the nut.

Ascembly of the driven shaft. Press the outer race of the input shaft resubsaring into the recess of the toothed ring (interference is $0.025 \times .050$ mm). Press on the inner ring of its front bearing.

Assembly of the transfer case wide cover and installation of the driven shaft. Press the outer races of the middle axle output shaft and the intermediate shaft into their recesses in the cover (interferen. is no greater than 0.02 0.026 mm). Press outer races 1 and 3 (see Plate 8-15) into the driven shaft bearing carrier (interference is 0.01-0.05 mm). Press the bearing carrier in

assembly with its rings into the recess in the cover (interference is no greater than 0.048 mm). Install the driven shaft in the bearing carrier, insert the bearing spacing bushing, mount the adjusting weshers on the shaft (Plate 8-30, a) and press on the rear bearing. The transfer case driven shaft must turn freely without perceptible axial clearance. Mount the support washer, install the bearing cover with its gasket, and fasten it with bolts. Install the flange (the fit is free) and fasten it with a nut. Check the tension on the bearings, rotating the shaft with a dynamometer (Plate 8-30, h). The moment of shaft rotation must be within the limits of 0.05-0.13 kg meters (force on the dynamometer is 0.99-2.50 kg). The front axle output shaft must also turn with the same moment and force.

In a case where the moment of shaft rotation lies outside the limit of the indicated parameters, it is necessary to perform adjustments, changing the thickness and rumber of the adjusting washers (see Plate 8-30, a).

Install the intermediate shaft bearing cover with its packing and adjusting gaskets in the transfer case cover, and fasten it with bolts. Install the support ring on the face of the inner race of the middle axle power output shaft bearing. Lay the oil deflecting washer into its recess in the bearing cover, install the middle axle power output shaft bearing cover with its packing and adjusting gaskets, install the protector ring on the cover, and fasten it to the transfer case cover.

General assembly of the transfer case. Set the transfer case housing on a bench with its open side up, and lay wooden blocks beneath it so that the ends of the shaft do not rest on the bench. Install the input shaft 14 (see Plate 5-1), incomediate shaft 50, and middle axle output shaft 52.

The assembled transfer case cover must be installed on the transfer case housing by laying the sealing gasket and guiding the shaft bearings in their correspinding outer races, which are pressed into the covers in the cover.

Placing spring washers beneath the bolt heads, screw in the holts by hand and fasten the cover with bolts. It is recommended that an angle socket wrench be used to tighten the bolts.

Install the bearing carrier of the from axle output shaff on the transfer case housing in assembly with its bearings, fealing gaskets, and adjusting gaskets, and casten it with bolts.

Having also in'd the scaling and adjusting gaskets, install the intermediate shaft front bearing cover, and fasten it with holts. Insert the speedometer drive driven gear cover in its recess, and fasten its tension nut.

Having mounted the realing and adjusting geokets, install the input shaft front bearing cover and fuston it with bolts. Install the flange and faston it with the nut.

Assemble the gear changing mechanism (see Plate 8-11), for which seal 2 of rod 1 is present into the recess in the housing, the rod is inserted into the hole, and fork 7 is mounted onto the end of the rod through the hole in the housing, and the fork ends are guided into the slot in the gear. Insert a metal handle into the hole in the rod and, turning the rod, screw it into the threaded hole in the fork. During this, the high and low range engaging gear must be in the neutral position. Pasten fork 7 with tension bolt 6 and pin the bolt with wire. Install bolt 3, spring 5, and plug 4 of the catch lock in their recess. Closs the inspection hole with its cover and gasket, and fasten the cover with bolts and washers.

Adjustment of the ZIL-157K transfer case. The following must be adjusted in the transfer case: tightness of the tapered coller bearings; the position of the faces of the gear teeth of the input, intermediate, and driven shafts; the neutral position of the high and low range engagement gear; and the simultaneous engagement of the front axle and low range.

Bearing tightness is adjusted by changing the number of adjusting gaskets installed beneath their covers (in the output shaft, gaskets are installed between the spacing bushing and the inner race of the rear hearing.).

Adjustment of the bearings of the driven shaft and front axle power output shaft takes place during assembly of the units.

lirst adjust the driven shaft bearings. They are adjusted after final tightening of the driven shaft bearing carrier 26 (see Plate 8-1) onto lover 46 of the transfer case housing.

After adjusting the driven shaft bearings, the input shaft bearings are adjusted, and then the intermediate shaft bearings and the middle axle output shaft bearings.

The bearing on the front axie output shaft may be adjusted with the front axie output shaft housing 54 removed. With the bearings normally adjusted and the covers fastened, the shafts must turn freely by hand but must not have any axial clearance. Tightness of the input shaft bearings may be checked by means of turning the shaft with a dynamic ster. The method of turning the shaft is shown in Plate 8-30, b. The moment on shaft rotation must lie within the limits of 0.05-0.13 kg meters (a force of 0.99-2.50 kg). During the rotation of the shaft, the bearing cover bolts and flunge nuts must be tightened all the way.

Adjustment of the position of gene teeth faces is provided by tightening the intermediate shaft hearings. In this, first adjust the hearings, and then move the shaft forward and hackward, changing the thickness of the gaskets between the intermediate shaft hearing cover on both ends of the case (see Plate > 30, a and f).

With a decreased gasket thickness on one side, thickness of the gaskets on the other time should be increased by the same amount. The adjustment may be considered first if the distance from one year to the other along the faces of

their teeth is identical in both rows. During this, the gear teeth faces must be located in a single line, as shown in Plate 8-2, a.

Setting of the high and low range engagement gear in the neutral position is done by screwing rod 1 (see Plate 8-11) into fork 7 until the teeth faces of the input shaft drive gear touch those of the speed engagement gear. When the gears touch, it is necessary to unscrew the rod back by 1/3-1 revolution, checking to make sure that the axis of the hole for the rod pin is parallel to the assembly plane of the inspliction hole. After setting the fork in the required position, it is necessary to fasten it with its tension bolt 6 and pin it with wire. The neutral position of the transfer case is shown in Plate 8-2, a. Plate 8-2, b, shows the simultaneous engagement of the gears for low range and front axle drive, and Plate 8-2, c, shows high range engagement.

Installation of the transfer case in the motor vehicle. Set the transfer case into its receptacle 4 (see Plate 8-9) and roll the hydraulic jack, together with the case, under the motor vehicle. Pumping handle 2, raise the transfer case, guiding its fastuning study into the holes in the frame cross member, having previously mounted the rubber lower suspension cushions 4 (see Plate 8-8, a) on the study. Install the upper cushions 3 on the study, screw on nuts 2, and tighten the transfer case. The nuts are pinned.

Adjusting the transfer case control linkage. Install rods 8 and 12 (see Plate 8-5), and fasten their rear ends with pins on the rods for engaging the transfer case shift and engaging the front axle.

Simultaneous engagement (interlocking) of the front axle and low range in the transfer case is achieved by adjusting the position of bolt 6, which is screwed into the lower end of the front axie engaging lever.

For adjusting the simultaneous engagement of the front axle and low range, it is necessary to set the front axle engaging rod in the "front axle engaged" position, and set the speed changing rod in the position corresponding to engagement of low range. In this, full engagement is determined by the clicking of the catch lock when it falls into the detent in the rod.

When low range is engaged, the speed shifting rod is in a position such that the mark placed on the lower side of the rod with a punch must be located at a distance of 40 mm from the machined end of the boss face on the housing

Interlocking of front axle and low range engagement in the transfer case must be adjusted in the following sequence. Set transfer case control lever 4 in a position so that it is inclined forward at an angle of approximately 15 from the vertical position, and connect the front end of rod 8 to the lover, adjusting the length of the lever by turning fork 11. Place cotter is the rod pins.

Set front aske engagement lever 5 so that it is inclined forward at an angle of approximately 15" from the vertical position, unacrew adjust ig bolt 6 of the lever until the bolt head touches the boss on transfer case control lever 4, and fasten the bolt with nut?

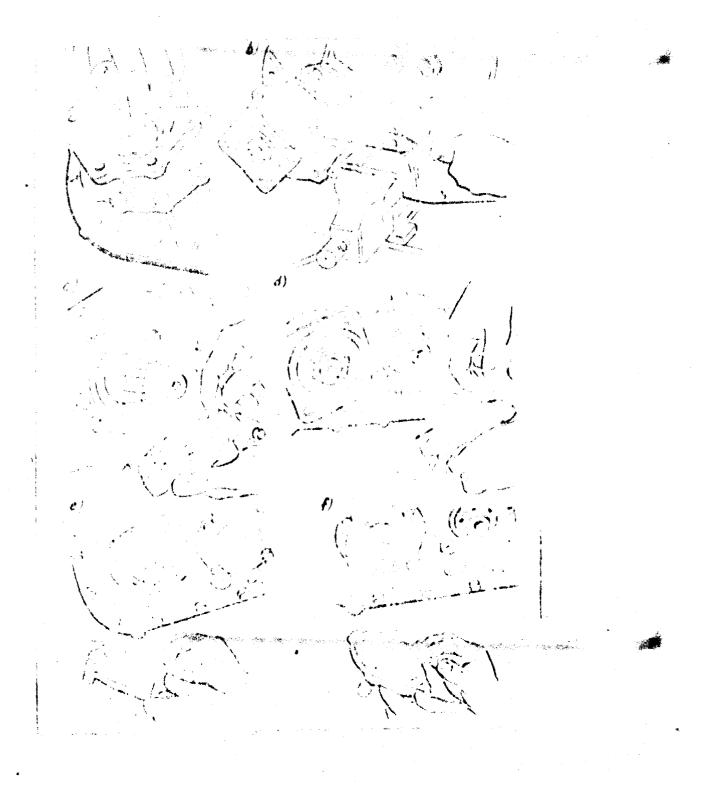


Plate 3-30. Merhods of adjusting bearing tightness:

a) changing the number of washers on the driven shaft bearing b) checking driven shaft bearing tightness c) changing the number of gaskets in the input shaft bearing d) changing the number of gaskets in the front bearing of the intermediate shaft e) changing the number of gaskets in the front axle output shaft bearing f) changing the number of gaskets in the intermediate shaft rear bearing

Connect the front and of front axis engaging rod 12 to lever 10, adjusting its length by turning fork 11, and place cotter keys in the rod pin.

the proper setting and adjusting of the length of the transfer case control rods are checked during a short run of the motor vehicle by means of engaging the gears and disengaging the front axle with simultaneous disengagement of low range.

Removal of the transfer case from the 211.131 tor vehicle. Disconnect the propellor shafts, control linkage rods, handbrake centrol rod, air hose, and electric wire to the electric switch from the transfer case. Roll a model 444 hydraulic lack beneath the motor vehicle. Remove the transfer case (see Plate 8-9).

Unpin the nats, release the suspension bolts, lower the transfer case on the hydraulic jack, and roll it out from beneath the motor vehicle together with the transfer case. Remove the suspension parts from the transfer case and from the motor vehicle frame.

Installation of the transfer case in the motor vehicle is accomplished in a sequence opposite to that of removal.

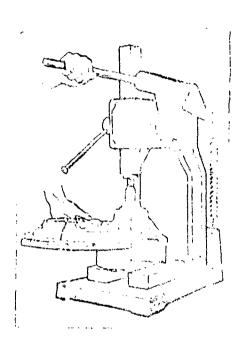
Disassembly of the transfer case of the ZIL-131 motor vehicle. Before disassembling the transfer case, it is necessary to clean the dirt and oil from it, wash it off and blow it off with compressed air, remove the handbrake together with the drem 21 (see Plate 8-3) and the frange from the splined end of the output shaft, unscrow switches 43 and 48, and remove them together with their scaling and adjusting washers.

Removing the flanges. For removal of the front flanges 8 and 11, it is necessary to open cover 17 of the inspection hole. Unscrew the nuts fasten the cover, pmove the parts of the handbrake linkage, and remove cover 17 with its gasket. Block the goars so that the transfer case shafts cannot turn. Unscrew nut 9 fastening the flange, and remove it with a 20P-7968 puller. Remove the other flanges in the same manner. There are a total of three flanges on the transfer case.

Removal and disassembly of the transfer case side cover. Unscrow the boits fastoning the cover with the socket wrench. Lightly tapping on it with a hammer, separate the cover using a scrowdriver, insorting it in the notch opposite the catch lock.

Remove the cover together with the driven theft and the outer race of the trent alle power shaft bearing. Unscrow the bolts fastening bearing cover 24 and tamove the cover with its sealing gasket. Press the outer race of the front gate rations shaft relier bearing out of its recess in the cover with a mandrel and harmer.

Friends the bolts fritoring the stop plate 27 of the speedometer fitting. Remove to locking plate, and pull out fitting 27 and the speedometer driven year 29.



Piste 8-31. Pressing out the driven shaft

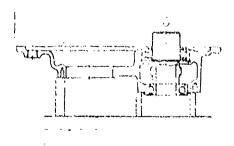


Plate 8-33. Pressing the driven chaft rear bearing out of the cover

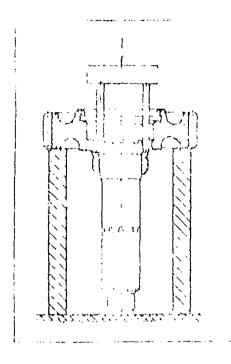


Plate 8-32. Pressing out the inner race of the driven shaft front bearing



Plate 8-34. Pressing the outer race of the driven shaft front Learing from the cover

Disassembly of the driven shaft. Install the housing side cover with blocks on a borch press, and press out the driven shaft with its gear (Plate 8-31). During this operation, the driven shaft rear bearing is pressed out. In order to remove the inner race of the roller bearing from the driven shaft, it is necessary to set the gear on a support, guide the pins of the device through the hole in the gear hub, and rest them on the bearing race, fater which the race is pressed off the shaft with the press (Plate 8-32).

In order to drive the driven shaft rear bearing from the housing cover, it is necessary to set the cover on a support, and, using a hammer and mandrel (Plate 8-33), press out the bearing together with the speedemeter worm gear. Turning the cover over and setting it on a support, press out the outer race of the driven shaft front hearing (Plate 8-34), using a mandrel and hammer.

Disassembly of the gear changing mechanism. Plate 8-3 (Section 8--0) shows the gear changing mechanism. In order to remove rods 36 and 47, it is necessary to unpin step belts 34, fastening gear changing focks 33 and 35, and unscrew them. After this, unscrew the belts fastening catch lock body 45 with a socker wrench, and, using a screwdriver, knock out both rods, first from the forks, and then together with the catch lock body from the housing. Withdraw both forks 33 and 35 from the circular slots in their respective carriers 16 and 31, and from transfe, case housing 1. Unscrew plug 37 of the catch lock, and remove spring 38 and ball 39.

Set rods 36 and 47 in the neutral position. Knock out one of the rods and then remove ball 46 of the blocking mechanism. Knock out the second rod. Both rods cannot be knocked out simultaneously, nor can one rod be knocked out without the second one in the neutral position, since this will lead to breakage of the blocking mechanism. If the rod seals are not in proper condition, unscreen nut 42 of the seal and replace rubber 40 and felt 41 rings.

Removal and disassembly of the front axle drive engaging mechanism. Flate 8-3 (Section E--E) shows the front axle drive engaging mechanism. For removal of the mechanism, it is necessary to unpin step bolt 34 fastening front axle drive engaging fork 22, anscrew it from the fork, unscrew the bolts fastening body 49 of the air-diaphragm chamber 10 of the front axle drive, and, using a screwdriver, first knock rod 52 out of the fork, and then out of the transfer case housing 1. The scaling and packing gaskets 53 are removed simultaneously with the front axle drive on iging chamber. After this, remove fork 22 from the circular old in carrier 23 and from the transfer case housing.

Further disassembly of the mechanism takes place in the following order. Unscrew holts 2 (see Plate 8-4) fastening cover 3 of the engaging chamber, remove the cover and the diaphragm 1, and remove external rod 5 in assembly from the body 4. For disassembly of the external rod of the mechanism, it is necessary to insert a special 10 mm wrench between the coils of the return spring 19 and grasp the internal rod 9 on its flat 12. Then unscrew cup 6 of the rod spring either by hand or in a vise, remove the wrench from the spring, and remove return spring 13. Holding external rod 5 in a vise, remove stop ring 7 with a screwdriver and hammer. After this, pull the internal rod 9 in assembly from the hollow in the external rod. Then, after unscrewing the stop nut and nut 11, remove compression spring 10 and support washer 8.

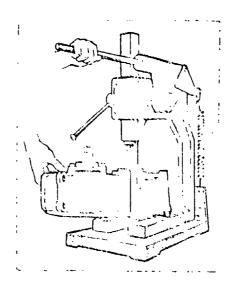


Plate 8-35. Pressing out the front axle output shaft

Removal and disassembly of the front axle power shaft. Remove cover 5 (see Plate 8-3) of the power shaft frost bearing. For this, unscrew the bolts fastoning the cover, remove the cover in assembly with its seal, and remove the scaling gasket. If the scal in the cover is not in proper condition, it should he presend out of the cover with a mandrel and hammer. Remove the oil deflecting ring 6 and currier 23 from the shart. Before removing the front axle power shaft, it is necessary to move it somewhat forward in the housing by tapping on the rear tace of the shaft, so that the bearing lock ring moves away from the housing wall. Then remove the stop ring from the circular slot in the bearing with combination pliers. After thic, set the housing on a support and press the front axle power shaft in assembly with its hearing (Plate 8-35) from its receptacle in the housing with a mandrel and hammer or with a press. For disas early of the shaft, it is necessary to set it on support 13 (Plate 8-36) and press the ball bearing 2 from the from face of shaft i with a mandrel and h. mer or with a press. Then remove support washer 3, low range goar 4 with its needle bearing 12, low range carrier 5, and high range goar 6 with its needle bearing. If necessary (for replacing the searing or repairing the shaft), remove inner race 7 of the rear bearing from the snaft. For this, it is first necessary to remove stop ring 3 with combination pliers or a screwdriver, and then press the bearing inner race 7 from the shaft (Plate 8-37) with a 20P-7968 puller and a spacial ring. After this, remove the needle begings 12 and intermediate rings 11 and 9 from goars 4 (see Plate 8-36) and 6, and also remove the support ring 10 from low range goar 4. The needle bearing does not have a separator, and therefore it is necessary to la, them in a separate box to avoid losing the needles.



Plate 8-37. Pressing off the inner race of the front axle power shaft rear bearing

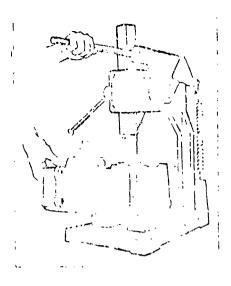


Plate 8-38. Pressing the input shaft out of the housing

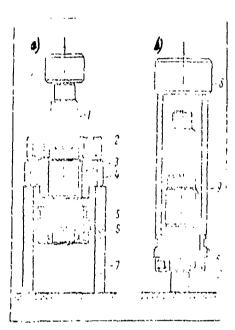


Plate 8-39. Disassembly of the input snaft:

- a) pressing off the front bearing and gear b) pressing off the rear bearing 1) shaft 2) front bearing 3) key
- 4) drive gear 5) high range engaging carrier 6) rear bearing 7 and 10) supports 8) blocks 9) mandrel

In case of necessity, it is possible to bend down the ears of the stop washer, unscrew the fastening bolts in the oil-guiding trough, and remove the trough 2 (Plate 8-3).

Romoval and disassembly of the electro-pneumatic front axle power control valve. A diagram of the transfer case centrol linkage is shown in Plate 8-6. Before removing the electro-pneumatic valve 2, pipe 14 supplying air to the valve, hose 5 supplying air to the air-diaphragm chamber 7 controlling the front axle power, and pipe 3 of the vent should be disconnected from the fittings on the valve body, and the wire should also be disconnected from the hole of the electromagnet.

After this, unscrew the nuts fastening the electromagnetic valve to the frame cross member bracket, unscrew the bolts with their stop washers, and remove the electromagnetic valve.

The electromagnetic valve (see Plate 8-7) consists of body 19 with two valves (inlet and outlet) and the electromagnet body 8.

Before disassembling the electromagnetic valve, it is necessary to lean the dirt and oil off its exterior, wash it off, and blow it off with compressed air. After this, unscrew holts 16 fastening the electromagnet and, observing caution, separate body 8 of the electromagnet from body 19 of the valve. For removal of the inlet 20 and outlet 6 valves, it is necessary to unscrew plug 2 and remove spring 3. After this, set valve body 19 vertically, and carefully, without striking them, press out the valves in assembly with seat 4 with rod 17, and remove rod 17. In case rings 18 are not in good condition, it is necessary to remove them from seat 4 with a screwdriver for replacement. If the body of the outlet valve 6 or inlet valve 20 are damaged, nut 21 holding the valves on the rod should be unscrewed, and they should be removed for replacement.

Fittings 5 and 7 should not be unscrewed from the valve body unless it is necessary, since their threads may he damaged and their tightness be destroyed, necessitating a full disassembly of the electromagnet. If necessary, the bolts 9 fastening cover 11 to body 8 of the electromagnet should be unscrewed and the cover removed in assembly with coil 13. Remove the core 12 and spacing washer 14 from the body.

If the sealing rings 10 and 15 are not in good condition, they are removed from the circular slots in the body and cover.

Having finished disassembly of the transfer case, it is necessary to wash all parts in a degreasing solution and carefully check the amount of their wear, the condition of their connecting surfaces, the absence of cracks. Then perform the assembly of the transfer case, using all usable parts.

Requirements on transfer case parts. The transfer case housing and side cover are machined together, and therefore they comprise a unit. If one of the parts of this unit fails, both of them should be replaced simultaneously.

Their installation with parts from another unit is not permissible. Cracks on parts of the case are not allowed.

Nonparallelness and deviation from the common plane of the axes of bearing holes in the housing and cover are not allowed to be greater than 0.03 mm on a length of 100 mm.

Requirements for the case, side cover, and gears of the ZIL-131 motor vehicle transfer case are similar to the requirements for those same parts in the transfer case of the ZIL-157K motor vehicle.

If there is wear in the fitting holes in the hubs of the high and low range gears or there are chips on the faces of the gear teeth which are greater than the dimensions allowable without repair, the gears should be replaced.

If splines on the shift are worn more than the dimensions allowable without repair, or also if they are bent or twisted, the shafts should be replaced. Worn out shaft journals, besides the front axle power shaft journal, intended for work with needle bearings, may be repaired. If the front axle power shaft journal is worn, it should be replaced. The following are allowed: in a new input shaft, oscillation of the surface for the gear relative to the surface for the bearing no greater than 0.05 mm; in a new driven shaft, oscillation of the hole for the input shaft bearing relative to the surface for the driven shaft bearing, no greater than 0.03 mm; in a new front axle output shaft, oscillation of the journal for the needle bearings relative to the surface for the shaft support bearing, no greater than 0.03 mm; damage to threads on the shaft for the flunge fastening nut covering no more than 1.5 thread turns.

There must be no damage to the assembly surfaces of the splined portion of the flanges. Chips in the flanges should be smoothed off. If cracks or unallowable wear are present on the flanges, they should be replaced.

If the rear faces of the splines on the currier enclosing low range and the middle axle drive become dulled, it is necessary to grind the rear face of the carrier by 0.1-0.3 mm so as to regain the sharp edges which prevent self-disengagement.

Nonparallelness of the faces of the flange and contering collar in the bearing covers must be no greater than 0.05 mm. If clearance in the bearings is increased, or there are cracks, chips, or spots of corrosion on the rings, they should be replaced.

The goar engaging rods are not allowed to be bent by more than 0.1 mm. Bent rods may be repaired by straightening. Rod surfaces which are worn more than the allowable dimensions may be repaired. Wear in the notches on the rods for the catch lock balls is allowed as long as the clearance between the shaped template and the notch does not exceed 0 6 mm. If this notch is increased, the rods should be replaced. If there are cracks, chips, or wear or the fingers of the goar changing forks above the allowable dimensions, the forks should be replaced. Eent forks may be repaired by straightening.

Assembly of the transfer case for the ZIL-131 motor vehicle. The transfer case assembly must be sufficiently tight. To this aim, the sealing gaskets of the bearing covers, housing cover, and top inspection hole cover, and also the bolts fastening the covers of the input shaft bearing, the rod catch lock body, the front axle drive engagement chamber body, and the speedometer spline are installed with non-leaking UN-25 sealing paste (VTU MKhP 3336-52) during assembly.

Parts and components prepared for assembly must be carefully washed out and blown out with compressed air.

Assembly and installation of the input shaft. With a hammer, install the key 15 (see Plate 8-3) in its keyway with a fit from clearance of 0.015 mm to interference of 0.065 mm. Press drive gear 14 onto shaft 12 either manually or with a press with an interference of from 0.003-0.047 mm, so that it is simultaneously installed with its keyway on the key. The front bearing is installed in a similar manner, with an interference of from 0.003-0.032 mm. Mount carrier 16 on the splines on the shaft. Then press the rear bearing on the shaft journal with an interference of from 0.003-0.032 mm.

Set the transfer case housing on the support on a bench. The input shaft assembly is installed in the hole for the front bearing of the carrier. With a mandrel and hammer, press the input shaft bearing in assembly with the shaft into the indicator hole with a fit from clearance of 0.038 mm to interference of 0.012 mm. In this, the circular slot on the bearing must project a small amount from the housing. Install stop ring 4 in the slot with combination pliers and a screwdriver. Press the seal into the bearing cover, install the cover logether with its sealing gasket, and fasten it on the housing with bolts. The bolt threads should be smeared with sealing paste, and spring washers should be laid beneath their heads.

Assembl and installation of the front axle power shaft. Press the inner race of the roller bearing onto the rear journal of shaft 3 with an interference of from 0.003-0.032 mm with a mandrel and hammer or press. Insert the stop ring into the circular slot with a screwdriver and hammer. Pack the hub of high range gear 25 with solid type grease and insert the rollers (57 pieces) of the bearing, and then install the intermediate ring and assemble the second roller bearing (the rollers in each bearing must not differ in diameter by more than 0.005 mm from each other). After this, carefully install the gear in assembly with the bearings on the journal of shaft 2

Install the intermediate ring in the low range goar 32 with a fit of from clearance of 0.3 mm to interference of 0.1 mm with a mandrel and hammer. Then assemble and install the needle bearings in the goar hub by the method indicated above. Carefully install the assembled low range goar on the shaft journal. Mount the support washer on the front end of the shaft, and press the front bearing on with an interference of from 0.003-0.32 mm with a mandrel and hammer or with a press.

Set the transfer case housing so that the end of the input shaft does not touch the bench. Take the front axle power shaft in assembly and insert it in the hole in the housing for the front bearing. Press the bearing into the indicated hole with a fit from clearance of 0.038 mm to interference of 0.012 mm with a mandrel and hammer in such a way that the circular slot for the stop ring in the bearing projects somewhat from the housing. Then insert stop ring 4 int the circular slot of the bearing with combination pliers and a screwdriver. Mount the oil-deflecting ring 6 on the splined end of the shaft and press it tightly to the face of the bearing. Press a seal into cover 5, install the cover together with its sealing gasket, and thread it to the housing with bolts, installing spring washers beneath the bolt heads.

Assembly and installation of the front axle drive engagement mechanism. For assembly of the air-diaphragm chamber, it is necessary to mount the first washer 8, pressure spring 10, and second washer 8 on rod 9 (see Plate 8-4). Screw nut 11 onto rod 9, and, continuing to turn the nut with a wrench, compress the spring so that the distance between the external faces of washers 8 is within the limits of 85, 55--85, 85 mm. After attaining this dimension, screw on the stop nut. Insert the assembled rod 9 into external rod 5 and fasten it with stop ring 7. Then mount return spring 13 on the end of the rod, and, inserting a wrench between its coils, grasp them by flat 12 of the rod, and scrsw cup 6 onto the threaded end of rod 9 until it stops. Removing the wrench, punch the cup in its threads to prevent its spontaneous unthreading. Insert external rod 5 in assembly with internal rod 9 in body 4 of the front axle drive engaging chamber, install diaphragm 1 with cover 3 on the body and fasten it with bolts 2 ensuring tightness of the chamber. The diaphragm should not be excessively stretched, since this will lead to undesirable movement of the flat on the rod S relative to the hole for the engaging ball in the diaphragm body.

Before installing the air-diaphragm chamber for engaging the front axle drive in the transfer case housing, it is necessary to install the adjusting gaskets 53 on its body 49 (see Plate 8-3) so as to attain a dimension within the limits of 173.9-174.1 mm from the external gasket to the axis of the hole in the rod for stop bolt 34. Then, after mounting the sealing gasket, insert the rod of the assembled front axle power engaging air-diaphragm chamber in its corresponding hole in the transfer case housing. Install front axle power engaging carrier 23 on goar 25. Insert the fingers of front axle power engaging fork 22 into the circular slot in carrier 23. Gradually moving the front axle power engaging rod into its receptable in the housing, mount fork 22 on it. Aligning the holes in the fork and the rod, screw in stop bolt 24 until its stops, and pin it with wire.

After this, faston the body of the front axle drive engaging air-diaphragm chamber to the transfer case housing with bolts and spring washers.

Assembly of the speed changing mechanism. The speed hanging mechanism is shown in Plate 8-3 (Sections B-D and H-H). Insert low range engaging rod 47 into the catch lock body 45 so that the flats are visible in all three holes for the catch lock ball (the blocking mechanism ball and the switch). Then

place the three balls 46 of the blocking mechanism in the hole between the rods. After this, insert high range engaging rod 36 and scrow in the sealing plug with a scrowdriver. Insert the speed changing rods 36 and 47 in assembly with the catch lock body 45 and sealing gasket into their corresponding holes in the transfer case housing (with a free-moving fit). Insert 16 range engaging fork 33 in the circular slot in carrier 31. Then, moving the rols late the housing, mount the engaging fork on low range rod 47. Insert the high range engaging fork 35 in the circular slot in carrier 16 and likewise mount it on rod 36. After this, move the rod until catch lock body 45 rests against the face of transfer case housing 1, and fasten body 45 to the housing with belts, placing spring washers beneath their heads. Scrow stop belts 34 into the holes in the fork splines and, moving the forks along the rods, align them to that the conic ends of the belts move into the corresponding onic holes in the rods. After this, tighten the belts with a wrench until they stop and the firm off with wire as shown in Plate 8-3, to prevent their coming unscrewed.

Insert the balls 39 and springs 38 into their recess in the catch lock body, and screw in the catch lock plug 37 until it stops.

Assembly of the transfer case housing side cover. Before assembling the side cover 18, it is necessary to prepare the driven shaft of the case, pressing the inner race of the roller bearing onto it with an interference of 0.003-0.03 mm. Then insert the outer race of the driven shaft front roller bearing into the recess in cover 18 until it stops with a fit from clearance of 0.038 mm to interference of 0.012 mm. After this, install the driven shaft with the front bearing inner race pressed on it in the outer race of this bearing, which is installed in the cover. Set the cover on supports, likewise placing supports beneath the driven shaft goars in such a way that the shaft jeurnal for the rear bearing projects from the rear face of the cover. Mount speedometer worm goar 20 and the ball bearing in assembly with its stop ring on the driven shaft. Then press the ball bearing on the shaft journal with an interference of 0.003-0.032 mm with a mandrel and hammer, and also simultaneously install the bearing into the cover hole with a fit from clearance of 0.038 mm to interference of 0.012 mm.

General assembly of the transfer case. Set the assembled transfer case housing on the bench with its open side up, and lay wooden blocks beneath it so that the ends of the shafts do not rest on the bench. Install the sealing gasket on the assembly surface of the housing, aligning the bolt holes in the housing and the gasket. After this, install the assembled cover on the housing, guiding the input shaft bearing into the corresponding recess intthe gear in driven shaft 19, with the front axle power shaft engaging rod simultaneously moving into its corresponding recess in the cover. The over must be finally centered along the installing pins. Placing spring washers be eath the bolt heads, screw in the bolts by hand and fasten the cover on with bolts. It is recommended that an angle socker wrench be used to tighten the bolts. Press the outer race of the roller bearing of the front axle power shaft 3 into the cover with the hammer and mandrel with a fit from clearance of 0.038 mm to interference of 0.012 mm. Install cover 24 of the front axle drive shaft rear bearing with its sealing gasket and fasten it with bolts, placing spring scathers

beneath the bolt heads.

Install the speciometer driven grar 29 into cover 18 on the housing so that the front journal of the gear goes into the corresponding recess. The cover with a clearance of 0.135 mm. After this, mount fitting 27 together with its rubber seal onto the speedcmeter gear with a clearance of 0.026-0.13 mm, simultaneously inserting the fitting into the hole in the housing cover with a clearance of 0.066 mm. Install the locking plate 28 on the speedometer fitting, and fasten it with a belt and spring washer. Screw the drain hole plug 28 and filler hole plug 7 in 5 the housing cover. Mount rubber 40 and felt 41 packing rings on the low and high range engaging rods, insert them in the catch lock body recess, and fasten them with spring nuts 42. The auts should be tightened until the packing rings press against the rods along their deameters, and the rods must move freely along their axes into the body.

Install the driven shaft rear bearing cover together with its sealing gasket in assembly with hand brake mechanism on the transfer case housing cover. The cover must be centered along the external diameter of the bearing and with the installing pins.

Placing spring washers beneath the bolt heads, fasten the cover with bolts. Mount the splined flange in assembly with the handbrake drum on the driven shaft, mount the support washer, and fasten the flange with a nut until it is seed in Install and fasten flanges 8 and 11 on the input shaft and the front axle power shaft by a similar method. Install cover 17 with its sealing gasket on the study of the transfer case housing inspection hole, and then install the parts of the handbrake linkage on the inspection cover. After this, fasten the cover and brake parts to the housing and, having installed spring washers and nuts on the study, tighten the latter until they are firmly seated.

Checking the proper assembly of the transfer case. Alternately insert the metal handle into the hole and with a hammer move the rod into the extreme left position until the catch lock clicks. Both rods must project from the transfer case by an equal amount. In this position of the rod, the transfer case is ast in noutral. If the driven shaft is turned by the handbrake drive, the flanges of the input shaft and the front axle power shaft must not turn. If the rods are moved alternately into the housing, i.e., engaging low or high range, then with rotation of the driven shaft, the input shaft must rotate, and the front axle power shaft must be stationary. If air is supplied to the front axle drive engaging chamber under a pressure of no less than 5 kg/cm², the front axle drive must engage. Consequently, with rotation of the driven shaft, the front axle power shaft flange must also rotate regardless of engagement of either range or neutral position of the transfer case. No adjustments besides those indicated above during assembly of the front axle drive engaging chamber are foreseen in the transfer case.

Assembly of the electro-pnoumatic valve for front axle drive control in the transfer case. The assembled valve is shown in Plate 8-7. Before assembly, check the travel of valve 8, which must be within the limits of 0.6-2.5 mm. Deviation of this valve above that indicated is not allowable. If it takes place, the reason should be found and eliminated. Assembly order is as tollows.

Install seat 4 in assembly with valves 5 and 20 and scaling rings 18 in body 19. Insert spring 3 and screw plug 2 into body 19 until it stops. Screw fittings 5 and 7 into the body, and screw one fitting into plug 2. Insert rod 17 into body 19, install packing ring 15, and, guiding the top end of rod 17 into body 8, connect the valve body and the electromagnet body, and then fasten them with bolts 16. After this, check dimension A (the amount of projection of rod 17 above the seat of valve 8). This dimension must be within the limits of 3.3-3.7 mm. If the dimension is larger than that indicated, the electromagnet cannot open the valve, since it does not have the strangth to overcome the resistance of air acting on valve 20, and overcome the resistance of spring 3. If the dimension is smaller, valve 6 will not close, and air will escape into the atmosphere, the chamber will empty, and the front axle will not be engaged.

Having checked dimension A, it is necessary to insert support ring 14 and core 12 into body 8. Instail sealing ring 15 into cover 11, and then install it in assembly with coil 13 on the electromagnet body 8, and fastin it with bolts 9.

Installation of the transfer case and electro-pneumatic valve in the motor vehicle. Set the transfer case in the receptacle on the hydraulic jack and roll it beneath the automobile. Pumping the jack handle, raise the case to the necessary height. Insert colts 12 with their welded-or plates into the holes in the longitudinal rails 10 (see Plate 8-8, b) so that the bolts move through the holes in the transfer case housing feet.

forew nuts 2 onto all the boits and tighten them with a wrench until they are final scated. After this, all the nuts are pinned

Install the electro-pneumatic valve in assembly with the electromagnet on the cross member bracket, insert the fastening bolrs, mount the spring washers on them, and screw on the nuts until they are scated. Connect pipe 14 (see Piste 8-6) supplying air from the brake valve to fitting 1 (see Piste 8-7). Install hole 5, connecting it to fitting 5 (see Piste 8-7) of the valve, and connect its other end to the front axis drive engaging chamber. Connect the hose from the vent pipe 3 (see Plate 8-6) to valve fitting? Connect the electric wires to poles K (see Plate 8-6) to the electromagnet and to poles K and 57 (see Plate 8-3) of the front axis drive switch and the control lamp.

Adjusting the transfer case control linkage. Fasten the rear ends of the rods to the transfer case speed changing rods with pins. Check to see if the gears can be engaged with lever 1 (see Plate 8-6). If the lever rests against the front or rear adge of the slot in the floor, the linkage rods should be disconnected from the changing rods, stop nuts 8 unscrewed, and, turning threaded fork 6 in one direction or the other, the necessary linkage rod length attained.

After this, tighten the forks with the stop nuts, connect the linkage rods with the changing rods, and put cotter keys in the pins.

The proper installation of the transfer case control linkage rods, and also the proper assembly and operation of the electromagnetic valve and switches controlling the front axle drive should be checked during a brief run of the motor vehicle by means of engaging the speeds. Switch 48 (see Plate 8-3), which closes the electrical circuit of the electromagnet's valve solenoid (see Plate 8-7), must switch in simultaneously with the engagement of low range in the transfer case. During this, the electromagnet aust push core 12 out of the coil. The core, through rod 17, opens valve 20 and closes valve 6. At this moment, air moves into drive engaging chamber 10 (see Plate 8-3), which switches in and engages the front axle. During this, switch 43 cuts in simultaneously, closes an electrical circuit, and the control lamp indicating that the front axle is engaged lights up on the instrument panel. When the low range is disengaged, the electromagnet circuit is broken.

Valve 20 is closed and valve 6 is opened by air pressure and the force of spring 3 (see Plate 8-7). Air moves from the front axle drive engaging chamber through the open valve 6 and fitting 7 into the atmosphere. Return spring 51 (see Plate 8-3) disengages the axle drive, and the control lamp on the instrument panel goes out.

Besides this, the compulsory engagement of the front axle drive should be checked. There is a switch on the extreme right hand side of the instrument panel. The left position of the switch handle corresponds to an engaged position of the front axle. In this case, the valve solenoid circuit is closed and the lamp on the instrument panel will light up. The right position of the switch handle corresponds to a disengaged position of the front axle. In this position, the sol noid circuit is broken and the lamp goes out.

Dimensions of parts

Transfer case parts dimensions are given in Tables 8-2 and 8-3.

Table 8-2. Dimensions of transfer case parts for the ZIL-157K motor vehicle, ma

Disensions	Nowinal	Allowable without	repair

The housing and its cover

50h 18-36 cast from (GOST 1412-54)

Dismeter of hole for input shaft bearing and middle		100 050
arle power shaft Disaster of holes for high and low range changing	99.974-100.009	100 050
fark rod: front hole rear hole	22.04-22.08 19.04-19.08	22.12 19 12

Diameter of hole for fitting driven axle bearing carrier	116.000-116.135	116.050
Diameter of holes for intermediate shaft bearing and middle axle power shaft		
bearing	89.974-90.00S	90.050

Inpu. shaft

12 Kh 2N4A steel (GOST 4543-61); hardened layer depth, 0.9-1.3 mm; surface layer hardness HRC 56-62.

Diameter of journal for front roller bearing		
and bushing	45.003-45.020	44.98
Diameter of journal for		
rear roller bearing	40.018-40.035	40.000
Tooth thickness on splined		
portion of whaft for		
engaging go	8.935-8.975	8.52
Diameter of shaft threaded		
end for flange fastening		
nut	M27 X 1.5 class 2	• •

Input shaft drive gear

Number of teeth: external, 26; internal, 16; 10KhGT steel (COST 4543-61); hardened layer depth, 0.6-6.9 mm; hardness on teeth HRC 56-62.

Length of exterior teeth	48	4 •
Thickness of extensor teath		
(measured at a height of		
4.32 🗪	6.523-6.573	6.35
Length of internal teeth	7.75-8.25	7.2
Groove width of internal		
tooth along are of		
separating circumference	8.582	* *
Disaster of driving gest		
hole for bushing	56,065-56,125	\$6.150
Gear hub	49.900-49.968	49.900

input shaft less and high range engaging goar

Number of teeth--16, 12Kh2M4A steel (GOST 4543-61), bardened layer depth--0 9-1.3 mm; hardness on teeth--MRC 55-52.

Tooth length	34.0	32.0
Tooth thickness (measured at a height of 5.2 mm)	8.418-8.458	8.20
Groove thickness of gear splined portion	9.015-9.085	9.15
Dismoter of gear journal for bushing Width of slot for fork	61.805-61.905 10.00-10.2	61.70 10.5

laput shaft bushing

Type 20 steel (GOST 1050-60); hardened layer depth--0.7-1.1 mm; hardness-> MRC 56-62.

Internal	diametar	45.000-45.027	45.050
External	diameter	52.940-52.970	52.900

Input shaft drive gear bushing

Als54-4-2.5 browles; band thickness, 1.79:1.90 mm (TsMTU 512-41).

Internal diamoter	53.012-53.042	53,020
External diameter	56.25-56.35	

Support washer of front soller bearing inner race

Type 65 steel (GOST 1050-60), hardness HRC 52-58.

Inickness 4.84-5.0

Thomas whose Stand

Input shaft flange

Type 45 steel (GOST 1050-60); case hardened layer depth--1.0-3.0 mm; hardness of case hardened surface for seal--HRC 52-62.

Diameter of Journal	[or	
Suel	61.94-62.00	61,70
Groove width	5,82	5.9
Dismotor of holes for	r	
flange fastening		
belts	14.24-14.36	15.0

Driven shaft

number of gear teeth- ?? FOKhGT steel (GOST 4543-61); hardoned layer depth--

Star eter of shaft coursel 45.009-45 077 44.98

Diameter of shaft journal for rear bearing Diameter of driven shaft	39.975-39.990	39.950
gear recess for input shaft rear bearing	89.950-89.975	90.00
Tooth thickness of shaft splined portion Diameter of shaft and	5.925-5.975	5,8
threads for flange fastening nut	M27 X 1.5 class 2	
Gear tooth length Gear tooth thickness	40	
(measured at a height of 4.32 mm)	5.\$23-6.\$73	6.32

Driven shaft flange

Type 45 steel (COST 1050-60); case hardened layer depth--1.0-2.5 mm; hardness of case hardened surface for seal--HRC 56-62.

Dismeter of flange journal		
for soal	54,88-55,00	54.70
Groove width of flange		
splined portion	6.00-6.05	6.20
Diameter of hole for		
flango fastoning bolts	14.24-14.36	15.0

Driven shaft bearing carrier

SCh 18-36 cast iron (GOST 1412-54).

Dismoter of carrier recess for front bearing	99.955-99.990	100.01
Diamoter of carrier recess	•	
for rear bearing Diameter of bearing carrier	89.955-89.990	90.01
journal for transfer case		
housing cover	116.013-116.048	~ ~

Intermediate shaft

40KhNMA steel (GOST 4545-61); hardness--HB 341-415.

Diameter of shaft journal for speedometer drive		
worm goar	33.975-34.00	** =

Liamuter of shaft journals

for front and rear bearings

40.009-40.027

39,990

Tooth thickness of shaft

splined portion

12.88-12.97

12.7

Constant engagement goar

Number of gear teeth--29; 30KhGT steel (GOST 4543-61); hazdened layer depth--0.6-0.9 mm; tGoth surface hardness--HRC 56-62.

Gear tooth length

48.0

_ _

Gear tooth thickness

(measured at height of 4.31 mm)

6,523-6,573

6.32

Groove width on gear splined portion

13.0-13.05

13.10

Middle and rear axle drive gear

Number of teeth--27; 30KhGT steel (GOST 4543-61); hardened layer depth--0.6-0.9 mm; tooth surface hardness--HRC 56-62.

Gear tooth length

40.0

. -

Gear tooth thickness (measured at height of

(measured at he 4.32 nm)

6.523-6.573

6.32

Groove width on gear splined portion

13.0-13.05

13.10

Low range gear

Number of teeth--35; 12Kh2N4A steel (GOST 4543-61); hardened layer depth--0.9-1.3 mm; toot! surface hardness--HRC 56-62.

Tooth length

26.5

Tooth thickness (measured at a height of 2.54 mm)

6.975-7.025

6.80

Cover for intermediate shaft and middle axle power shaft bearings

SCh 15-32 cast iron (GOST 1412-54).

Diameter of cover centering

collar for hole in transfer

Diameter of holes for cover

fastening bolts

case housing

10.7

89.93-90.00

11.2

Middle axle power shaft

40KhNMA stoel (GOST 4543-61); hardness--HB 341-415.

Diameter of shaft journal		
for front bearing	45.018-45.035	45.00
Diameter of shaft journal		
for rear bearing	40.009-40.027	39.990
Tooth thickness on shaft		
splined portion:	_	
for engaging sloeve	5.75-5.78	5.6
for flange	5.925-5.975	5.80

Middle axle power shaft gear

Number of teeth--28; 30KhCT steel (GOST 4543-61); hardened layer depth--0.6-0.9 mm; tooth surface hardness--HRC 56-62.

Gear tooth length Gear tooth width (measured	40.0	
at a height of 4.32 mm) Groove width on gear	6.523-6.573	6.32
splined portion	13.00-13.05	13.10

Flange of the middle and front axle power shaft

Type 45 stee! (GOST 1050-60); 1 yer depth of surface case hardening for seal-1-3 mm: case hardened layer burdness--HRC 52-62.

Pismeter of flange receptacle for flange		
fork	95.000-95.054	95.1
Diameter of flange		
journal for seal	54.88-55.00	54.70
Width of groove on		
flange splined portion	6.03-6.05	6.20
Diameter of hole for		
flange fastening bolts	14.24-14.36	15.0

Front axle power snart carrier

SCh 18-36 cast iron (GOST 1412-54).

Diameter of carrier recess for bearing	89 .974-90 .009	90.040
Diameter of centoring projection for installa-		
tion in transfer case housing hole	99.965-100.000	

Diameter	of	hole	for
engagi	ng	fork	rod

14.03-14.06

14.1

21.950

Front axle power shaft

40KhNMA steel (GOST 4543-61); hardness--HB 341-415.

Diameter of shaft journal for bearing	40.009-40.027	39.99
Tooth thickness on shart		
splined portion for flange	5.925-5.975	5.8
Tooth thickness for engaging		
sleeve	5.75-5.78	5.6
Diameter of shaft and threads	·	
for flange fastening r	M24 X 1.5 class 2	

Front axle power shaft engaging sleeve

Number of teeth--12; 40KhNMA steel (GOST 4543--1); hardness--HB 341-415.

Width of tooth grooves along separating circum-		
ference arc	5.86	
Width of sleeve groove for		
fork	10.00-10.20	10.4
Dimmator of sleeve groove		
curnal for fork	50.88-60.00	59.70

High and low range engaging fork rod

Typo 45 steel (GOST 1050-60); case hardened layer depth--1.0-3.0 mm; hardness of case hardened surface--HRC 52-62.

Diameter of fork rod for hole in transfer case	
housing	21.979-22.000
Radius of notch for catch	
lock	5.65-5.75

High and low range engaging fork

Type 20 steel (GOST 1050-60); hardened layer depth--0.3-0.5 mm; hardness of hardened layer--HRC 52-62.

Fork finger thickness	9.7~1.8	9.5
Diameter of fork bushing		
throads	M22 1.5, class 2	

Front axle engaging fork rod

18KhGT stool (GOST 4543-61); hardened layer thickness--0.7-0.1 mm; hardness of hardened surface--HRC 56-62.

Diameter of rod for hole in fork

13.965-14.000

13.940

Front axle engaging fork

Type 20 steel (GOST 1050-60); depth of nitrided layer--0.3-0.5 mm; hardness of hardened surface--HRC 56-62.

Diameter of hole for

engaging fork rod

14.006-14.025

14,045

Thickness of fork fingers

9.7-9.8

9,5

Plate 8-3. Dimensions of transfer case parts of the ZIL-131 motor vehicle, mm

Dimensions

Nominal

Allowable without repair

The housing and its cover (Plate 8-40)

SCh 15-32 east iron (GOST 1412-54)

Diameter of hole for input shaft bearing 119.988-120.023 120.060 Diameter of hole for driven shaft front bearing and front axle power shaft rear bearing 109.988-110.023 110.060 Diameter of hole for front axle power shaft front bearing and driven shaft roar bearing 99.988-100.023 100.060 Diameter of hores for speed changing fork rods and rear hole for front axle power engaging fork red 19.04-19.08 19.13

Input shaft

40Kh steel (GOST 4543-61); hardness--HRC 35-40.

Diameter of journal for		
front ball bearing	45.003-45.020	44.98
Diameter of journal for		
rear roller bearing	35.003-35.020	34,98
Diameter of shaft journal		
for drive gear	50.030-50.047	 •
Tooth thickness for		
ongaging carrier along	•	
separated circumference		
with diameter of 56 mm	5.637-5.752	5.5
Tooth thickness of shaft		
splined portion for	F 04 F 00	
flange	5.94-5.99	5.8
Diameter of shaft threaded		
ond for flange fastening	M77 V 1 E -1 7	
nut	M33 X 1.5, class 2	• •

Input shaft driving goar

Tooth length Tooth thickness measured	39	
at a height of 5.19 mm	7.151-7.191	6,95
Diameter of hole for input shaft journal	59.000-50.027	

High Range Engaging Carrier

Number of teeth--27; 25KhGT steel (ChMTU TsNIIChM 761-62); depth of nitrided layer--0.6-0.8 mm; on the surface of the fork groove --0.4mm; surface layer hardness--HRC 60-65; core hardness--HRC 35-45

Tooth length	13.2	12
Tooth thickness along		
arc of separated circum-		
forence at a distance of		
3.5 mm from the face	5.722-5.637	5.5
Width of tooth grooves along		
arc of separated circum-		
ference for input shaft	5.787-5.872	6.000

Width of groove for fork	10.00-10.20	10.40
Diameter of groove journal		
for fork	71.88-71.96	71.7

Input shaft and front axle power shaft flange

Type 45 steel (COST 1050-60); case hardoning by means of heating with high frequency current, with a case hardened layer depth of 1.0-2.5 mm; case hardened layer hardness--HRC 56-62.

Diameter of journal for Jeal	57.88-58.00	57.7
Width of groove in flange splined portion Diameter of centering hole	6.00-6.05	6.20
for Cardan shaft flange fork Diameter of holes for	95,000-95,054	95.1
Cardan flange fork fastening bolts	14.24-14.36	15.00

Driven shaft

Number of gear teeth--38; number of internal teeth for carrier--26; 25KhGT (ChMTU Ts NIIChM 761-62); depth of nitrided layer--0.6-0.8 mm; surface layer thickness HRC 60-65; core hardness HPC 35-45.

Diameter of journal for		
front roller bearing	50.003-50,020	49.98
Diameter of journal for		
rear ball bearing	45.003-45.026	44.98
Diameter of hole in driven		
chaft coar for input		
shaft rear boaring	80.000-80.030	80.050
Tooth length	42	40 74
Guar tooth thickness		
(measured at height of		
5.431 mm)	7.412-7.452	7.2
Tooth length	8	7
Groove width along arc		
in divided circumference		
at distance of 3.5 mm		
from face	5,842-5.927	6.1
Tooth thickness on shaft		
splined portion for		
flange	6.94-6.99	6.8

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Diameter of shaft and threads for flange fastoning nut

M33 X 1.5, class 2

Speedometer worm gear

Number of turns-5; type 20 steel (GOST 1050-60); depth of cyanated layer-0.15-0.30 mm; hardness -HRC 56-62.

Tooth thickness (measured a	Tooth	:hickn o ss (m	easured :	at
-----------------------------	-------	-----------------------	-----------	----

height of 1.25 mm) 1.76-1.81 1.6

Diameter of hole in worm gear

for driven shaft journal

45.032-45.100

peedometer drive driven gear

Number of teeth--17; type 20 steel (GOST 1050-60); depth of cyanated layer--0.15-0.30 mm; hardness--HRC 56-62.

Tooth thickness (measured	at
height of 1.295 mm)	
Diameter of ingreal for	

1.76-1.81

1.6

coliar

10.940-10.974

10.90

Diameter of rear support journal

7,915-7,965

7.87

Driven shaft flange

Type 45 steel (GOST 1050-60); case hardened by heating with high frequency current with a case hardened layer depth of 1.5-3 mm; hardness of case hardened layer, HRC 56-62.

Diameter of journal for	Diameter	of	journal	for
-------------------------	----------	----	---------	-----

soal	61.88-62.00	61.7
Width of groove in flange		
splined portion	7.00-7.05	7.20
Diameter of centering		
collar for Cardan shaft		
flange fork	94.93-95.00	94.9
Diameter of holes for		
Cardan shaft flange fork		
fastening bolts	16.20-16.235	~ ~

Front axle power shaft

Number of teeth for engaging carrier--24; 25KhGT stee! (ChMTU TsNIIChM 761-62); nitrided layer dopth-1-1.3 mm; on the journals and support faces for the needle bearings--0.8 mm; surface layer hardness--HRC 60-65, and core hardness--HRC 35-45,

Diameter of journal for		
front ball bearing	45.005-45.020	44.98
Diameter of journal for		
rear roller bearing	50.003-50.020	49.98
Diameter of journal for		
gear roller bearings	51.58-51.60	\$1.55
Tooth length	8	
Tooth thickness along		
arc of divided circum-		
ference	3.904-3.980	3.7
Tooth thickness of the		
shaft splined portion		
for shaft	5.94-5.99	5.8
Diameter of shaft and		
throads for flange		
fastoning nut	M33 X 1.5, class 2	= -

High range gear

Number of teeth--38; number of teeth for engaging carrier--24; 25KhGT steel (ChMTU TsNIIChM 761-6.); nitrided layer depth--0.6-0.8 mm, in the supporting holes of the hub and on the faces--no less than 0.4 mm; surface layer hardness--HRC 60-65; core hardness--HRC 35-45.

Tooth length	42	•• ••
Gear tooth thickness		
(measured at height of		
5.43 mm)	7.412-7.452	7.2
Diameter of hole for		
needle bearings	57.6J 57.648	\$7.67
Tooth length		
for low range engaging		
carrior:	13	12
for front axle power		
shaft engaging carrier	11	10
Tooth thickness along are		
of divided circumference:		
full	3.904-3.989	3.7
t : ored	3.3-3.6	3.1

Front axle drive engaging carrier

Number of carrier teeth -- 24; z5KhGT steel (ChMFU TeNIIChM 761-62); gitrided layer depth -- 0.6-0.8 mm, and on surface of groove for fork -- 0.4 mm; surface layer hardness -- HRC 60-65, and core hardness -- HRC 35-45.

Tooth length	24	** **
Groove width along are of		
divided circusforence	4.054~4.139	4.30

Width of Slot for fork Diameter of slot journal	10.00-10.20	16.40
for fork	96.86-96.95	96.7

Low range gear

Number of teeth--52; number of teeth for engaging carrier--24; 25KhGT steel (ChMTU TsNIIChM 761-62); depth of nitrided layer--0.6-0.8 mm, in the supporting hole of the hub and on the faces--no less than 0.4 mm; surface layer hardness--HRC 60-65; core hardness--HRC 35-45.

Tooth Jongth	39	₩ #
Gear tooth thickness		
(measured at height of		
3.432 Pm)	5.916-5.956	5.7
Diameter of hole in hub for		
ncedle bearings	57.630-57.648	57.67
Tooth length	14.5	
Tooth thickness along arc		
of divided circumference:		
ful1	3.904-3.989	3.7
tapered	3.3-3.6	3.1

Low range engaging carrier

Number of currier teeth--24; 25khGT steel (ChMTU TsNIIChM 761-62); depth of nitrided layer, 7.6-0.8 mm, on the surface of the groove for the fork--0.4 mm; surface layer hard.cas--HRC 60-56, and core hardness--HRC 35-45.

Tooth length	34	
Groove width along arc		
of divided circumference	4.054-4.139	4.30
Width of slot for fork	10.00-10.20	10.40
Diameter of slot journal		
for for	96.86-96.95	96.7
Diameter of holes for		
catch lock balls and		
blocking mechanism	11.24-11.36	11.5

Low and high range ngaging rods

Rod diameter	18,979-19,000	18.95
Radius of notches for		
catch lock	5.65-5.75	Clearance no greater
		than 0.5 mm from template

Radius of notch for block

7.0-7.3

Dismoter of hole in rod for linkage rod

for linkage rod fastering pin

12.12-12.24

12.4

Low and high range engaging forks

Type 20 steel (GOST 1050-60); depth of cyanated layer -0.3-0.5 mm; hardness of case hardened layer -- HRC 56-62.

Diameter of hele for speed

engaging rod

19.02-19.05

9.1

Thickness of fork fingers

9.7-9.8

9.4

Speed engaging rod catch lock body

SCh 15-32 cast iron (GOST 1412-54).

Diameter of holes for

speed engaging rods

19.14-19.28

19.5

Front axle power engaging chamber body

ALIOV aluminum alloy (GOST 2685-53).

Diameter of hole for

front axle power

engaging chamber rod

29.000-29.033

29.080

Diameter of centering

collar for installa-

tion in housing

39.95-40.00

Diameter of threads in

flange holes

M6 class 2

Front axle drive engaging chamber rod

Type 45 steel (GOST 1059-60); case hardened by means of heating with high frequency current, with a case hardened layer depth of 1.3 mm; hardness of case hardened layer--HRC 52-62.

Diameter of rod for

engaging chamber body

28.93-28.96

28,90

Diameter of rod for

transfer case housing

COV#1

18 979-19.000

18.95

Return spring for front axle power engaging chamber

Number of cox1s--8; steel spring wire 4 mm in diameter (GOST 5047-49).

Exterior spring diameter Spring length in free	33.6-34.4	
condition	60	*
Spring length (under load of 18-23 kg)	48	

Pressure spring of front axle power engaging chamber

Number of coils--24; steel spring wire 2.5 mm in diameter (GOST 5047-49).

Internal spring dismeter Spring length in free	8.25-9.75	••
condition	100	q •
Syring length under load of 24-30 kg	80	••

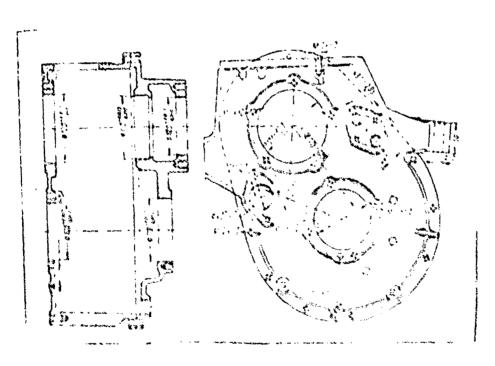


Plate 8-40. Transfer case in assembly with its cover

Chapter 9. Universal Drive [Cardan Drive]

Layout

All ZIL cargo motor vehicles are equipped with open universal drives made of thin-walled welded tubing with universal joint forks welded onto both their ends (or with the fork welded onto one end and a splined end or splined hushing welded onto the other end). All the universal joints run on needle bearings.

Universal drive of the III-130 motor vehicle. Propeller shafts (Plate 9-1) are manufactured of drawn tubing welded out of cold-rolled plate 3 mm in thickness. The external diameter of the tubing is 77 mm. The fork is welded to both ends of the main propeller shaft 12 and to the front end of the intermediate shaft 2. To the rear end of the intermediate shaft is welded a splined bushing 26, on whose exterior diameter is installed ball begring 5 of the intermediate support.

The universal drive of the motor vehicles is equipped with scaled splined connections. Eudrication of the inner space of bushing 26 is maintained by leakage from buffle 27 which is rolled into the splined bushing, and from the opposite side, by the subber and felt scale. Both scale, in combination with the splined protective boot 10, prevent the splined connections from becoming dirty. The protective boot is fastened onto the shaft with spring rings.

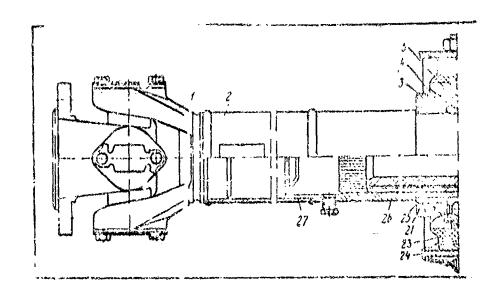
The construction of all universal joints is identical. The universal joints have rubber seals to hold imbication and prevent the needle bearings from becoming dirty. The crosses and bearings of all three universal joints are interchangeable.

Universal joint bearings are lubricated through lubrication fitting 11, which is acrewed into the cross. To avoid damaging the bearing seals during increased pressure in the process of lubrication, there is a protector valve 14 in the center of the cross which opens under a pressure of 3.5 kg/cm².

The intermediate support of the propeller shaft consists of ball bearing \$, on which covers 4 with seals 3 and 7, holding lubrication and protesting the bearings from dirt, are installed and rolled in. The bearing, together with the covers, is installed in the rubber cushion 23 of the support. The brankets of the rear bearing cover go into slows in the support cushion and prevent the bearing from rotating in the cushion.

The intermediate support is fastened to the motor vehicle frame by bolts with support bracket 22 and the cross member. To limit axial travel of the cushion in the support bracket, a cushion stop bracket is installed between the bracket and the frame cross member. Besides this, the lower part of the cushion is festened to the bracket with a tession clump for the same purpose.

The support bearing is lubricated through an angular lubrication ditting which is sersued into the bearing cover.



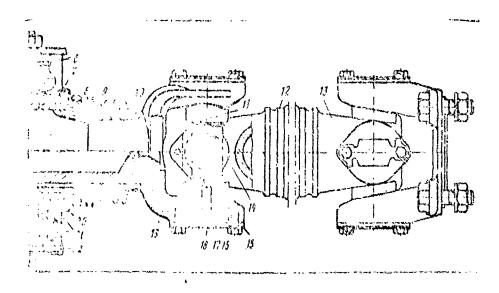


Plate 9-1. Universal drive or the ZIL-130 motor vehicle:

11 from universal joint 2) intermediate shaft 3) and 7) felt seals
4) support cover 5) bearing 6; intermediate support cushion stop
bracket 8) seal nut 9) felt seal 10; protective seet 11; subrication
(atting 12) main propelly shaft 13; rear universal joint 14; protective value 15; locking plate 15; needle bearing 17; cross 18; support
plate 19; intermediate universal joint sliding fork 20 and 25; seal
deflectors 21; hearing spacing bushing 22; bracket 23; cushion
24; locking class 26; bushing 27; baffle

Plate 9-2. Universal drive of the ZIL-157K motor vehicle:
1) transmission 2) universal joints 3) main propeller shaft
4) transfer case 5) handbrake 6) intermediate roar .xle propeller shaft 7) intermediate support 8) rear axle propeller shaft 9, 10, and 13) drive axles 11) middle axle propeller shaft 12) front axle propeller shaft

The universal drive of the ZIL-157K motor vehicle is shown in Plate 9-2.

All universal shafts except the main one (located between the transmission and the transfer case) are constructed identically and differ by their length and the dimensions of their forks and flanges. All universal joints are identical and interchangeable. Since September of 1965, the bearings of the crosses have been inscalled with robber-bodied seals.

Each propeller shaft (Plate 9-3) consists of a thin-walled tube, on one end of which is wolded the stationary yoke, and on the other, a splined end connecting with the sliding yoke.

The main propelly r shaft differs from the other shafts by the absence of its protecting sleeve and the dimensions of its splines. The two forks, having a splined end and a splined bushing, are directly connected together, and are connected to the flange fork through the cross and bearings.

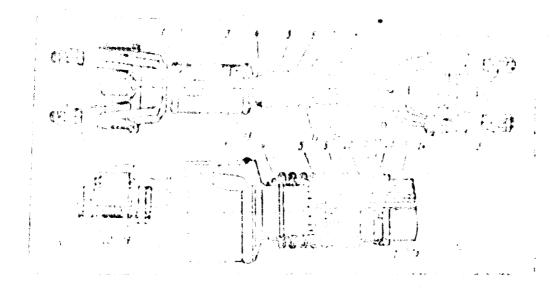
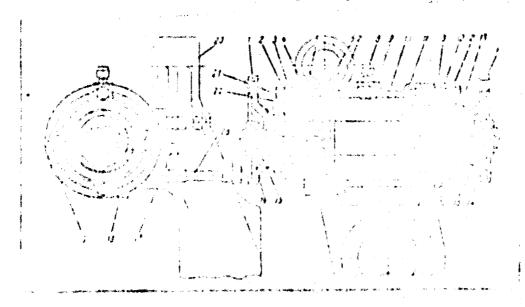


Plate 9-3. Propeller shaft of the rear axle of the ZIL-157K motor vehicle:

1 and 5) lubrication fittings 2) yoke 3) propeller shaft
4 and 17) safety wire 5) protective boot 6) splined end
7) sliding fork seal 8) sliding fork 9) baffle 10) needle
bearing 11) universal cross 12) flange yoke 13) protector
valve 14) seal 16) seal clamp tab 18) belancing plate
19) support plate 20) locking plate 21) removable balancing
plates 22) seal end 23) seal ring clamp



Place 9-4. Universal drive intermediate support of the ZIL-157K motor vehicle:

1) flange 2) seal 3) hearing cover 4) sealing gasket 5 and 12) oildeflecting washers 6) support washer 7) tapezed roller hearing 8) vent 9) filler hole plug 10) intermediaty support shaft 11) housing 13) deflector 14) nut 15) washer 16) adjusting gaskets 17) pin 18) drain hole plug 19) control hole plug 20) upper reaction lever 21 and 23) holts 22) seal protector ring

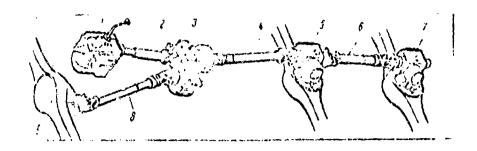


Plate 9-5. Universal drive of the ZIL-131 motor vehicle:
1) transmission 2) main propeller shaft 3) transfer case
4) middle axle propeller shaft 5) middle axle 6) rear axle
propeller shaft 7) rear axle 8) front axle propeller shaft
9) front axle

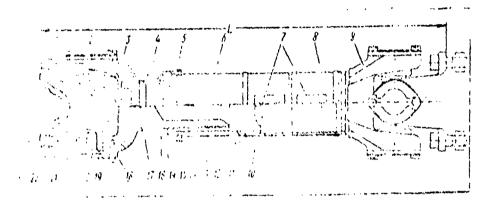


Plate 9-6. Middle axle propoller shaft of 21L-131 motor vohicle:
1) flange yoke 2) cross 3) splined yoke 4) protective boot
5 and 17) safety wire 6) splined bushing 7) balancing plate
8) propellor shaft 9) yoke 10) baffle 11) plug 12) slotted
ring 13) rubber seal 14) slotted washer 15) felt seal 16) nut
18) support plate 19) lock plate 20) needle bearing 21) valve
22) bolt L) propellor shaft length

The support of the rear axie intermediate propeller shaft (Plate 9-4) is fastened to the upper reaction lever 20, which is wolded to the jacket of the middle axie half shaft. Shaft 10 of the intermediate support is installed in housing 11 on two tapered relief bearings 7.

The universal drive of the ZIL-131 motor vehicle consists of four propeller shafts with eight universal joints. Construction of the propeller shafts (Plate 9-5) is identical except for the middle axle propeller shaft. Universal joints of shafts 2, 6, and 8 have identical dimensions and are interchangeable.

The middle axle propeller shaft 4 carries a double load, in that it transmits the torque moment to the middle and rear axles, and therefore it has increased dimensions of its bearing cross, splined connection, and its own exterior diameter. The middle axle propeller shaft is manufactured of drawn tubing which is welded out of cold rolled plate 3.5 mm thick. The external diameter of the shaft is 89 mm. An end yoke 9 is welded to one end of the middle axle propeller shaft 8, and a splined bushing 6 is welded to its other end.

Scaled splined connections are used in the propell r shafts of the ZIL-131 meter vehicle. Lubrication in the inner space of the splined bushing 6 is held from one end by baffle 10, which is rolled into the face of the splined bushing, and on the other end by rubber seal 13. Felt seal 15 and external protective boot 4 prevent dirt from getting on the cylindrical part of slide yoke 3 which projects from the bushing. This significantly improves the longevity of the rubber seal and of the splined connection. The protective sleeve is fastened to the shaft by safety wire 5 and 17. Each universal joint consists of flange fork 1 and splined fork 3, or of flange fork 1 and end fork 9, connected together by cross 2, on whose journals are mounted needle bearings 20. To held the lubrication and pretect the bearings from becoming dirtied, they have rubber seals.

The universal joint bearings are lubricated through a lubrication fitting which is screwed into the cross. So as not to damage the bearing seals during increased pressure while lubricating, the cross has a protector valve 21, which opens at a pressure of 3.5 kg/cm².

Tochnical service

During DS, wash and inspect the universal drive from the outside.

During TS-1, it is necessary to check the fastening of the cross bearing support plates and fastening of the propeller shaft flanges. All flange fastening bolts must be tightened until they are firmly seated. If the flange fastening becomes excessively loose, it is necessary to check the balance of the propeller shafts.

If the bolts fastening the bearing support plates on the crosses become loosened, they should be tightened and locked by bending one ear of the locking plate up against a flat of each bolt head.

If significant radial or longitudinal clearance is present in the cross bearings, the universal joints should be disassembled and, if necessary, the bearings or crosses in assembly with the bearings should be replaced.

On motor vehicles having an intermediate support, besides this, the fastening of the intermediate support bracket to the frame cross member (on the ZIL-130 motor vehicle), or to the middle drive axle (on the ZIL-157K motor vehicle), should be checked. On the universal drive intermediate support of the ZIL-157K motor vehicle, during TS-1, it is necessary to blow out the air passages of the vent; whose clogging might cause increased pressure in the bearing housing and serve as reason for oil leakage through the seals.

Before lubricating the Cardan drive units, dust and dirt should be cleaned off the point of lubrication.

It is necessary to pack the bearing of the propeller shaft intermediate support on the ZIL-130 motor vehicle through the prossure lubrication fitting until grease is pressed out of the control hole.

It is necessary to pour transmission oil into the housing of the propeller shaft intermediate support of the ZII-157K motor vehicle up to the bottom edge of the control hole opened by plug 19 (see Plate 9-4). Universal joint needle bearings are lubricated with transmission oil. Needle bearings 10 (see Plate 9-3) are lubricated through lubrication fitting 1 in cross 11, until oil appears out of protector valve 13. Lubrication of the needle bearings with consistent greases is not allowed.

It is necessary to lubricate the splined propellor shaft connections on the ZIL-157K motor vehicle through the pressure lubrication fitting, pressing the lubricant until it is forced out.

Before lubricating the propeller shaft sliding forks on the ZIL-130 and ZIL-131 motor vehicles and their modifications, it is necessary to disassemble it, unscrew the plug, remove the splined yoke, remove the old grease, wash out the splined sliding yoke and internal space of the splined bushing, and pack this space with fresh lubricant.

Disassambly and assembly

ZIL-130 motor vehicle

For removal of the universal drive from the motor vehicle, it is necessary to unscrew the nuts fastening the shaft rear yoke flange to the rear axle main drive input shaft flange, remove the washers, drive the bolts out of their flange helps, and, supporting the propeller shaft, move it slightly forward and release its rear end onto the floor on a support. Unscrew the bolts fastening the intermediate support to the frame, unscrew the nuts from the front yoke

flange fastening bolts, remove the universal drive from the motor chicle, and take it to the point of disassembly.

Disassembly of the universal drive. Before disassembling the universal drive, it is necessary to clean the dirt from it and wash it in the degreesing solution. To maintain the balance, it is necessary to mark the relative position of the splined end and bushing, and the relative position of the yokes, flanges, cross arms, and bearings with a punch or paint. For Alsessembly, it is necessary to install the universal drive on the bench.

Remove the locking clamp 24 (see Plate 9-1), the stop clamp 6, and intermediate support bracket 22. Remove the safety wire fastening protective boot 10.

Remove the rubber cushion 23 and rear deflector 29 fixes the intermediate propeller shaft splined bushing, and then press off bearing 5 of the support in assembly with its covers with a 20P-7968 puller (Plate 9-8).

For pressing off the bearing, split ring 2 should be mounted on the support cover 4 and fastened with tension screw 8, mandred 6 is inserted into the splined bushing, lover 5 of the puller is installed on the ring, end, turning screw 7, the bearing is pressed off the shaft together with its evers, support seals, and rear spacing bushing 21 (see Plate 9-1). The front spicing bushing 21 and deflector 25 are removed from the shaft.

The universal joints are disassembled with a divice (Plate 9-9) which prevents deformation of the yoke and breakage of the bearings and eases disassembly.

Before disassembling the universal joints, the ears of the locking plates should be bent out, bolts fastening these plates should be unscrewed, and the locking and support plates should be removed.

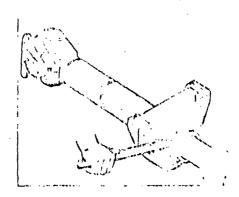


Plate 9-7. Unscrewing the nut fastening the support bearing

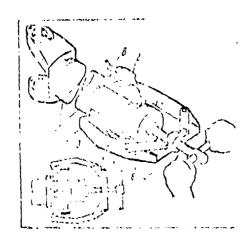
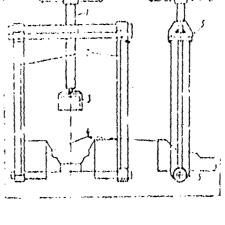


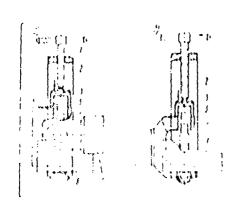
Plate 9-8. Removing the intermediate support bearing:

1) incormodiate propoller shaft 2) split ring 3) bearing 4) support rear cover 5) puller lever 6) support mandrol 7) puller screw 8) ring tension screw



Device for universal joint Plate 9-9. disassembly:

- 1) working screw 2) extension stand
- 3) cup 4) support surface 5) catch lock



Place 9-10. Method of disassembling the universal joint with device: a) pressing the bearings out of the flange yoke t) pressing the bearings out of the propoller shaft yoke

- 1) working screw 2) extension stands
- 3) cup 4) flange yoke 5) bearing
- 6) cross 7) drive shaft yoke
 - 8) support surface



Plate 9-11. Model 684 stand for checking and correcting propeller shafts:

1) centers 2) supports 3) pnoumatic press 4) base 5) phoumatic press power handle

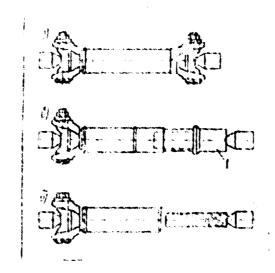


Plate 9-12. Diagram for installing propeller shafts on stand for checking oscillation and correcting:

a) for rear axle propeller shaft of ZIL-130 motor vehicle h) for intermediate propeller shaft of ZIL-130 motor vehicle and all propeller shafts of ZIL-131 motor vehicle c) for propeller shafts of ZIL-131 motor vehicle i) mandrel

The device allows cup 3 to be rested on the face of one of the yokes by turning working screw 1, while the second yoke lies on the support surface 4. With further rotation of screw 1, the support surface draws closer to the cup and the cross bearing moves into the space in the cup. Rotation of the working screw continues until it is in a position in which the bearing easily (by hand) is pushed from the eye hole.

The universal joint is disassembled in two steps. At first, one of the yokes is installed on support surface 8 (Plate 9-10, a) so that is forms the support, and the bearings are pressed out of the yoke which is assembled with it. After both bearings have been pressed out of this voke, the bearings are pressed out of the yoke which was the supporting one. In the second case, the journals of cross 6, from which the bearings have already been removed, serve as a support (Plate 9-10,b). The journals are set in notches formed in the supporting plate 8 and the bearings are pressed out of the second yoke.

If the indicated device is not available, the universal joint may be disassembled with a bronze mandrel and hammer. In this process, it is necessary to set the mandrel on the body of the needle bearing and, lightly hitting it with the hammer, press out the opposite bearing. Turn the shaft and press out

the other bearing, setting the mandrel on the face of the cross journal. Separate the flange yoke from the shaft. The same operations should be conducted for disassembly of the propellor shaft flange yoke crosses.

Control checking. Oscillation of the propeller shaft is checked on a stand (Plate 9-11) by indicators which are installed on a plate. The stand has movable face plates with centers 1 for installation and fastening of the shaft on it. Before installing the shaft on the stand, mandrels (Plate 9-12, a) centered along the faces of the yokes, are inserted in both yokes of the shaft. If oscillation greater than that allowable is present, the shaft should be corrected with press 3 (see Plate 9-11), installing the shaft on support 2. Oscillation, measured along the ends of the shaft, must not exceed 0.4 mm, and that measured along the length of the shaft must not exceed 0.8 mm.

If there is wear in the yoke holes for the needle bearings above the dimensions allowable without repair, the rear axle propeller shaft should be replaced.

Oscillation of the intermediate propell r shaft is checked on a stand (see Plate 9-11) with indicators. Before installing the shaft on the stand, a mandrel (see Plate 9-12, b) centered along the faces of the yoke is inserted in the yoke, and a mandrel centered along the external diameter of the splines on a length of 100 mm is installed in the splined bushing. Both mandrels have conic holes for installing them on the stand centers. If oscillation is present greater than that allowable, the sheft should be corrected using press 3 (see Plate 9-11) with the shaft installed on support 2. Oscillation of the bushing journals for the support bearing must not exceed 0.2 mm.

With wear in the yoke holes for the needle bearings, splined bushing journals for the intermediate support bearing, splined bushing, spacing bushings, or cross journals so that the dimensions allowable without repair are exceeded, it is necessary to replace the parts. Besides this, if the intermediate support bearing covers are dented or damaged, they should also be replaced.

Assembly of the universal drive. Before assembling the parts of the universal drive, wash them and blow them out with compressed air. The needle bearings must be smeared with TAp-15 oil (GOST 8412-57). The lubricating passages in the cross must be cleaned out, and the lubrication fitting and protector valve must be screwed into the threaded holes. Toward the aim of maintaining balance, assembly must take place with consideration for the marks made during disassembly.

Assembly of the universa joints. Press the needle bearing into one of the holes in the yoke, insert one journal of the cross into the yoke hole where there is no bearing, and guide the other end into the bearing. Install the second bearing and, guiding it onto the cross journal, press it in. Install the supporting plates so that the projection on the plate moves into the slot in the bearing face of the cross. Install the locking plates and fasten them with bolts. Torque moment on the bolts must be 1.0-1.5 kg meters. Lock the bolts with the locking plates, bending the ears up against flats on the bolts.

Assomble the remaining universal joints in the same manner.

Balancing propeller shafts. With replacement or repair of any of the propell r shaft parts, dynamic balancing should be done. Dynamic balancing takes place on the ST-1157 or ST-1199 (ZII) machine shown in Plate 9-13.

The propoller shaft if fastened to a balancing machine adapter by its flange yoke. The propeller shaft is installed with one end in the adapter by a contering coller 94.93-95.00 mm in diameter, and with its other end in a special lunette with centering along the smooth cylindrical journal of the Imbalance in the propollor shaft in assembly with the flange sliding yoke. yoke and sliding yoke is not allowed to be greater than 70 gram cm from each end. If imbalance exceeds 70 gram cm, it should be eliminated by welding additional balancing plates onto the shaft. During balancing, the balancing plates are funtened temporarily with wire on the shaft at a distance of 10 mm from the wolded seam. Upon completion of balancing, the plates are wolded to the shaft and the wire is removed. The welding must be accurate, without significantly increasing the weight of the propeller shaft. The number of balancing plates west not exceed four on each end of the shaft. If the balancing plates are fastened to the shaft quickly, it is recommended that they be knocked of the shaft and the shaft be balanced again.

The intermediate propellor shaft is also fastened to the adapter of the balancing machine by its flange fork. The propell r shaft is installed with one of its ends in the adapter with a centering collar which is 94.93-95.00 mm, and with its other end in a special lunette centered along the journal of the splined bushing for its support bearing. A part veighing approximately 10 kg and imitating half the weight of the rear exic propeller shaft is inserted in the splined bushing. This part must be centered according to the external diameter of the splined portion of the bushing. The allowable imbalance on the flange fork end of the shaft is 50 grem cm, and that on the splined bushing end of the shaft is 70 gram cm. The everall imbalance of the drive must not exceed 50 gram cm.

Assembly of the intermediate propoller shaft support and its installation on the shaft. Install the deflector 25 (see Plate 9-1) and the front spacing bushing 21 on the journal of the intermediate propoller shaft. Install the un-disassembled part of the intermediate propoller shaft support (bearing in assembly with its covers and seals) and also the rear spacing bushing 21 on the shaft journal. Press the support onto the shaft (Plate 9-14) with a hammer and mandral. The mandrel must rost against the rear face of the spacing bushing. Mount the rubber cushion 23 (see Plate 9-1) on the support. Install the second deflector 20 on the shaft, inserting its lower stop into the slot in the shaft.

Connecting the sliding yoke of the propollor shaft with the splined bushing of the intermediate propeller shaft. Install the protective book 10, nut 8, felt seal 9 with its split washers, the rubber seal and split washer, on the end of the sliding yoke. Insert the splined end of the sliding yoke 19 into sliding bushing 26 and fasten the intermediate support with nut 8, after which the nut must be locked, bending the stop into the slot in it. Fasten the protective boot 10 with its tension clamp or safety wire.

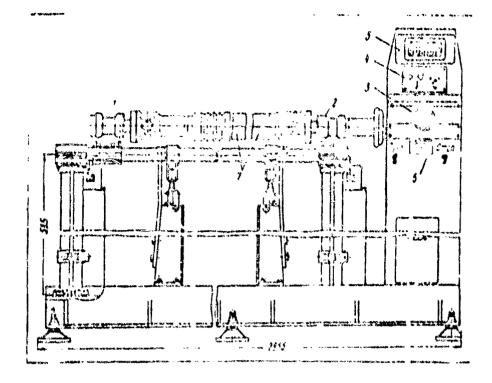


Plate 9-13. Diagram of machine for nameller shaft dynamic balan

1 and 2) adapters 3) graduated chicle of collector 4) electric panel 5) galvanomotor 6) magnetic starter 7) propeller shaft 8) "start" 9) "stop"

During assembly of the propeller shaft of a ZIL-130 motor vehicle, it is necessary to ensure that the flange forks of the transmission and rear axle are positioned in mutually perpendicular planes. During assembly of the universal drive in the ZIL-130V1 and ZIL-MHZ-555 dump truck, the indicated fork flanges must lie in the same plane.

Installation of the universal drive on the motor vehicle. Connect the rear end of the propeller shaft to the flange of the differential input shaft without tightening the bolts. Raise the universal drive and fasten the in resedinte support onto the frame cross member, having mounted the bracket on the support and tightened the bolts. During this process, the support cushion must be perpendicular to the axis of the intermediate propeller shaft.

Tighten the propeller shaft yoke flunge on the differential imput shaft flunge. Connect the intermediate propeller shaft fork flunge to the flunge of the transmission output shaft. Spring washers must be installed beneath the nuts on all bolts. Nut torque moment is 8-9 kg meters.

The ZIL-157K motor vehicle

Removing the universal drive. Each shaft of the universal drive is removed independent of the others. For removal of any shaft, it is necessary to caserew the bolts fastening its flanges and, holding the shaft, remove the bolts from the flange holes and withdraw the shaft from beneath the motor vehicle.

For removal of the intermediate support, it is necessary to unpin the bolts fastening the support, unscrew them with a socket wrench, and remove the support assembly from the middle laive axis.

Before disassembling the propeller shafts and intermediate support removed from the motor vehicle, it is necessary to clean the dirt from them and wash them in a degreesing solution.

Disassembly of the universal drive. Disassembly of the propeller shafts. It is recommended that the splined connections of the motor vehicle's propeller shaft be disassembled in the following order.

Lay the propeller shaft on a metal working bench, mark the relact position of the fork and shaft with a punch, remove safety wire 4 and 17 with combination pliers (see Plate 9-3), move the protective hoot 5 along the shaft axis toward its splined end, bend out tabs 16 of the clamp ring 23, separate the shaft, moving the splined end 6 out of the sliding yoke 8, and then remove the seal in assembly with rings 22 and clamp 23.

The universal joints are disassembled with the device (see Plate 9-9). The method of disassembly is shown in Plate 9-10.

Disassembly of the intermediate support. Fasten the intermediate support in a metal working vise and disassemble it is the following order.

Unscrew the lower plug and drain the oil. Unpin and unscrew nuts 14 (see Flute 9-4) fustening flunges I, and remove washer 15. Remove the flunges from the splined ends of shaft 10 with a 20P-7968 puller.

this crew bolts Il fastening covers 3, remove the protective rings 22 and covers, tapping on the covers with a hammer. Remove scaling gaskets 4 and adjusting gaskets 16, remove oil-deflecting washers 15 and 12, and support washers 6.

If they are not in proper condition, the subber hodied seals should be pressed out of the covers.

Install the support cover with its shaft on a press, and press out the shaft in assembly with its bearings and one outer race. Then press out the other outer race. During the pressing operation, the mandrel should be set on the inner race of the bearing or on the face of the shaft.

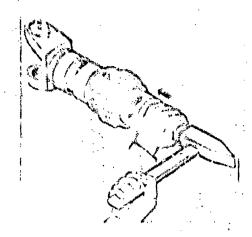


Plate 9-14. Prossing on the intermediate support bearing

Fasten the shaft and press off its bearing with a 300-7984 puller (Plate 9-15). If necessary, unserew the plug and vent (if it is not in good condition).

After disassembling the parts of the propeller shafts and intermedia.. support, it is necessary to wash them in a degressing solution, blow them out with compressed air, and check their condition.

Control checking. Excillation of the propeller shaft is checked on a stand (see Plate 9-11). Before installing the shaft on the stand, insert a mandrel into its yoke (see Plate 9-12, b).

Oscillation, measured on the end of the shaft at the voke, must not exceed 0.3 cm, and that along the length of the shaft must not exceed 0.5 cm; on the splined end, at a distance of 100 cm from the face, oscillation must not exceed 0.2 cm. If oscillation greater than that allowable is present, the shaft should be straightened with a press.

If there is wear on the hotes for the bearings, journals, and spilnes of the shaft, and also on the hotes in the intermediate support bearing covers, which is above the allowable discussions, the worn parts should be replaced.

Assembly of the universal drive. Is sembly of the universal joints on 3-axis motor vehicles is done in the same was as is that in 2-axis motor vehicles, with consideration for the marks made during disassembly. Assembly of the splined connection of the motor vehicle's rear axis projetter shaft, it is necessary to lay shaft 3 (see Place 9-3) with the welded voke and splined end 6 and allding roke 8 on a banch. Mount the protective sleere 5 and small, assembled in clamp 23 with ring seal \$2, on the splined end of the shaft. Imbrigate the splines with consistent

type grease and insert the splined end in the hole of the sliding yoke so that the arrows stamped on the shaft and the sliding yoke are located in the mans plane opposite each other. Bend tab 16 of the clamp onto the circular projection of the sliding yoke. Install the protective boot 5 in its place and fasten it with safety wires 4 and 17

Assemble the splined connections of the front and middle axle propoller shafts, and also those of the rear existintermediate shaft, in the same order. For assembly of the splined connection of the main propeller shaft, it is necessary to mount the threaded nut, supporting split washer, and folt seal on its splined end. Then insert the splined end into the splined bushing and screw the nut in assembly with the seal onto it until the seal is fully compressed onto the shaft.

The assembled propeller shafts must be dynamically balanced on a machine, Propell r shaft imbalance must not exceed 70 gram cm.

Assembly of the intermediate support. Press the inner races of the tapered bearings ento the shaft (Plate 9-16). Press one outer bearing race into the support body and insert the shaft assembly into the body, guiding one of its ends with its bearing into the pressed-in race.

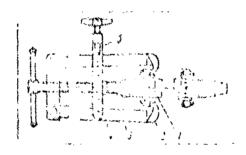


Plate 9-15. Pressing the bearing off the intermediate shaft of a ZIL-157K motor vehicle universal drive: 1) shaft 2) bearing 3) puller 4) seat 3) compression screw

furn the body over and install the second outer race on the second end of the theft with its bearing and press the race into the support body. The outer races of the hearings should be pressed in with a mandrel and press.

install the supporting and oll-repelling washers. During this, it is necessary to pay attention so that the oil-deflecting washer with the inscription Rear is mounted on the rest and of the shaft, and the one with the

inscription Front is mounted on its front end.

Assemble the covers with the soal, install one packing gesket on each of their grooves, install the adjusting gaskets on the rear cover, and then install the covers on the body with protecting rings, and fasten them with bolts.

Having fastoned the cover with bolts, it is necessary to check the free rotation of the support shaft. With properly adjusted support Dearings, the shaft must freely rotate without solving or noticeable axial clearance. If there is noticeable axial clearance, or if the shaft rotates tightly, tension on the bearings should be adjusted by changing the number of adjusting gaskets beneath the rear cover.

With proper bearing tension, the intermediate support shaft without its flanges must rotate with a moment of 0.4-0.9 kg meters applied to it.

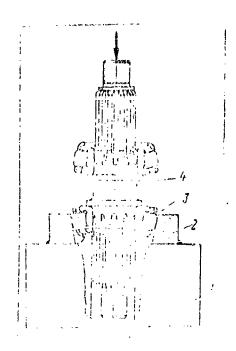


Plate 9-16. Pressing on the intermediate support bearings:
1) support 2) mandrel 3) bearing
4) shaft

After adjusting the bearings, it is necessary to install the flanges on the splined ends of the shaft, fasten thom with nuts and washers, and pin the nuts.

Screw the plug into the drain hole and fill the support body with TAp-15 oil (GOST 8412-57). The oil level is checked according to the lateral control hole. Screw the plugs into the lateral and top holes. The top plug must have the vent screwed into it.

Install the intermediate support on the middle drive axie, guiding the installing pins into the holes. Pressing the support to the upper bracket of the reaction lever, screw in the bolts by hand, tighten them with a socket wrench, and pin all four of the bolts together with soft wire. Connect the flanges of the rear axie propeller shaft yeke to the flanges of the rear axie differential input shaft and to the intermediate support, insert the bolts in the flange holes, install spring washers, screw on the nuts and tighten them until they are firmly seated.

Connect the remaining propellor shafts to the flanges of the other assemblies in the same manner.

The ZIL-131 motor vehicle

Removal of the universal drive. During removal of shafts 2, 6, and 8 (see Plate 9-5), it is necessary to unscrew the nuts fastening the flanges and, holding the shaft, drive the bolts out of the flange holes and withdraw the shaft from beneath the motor vehicle. During removal of middle axle shaft 4, it is also necessary to unscrew the nuts fastening the flanges and, holding the shaft, drive out the bolts fastening the flanges to the middle axle. Move the shaft slightly toward the transfer case so as to separate the clanges of the propellor shaft and the middle axle differential input shaft. After this, remove the propeller shaft from the bolts of the transfer case flange and withdraw it from the motor vehicle. The bolts in the transfer case flange are pressed in, and are therefore not removed. Each propeller shaft of the motor vehicle is removed independently of the others.

Disassembly of the universal drive. Before disassembling the propeller shafts removed from the motor vehicle, it is necessary to clean the dirt from them and wash them in degreasing solution. Propeller shafts are disassembled in the following order.

Lay the propeller shaft (see Plate 9.5) on a bench, mark the relative position of yoke 3 and splined bushing 6, remove the safety wire 5 and 17 with combination pliers, move the protective best 4 away from nut 16 along the axis of the shaft toward yoke 3, unscrew nut 16, and separate the shaft, withdrawing the splined yoke from the bushing. Then remove split ring 12, rubber seal 13, split washer 14, felt seal 15, the second split washer 14, nut 16, and protective boot 4 from the splined end of the propeller shaft yoke.

During disassembly of the universal joints of rear axle propellor shaft 6 (see Plate 9-5) and main propell r shaft 2, the position of the balancing plates screwed onto the faces of the fork ends should be marked, as well as the forks, so that during assembly, they can be placed in their previous positions.

Balancing plates on middle axle propeller shaft 4 and front axle propeller shaft 8 are welded on and do not require marking.

Control checking. Oscillation of the middle axle propeller shaft is checked on a stand (see Plate 9-11). Before installing the shaft on the stand, a mandrel (see Plate 9-12, b) centered along the faces of the yoke is inserted in the yoke, and a mandrel centered along the outer diameter of the splines at a length of 160 mm (at a distance of 140 mm for both remaining shafts) is installed in the splined bushing. Both mandrels have conic holes for installation in the stand centers. Oscillation at the end of the shaft with the yoke must not exceed 0.5 mm, that along the yoke must not exceed 0.4 mm, and that along the length of the shaft must be no greater than 0.7 mm. The requirements concerning oscillation are identical for all shafts. If oscillation greater than the allowable amount is present, the shaft should be straightened with a press.

Assembly of the universal drive. Before assembling the universals, it is necessary to lubricate the needle bearings with TAp-15 oil (GOST 8412-57). The lubricating passages in the cross must be cleaned out and the lubrication fitting and protector valve must be screwed into the threaded heles.

During installation of the universal crosses in the yoke eyes, it should be kept in mind that the cross lubrication fittings must face the side of the shaft and not the side of the flange.

The splined connections of all the shafts are assembled in an identical sequence. For this, it is necessary to lay the shaft in assembly with splined bushing 6 (see Plate 9-6) and splined yoke 3 on a bench. Install the protective boot 4, nuts 16, felt neal 15 with slotted washer 14, rubber seal 13, and stated ring 12 on the end of the splined fork. Then smear the splined ends of the main propeller shaft, front axle shaft, and rear axle shaft with a quantity of 0.24 kg of consistent type grease on each shaft. Besides this, permanent grease is also packed into the splined bushing. The quantity of 0.46 kg of it is put into the splined connection of the middle axle propeller shaft. Insert the splined end of the splined fork into the splined bushing. The arrows stamped on the bushing and splined fork must be located opposite each other. If there are no arrows on the parts, it is necessary to assemble the shaft in such a manner that the axes of the yokes (for the bearings) are located in the same plane.

Slotted ring 12 and rubber seal 13 are inserted in the depression in the splined bushing, and slotted rings 14 and felt seal 15 are mounted inside nut 16. During this operation, the slotted washers of the felt ring must be installed so that their slots are on different sides. Then mount the nut on the threaded end of the splined yoke, and tighten it until it is firmly seated.

Install the protective boot 4 in place and fasten it with safety wires 5 and 17. A protective boot is not installed on the main propellar shaft.

If any of the parts of the assembled propeller shafts are replaced or repaired, the shafts must be subjected to dynamic balancing.

Aside from the middle axle shaft, imbalance in the propeller shafts of the ZIL-131 motor vehicle is not allowed to be greater than 70 gram cm on each end. Imbalance on the middle axle propeller shaft is not allowed to be greater than 100 gram cm. Balancing propeller shafts, besides the main and rear exle shafts, is accomplished by welding balancing plates on both ends of the shaft. The rumber of plates welded onto the shaft must be no greater than three on each side of the shaft. Balancing of the main propeller shaft and the rear exle shaft on the side of the non-splined yoke is also achieved by welding balancing plates to the tube, and on the side of the splined yoke, it is achieved by screwing balancing plates ento the faces of the yoke eyes. Total thickness of the plates screwed onto the eyes must not exceed 3 mm.

Installation of the universal drive on the motor vehicle. Connect the flanges of the rear axle propeller shaft yoke to the flanges of the differential input shafts of the middle and lear axles, insert bolts in the flange holes, install spring washers, screw on nuts, and tighten them until they are firmly seated.

Connect the remaining propeller shafts of the motor vehicle to the flanges of their corresponding assemblies.

Dimensions of parts

Dimensions of the basic parts are presented in Tables 9-1, 9-2, 9-3, 9-4, 9-5, and 9-6.



Plate 9-17. Arbitrary designations of dimensions of two-axle motor vehicle universal drive parts

Table 9-1. Dimensions of propeller shafts of the ZIL-130 motor vehicle and its modifications, mm (Plate 9-17)

Longth	ZIL-130	ZIL~130B1	ZIL-130G
Rear axle propeller shaft in assembly along the axes of the universal in working position (dimension A)	1425	943	1425

Table 9-1. Dimensions of propeller shafts of the ZIL-130 motor vehicle and its modifications, mm (Plate 9-17)

Length	ZIL-130	ZIL-130B1	ZIL-130G	
Rear axle propeller shaft in assembly along the axes of the universal in working position				
(dimension A)	1425	941	1425	
Splined yoke				
(dimension B)	248	248	248	
Intermediate shaft in assembly from front universal to rear face of shaft				
(dimension C)	594	594	1295	

Table 9-2. Dimensions of propeller shafts of the ZIL-157K motor vehicle, mm

Dime:.sion	Dimension value
Total length of propeller shafts in assembly (from flange face to flange face in working position):	
Main shaft	443
Front axle shaft	1350
Middle axle shaft	1196
Rear axle shaft	689
Rear axle intermediate shaft	1267

Table 9-3. Dimensions of propeller shafes of the ZIL-131 motor vehicle, mm

Dimension Dimension value

Total length of propeller shafts in assembly L between flange faces (see Plate 9-6):

[able 9-3, continued]

Main shaft	679
Front axle shaft	1238
Middle axle shaft	1098
Roar axlo shafe	802

Table 9-4. Basic dimensions	of universal drive pa vehicle, mm	rts of the 7 L-130 motor
Dimension	Nominal	Allowablo without repair
	Propoller shafts	*
Type 20 steel; tubing drawn o	of cold rolled plate (TU-1046-62); hardnessHRB 80
Exterior diameter Interior diameter	77 71	4 0
	-	
<u>Uni</u>	versal yoke (welded o	<u>n)</u>
Type 35 steel (GOST 1050-60);	hardnessHB 207-241	•
Diameter of hole for needle bearing Diameter of journal assembled with	38.99-39.027	39.05
internal diameter of two	70.96-71.05	
bearing support plate fastening bolts	M8, 21ass 2	
	Flange yoke	
Type 35 steel (GOST 1050-60);	hardnessHB 217-255	•
Dismeter of hole for needle bearing Diameter of centoring	38.99-39.027	39.05
collar for groove in assembled flange Diameter of threads for	94.93-95.00	94.91
bearing support plute fastening bolts	M8, class 2	·

[Table 9-4, continued]

Diameter of holes for flange fastening bolts	14.24-14.36	15,00
Dimension from axis of bearing hole to support		
face	65	

Universal cross

Type 20KhGNTR steel (ChMTU 22-58) TsNIIChM; depth of nitrided layer on journals-1.1-1.5 mm; surface layer nardness--HRC 60-65.

Cross length along journal		
faces	107.925-107.960	107.80
Journal diameter for needle bearing	24.960-24.980	24.92
Thread diameter for lubrication fitting		
and valve	K1/8 (GOST 6111-52)	

Sliding yoke

Type 45 steel (GOST 1050-60); depth of case hardened layer--2-4 mm; hardness of case hardened layer--HRC 42-56.

Diameter of hole for		
needle bearing	38.99-39.027	39.05
Diameter of contering		
journal	53.92-53.95	53.87
Exterior contoring		
diameter of splines	61.895-61.935	61.85
Diameter of splined		
sectioned circumference	55	≠ **
Spline width along arc of		
sectioned circumference	4.561-4.681	4.000
Groove length	75	~ -
Diameter of threads for		
bearing support plate		
fastoning bolts	M8, class 2	

Intermediate propeller shaft splined bushing

40Kh steel (GOST 4543-61); hardness--HB 255-258.

divided circumference	55	
bearing Diameter of splined	69.99-70.01	**
Diameter of journal for shaft Diameter of journal for	70.96-71.05	

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[Table 9-4, continued]

Internal spilned diameter	54.00-54.06	54.10
External splined diameter	62.00-62.06	62.10
Width of groove in bushing		
splined portion along		
arc of separated		
circumforonce	4.73-4.815	5.2
Diameter of thread for		
bearing spacing bushing		
fast oning nut	M70 X 1.5	~ •
Length of splined portion	155	• •

Bearing spacing bushings of intermediate shaft support

Type 45 steel (GOST 1050-60); depth of case hardened layer--1.5-3.0 mm; hardness--HRC 45-56.

Exterior diameter	79.88-80.00	79.70
Interior dismeter of		
spacing bushing	70,00-70.06	70.10

Front and rear covers of intermediate shaft support bearing

08 steel, leaf thickness--1 mm (GOST 3680-57 and GOST 914-56).

Diameter of hole for support bearing

Dimension

109.965-110.070

--

Allowable without repair

Table 9-5.	Basic	dimensions	of	universal	drive	parts	of	the	ZIL-157K	motor
				vehicle		•				

Novinal

|--|

Propeller shafts

Type 20 steel (tubing drawn of cold-rolled plate, TU 1018-61); hardness--HB 80-100.

External diameter 76² -Internal diameter 71² --

yehicle.

Tubes with an external diameter of 77 mm and an internal diameter of 71 mm are acceptable.

¹ Dimensions for the flange yoke, universal yoke, universal cross and its bearings for the ZIL-157K motor vehicle are the same as those for the AIL-130 motor vehicle.

[Table 9-5, continued]

Universal sliding yoke

40Kh steel (GOSY 4543-61); hardness--HB 207-241.

Diameter of hele for		
needle bearing	38.99-39.027	39.05
Width of groove in yoke		
eplined portion	3.480-3.527	3.9
Determal diameter of		
splines	37.960-38.027	38.12
Length of splined portion	:	
Main shaft	140	
Other shafts	130	

Propeller shaft splined end

45Kh select steel (0.45-0.50%, GOST 4543-61); hardness--HRC 43-50.

Tooth thickness	3.410-3.455	3.00
External diameter of		
splinos	37.900-37.950	37.86
Length of splined		
portion:		
Main shaft	80	
Other shafts	160	< =

Shaft for rear axle propeller shaft intermediate support

39.99

5.7

40Kh steel (GOST 4543-61); hardness--HB 321-401.

Diameter of shaft journal for bearing 40.009-40.027 Spline thickness 5.925-5.975

Rear axle propeller shaft intermediate support housing

KCh 35-10 iron (GOST 1215-S9).

Diameter of hole for

bearing 89.974-90.009 90.04

Rear axle propeller shaft intermediate support bearing cover

SCh 15-32 iron (GOST 1412-54).

Diameter of hole for seal 82.00-82.97 --

[Teble 9-5, continued]

Rear axle intermediate shaft support flange

Type 45 steel (GOST 1050-60); depth of case hardened layer--1-3 mm; hardness of case hardened layer--HRC 52-62.

Diameter of flange journal		
for seal	54.88-55.00	\$4.60
Diameter of turning for		
flange yoke	95.000-95.054	95.07
Diameter of hole for		
fastening bolts	14.24-14.36	15.00

Table 9-6. Basic dimensions of middle axle propeller shaft parts of the ZIL-1S1 motor vehicle, mm			
Dimension	Nominal	Allowable without repai	
	Propeller shaft		
Type 20 stoel (tubing drawn	of cold-rolled plate);	hardnessHB 80-100.	
Exterior diameter Interior diameter	89 82		
	Universal yoke		
Type 35 steel (GOST 1050-60); hardness -HB 207-241.		
Diameter of hole for needle bearing Diameter of journal for	50.000-50.027	50.05	
internal diameter of propellor shaft Diameter of threads for bearing support plate	82.19-82.26	*-	
fastening bolts	M8, class 2	• •	
	Plange yoke		
Type 35 steel (GOST 1050-60); hardnessHB 207-241.		
Diameter of hole for needle bearing Diameter of centering	50.000-50.027	50.05	
journal for turning in flange	94.93-95.00	94.90	

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[Table 9-6, continued]

Diameter of threads for bearing support plate		
fastening bolts	M8, class 2	••
Diameter of hole for	·	
flange fastening bolts	16.24-16.36	17.00
Dimension from axis of		
bearing hole to		
supporting face	76	

Universal cross

20KhGNTR steel (ChMTU 1285-65) TsNIIChM; depth of hardened layer--1.8-2.2 mm; hardness of surface layer--HRC 60-65.

Length of cross along		
journal faces	126.91-126-95	126.80
Journal diameters for		
needle bearings	33.593-33.620	33.55
Diameter of threads for		
lubrication fitting and valve	K1/8 (COST 6111-52)	* *

Universal splined yoke

Type 45 steel (GOST 1050-60); depth of case hardened layer--2-4 mm; hardness of case hardened surface--HRC 42-56, core hardness--HB 207-241.

Diameter of hole for		
noedle bearing	50.000-50.027	50.05
Diameter of centering		
journal	63.94-63.97	63.88
External centering		
diameter of splines	71.895-71.935	71.85
Diameter of splined	4.5	
divided circumference	65	
Spline thickness along arc of divided		
circumference	4.596-4.681	4,000
Diameter of threads for	**************************************	***************************************
bearing support plate		
fastening bolts	NO, class 3	~ ~
Length of splined portion	75	m 04

Splined bushing

40Kh steel (Q)ST 4543-61); hardness--HS 255-285.

Diameter of journal for propeller shuft 82.19-82.26

Control of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the second of the s

[Table 9-6. continued]

Interior diameter of	•	
e sp lines	64.00-64.06	64.10
Exterior diameter of		
splines	72.00-72.06	72.10
Diameter of spline		
divided circumference	65	••
Width of splined bushing		
grooves along atc of		
divided circumference	4.73-4.815	5.2
Length of splined portion	181	
Diameter of threads for		
splined connection		
packing fastening aut	M85 X 1.5, class 3	

Chapter 10. The Drive Axle

Layout

The ZIL-130 motor vehicle. Plate 10-1 shows a longitudinal section of the rear axle of a ZIL-130 motor vehicle. The main drive of this axle is two-stage and is made up of a pair of beveled gears with spiral teeth and a pair of cylindrical gears with helical teeth.

The ZIL-130 motor vehicle uses a steel stamped welded drive axle carrier with welded-on flanges for fastening the wheel brake and rear cover supports.

The overall length of the rear axle carrier of the ZIL-130 motor vehicle is 2036 mm, and the tread of the rear wheels is 1790 mm.

The cups of the rear axle differential box are steel. The differential pinions of the ZIL-130 motor vehicle are equipped with bronze bushings.

Halt-shafts of the ZIL-130 motor vehicle are steel with reinforced flanges.

The half-shafts are fastened to the ZIL-130 motor vehicle by twelve study with conic split bushings. Stud diameter is 16 mm.

In line with further increasing the reliability of the rear axle main drive of the ZIL-130 motor vehicle, fastening of the cylindrical drive gess shaft bearing cover was strengthened by increasing the number of cover fastening bolts from six to eight (introduced into production in October 1965).

On the IIL-M62-555 dump trucks, instead of a gear ratio of 6.97 : 1, a gear ratio of 6.45 : 1 is used (introduced into production at the end of the

third quarter of 1965).

20NKhH steel is used as the material for the cylindrical drive gear instead of 18khGT steel.

Further 'ncreasing the reliability of the rear axis 5 %18 is accomplished by introducing adjusting teeth. With the introduction of this change, the final drive gear ratios were changed: from 6.45: 1 to 6.32: 1, and from 6.97: 1 to 6.99: 1. The adjustment gears are not interchangeable with the gears manufactured without the indicated correction.

Table 10-1 projects the total gear ratios and the number of teeth in the rear axle final drive glars.

The ZIL-157K motor vehicle. On the ZIL-157K motor vehicle and its modifications, all three exics are driving ones. The front exic assembly is shown in Plates 10-2 and 10-3.

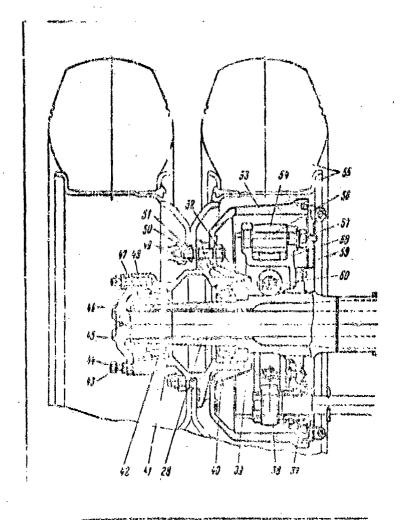
The middle and rear axle assemblies with their belancing suspension are shown in Plate 12-16 (see Part 2).

Each drive axle of the 21L-157K motor vehicle is a hollow-bodied rail which is disassembled in a vertical plane, and in which the final drive, differential (Plate 10-4), and drive wheel power are located. The final drive and differential of all three axles are interchangeable.

The drive axis final drive consists of a pair of beveled goars with helical teeth. The drive gear in assembly with its bearing), installed in the carrier, is shown in Plate 10-5. The final drive goar ratio is 6.67: 1. The drive axis half-shafts are not lead-bearing. The front axis half-shafts (Plate 10-6) have joints of equal rates of angular motion. The wheels on the front axis are the steering ones.

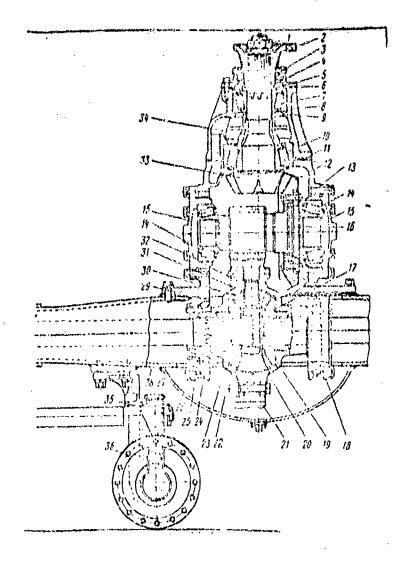
Steering spindles with ball support I are installed on the front axis (Plate 10-7). The steering spindles are connected with the body 10, which turns on tapered roller bearings 8 and 15, installed on king pins 11, which are pressed in and welded on the stationary ball support of the axis rail. Hab 19 (see Plate 10-5) is installed on spindle 46 with tapered roller bearings 18.

All axies of the III-157K motor vehicle (flate 10-8) are equipped with a centralized system for regulating air pressure in the tires with air being supplied to the tires through passage 4 in the stands (Plate 10-9) and the circular clearance between spindle 2 and its hading 1.



Olate 10-1. Rear axie of the ZIL-130 motor vehicle:

1) not 2) flange 3) seal 4) cover 3) support washer 6) gasket 7) front bearing 8) bearing carrier 9) adjusting washer 10) rear bearing 11) gaskets for adjusting bevoled gear engagement 12) driven avoid gear 13) adjusting gas(_ts 14) intermediate shaft bearings 15) bearing cover 16) driving cylindrical gear 17) right half-shaft gear 18) differential bearing cover 19) support washer 20) right differential box cup 21) driven cylindrical gear 22) left half-shaft gear 23) left differential box cup 24) differential box bearing 25) differential box bearing adjusting nut 26) stop belt 27) adjusting lever worm aschanism 28) rear axie housing 29) reduction gear housing



[Plate 10-1, continued]

30) differential pinion 31) differential pinion support washer 32) cross 35) pinion gear 34) spacing bushing 35 and 37) brackets for fastening spreader cam shaft 36) brake chamber 38) spreader cam 39) oil deflector 40 and 42) wheel hub bearings 41) wheel hub 43) bearing adjusting nut 44) puller bolt 45) half-shaft 46) stop nut 47) lock washer 48 and 52) seals 49) box nut for fastening inner wheel 50) nut for fastening outer wheel 51) hub lug studs 53) brake drum 54) brake shos 55) wheel 56) shoe shaft 57) shee shaft nut 58) brake support 59) backing plate 60) brake return spring



Plate 10-2. Overall view of the front axla of a 21L-157K motor vehicle

Table 10-1. Gear ratio and number of gear tenth in the final drive of a ZIL-150 motor vehicle and its modifications

Motor vehicle	Overall rear	&xle		Number o	of gear teeth	
	geer ratio		level ion	Bevel driven	Cylindrical driving	Ring gear
21L-130 21L-130G and .					÷	
21L-M42-S551	6.45 : 1	1	.3	25	14	47 or 46
	or 6.32 : 1					
ZIL-130V1	6.97 : 1					
	or			_		
	6.99 : 1	11 0	r 13	. 25	15 or 11	46 or 40

¹ Rear axles of the ZIL-MWZ-555 motor vehicle were produced with a goar ratio of 6.97: 1 only until the beginning of the third quarter of 1965.

The ZIL-131 motor vehicle. On the ZIL-131 motor vehicle and its modifications, all three axles are driving ones. The front axle assembly is shown in Plate 10-10 and 10-11.

The middle and rear exto assemblies are shown in Plate 10-12. The drive

aric rails are steel and are welded from two stamped halves with welded-on flanges and covers.

The reduction gear of the rear and middle axles (Plate 10-13) is installed above the axle carrier and is fastened to it with a horizontal flange. The reduction gear of the front axle (Plate 10-14) is fastened to the axle carrier with a vertical flange. In all three reduction gears, the double pinion gear shafts and bevel driven gears (Plates 10-15 and 10-16), the differential gears (Plate 10-17), the bearing recerses, and the bearings are interchangeable. The final drive is two-stage, with a pair of bevoled gears with spiral teeth and a pair of cylindrical gears with helical teeth. The final drive gear ratio is 7.339: 1.

The half-shafts are not loaded. The front axle half-shafts (Plate 10-18) have joints with equal rates of angular motion.

The wheels of the front axle are the steering ones. Turning spindles with a ball support (Plate 10-19) are installed on the front axle. All axles are equipped with a contralized system of regulating air pressure in the tires by supplying air to the tires through bales in the spindle (Plate 10-20) and a passage drilled in the half-shaft.

Fitting 4, screwed into the herd of the air supply passes through the hole in the spindle.

To provide stream fording capability, all axles are sealed.

Technical service

During US, conduct cleaning operations and an external inspection of the drive extes.

During TS-1, it is necessary to check the fastening of the reduction gear and the absence of leaks in the drive axle connections.

During TS-2, check for the absence of oil leaks through the seals and connecting flanges. Seals and packing gaskets which are in poor condition must be replaced, and flange connecting bolts and nuts must be tightened. Check the fastening of the half-shaft flanges to the wheel hubs, and the fastening of the front cover of the beveled spindle gear bearing. Wash out the air passages of the vents. Clogging of the vents may cause increased internal pressure in the axle housings, which will serve as a reason for oil leakage through the seals and connections.

On the ZIL-131 motor vehicle, besides the drive axle vents, it is necessary to wash out the additional vents for air exhaust in case of improper functioning of the head seals of the system of air supply to the tires. The appearance of lubrication from the holes in these seals indicates air leakage from the system of regulating air pressure in the tires.

It is necessary to eliminate the reason for this zir leakage, and if necessary replace the head for air supply to the tires.

On three-axle motor vehicles, it is necessary to check the fastening of the ball support to the half-shaft body flange and the fastening of the turning spindle arm.

Adjustment of the front axle king pin bearings on a three-axle motor vehicle. Every other TS-2, it is necessary to check the tightness of the front axle king pin bearings and adjust the bearings if there if axial clearance.

Axial clearance of king pin bearings is not allowed.

For adjustment of the king pin bearings on a three-axle motor vehicle, it is necessary to disassemble the steering spindle unit and adjust the bearings by changing the thickness of the set of adjusting gaskets.

After final adjustment, the number and thickness of the gaskets at the top and bottom bearings must be identical or differ by one thin gasket (0.05 mm thick). This is necessary to assure alignment of the turning spindle and ball support.

After adjusting the bearings, tighten the lower and upper cover fastening nuts until they are firm, and check for the correct adjustment of the bearings with a dynamometer. The force necessary for smooth turning of the spindle from one extreme position to the other, applied at the hole of the steering linkage arm, must be 2.25-2.75 kg for a ZIL-157K motor vehicle, and 2.0-2.4 kg for a ZIL-131 motor vehicle.

Tightness of the final drive bevel pinion gear shaft bearings is checked every third TS-2.

For this it is necessary to disconnect the propollor shaft from the shaft flange, set up an indicator directing its rod at the shaft face, and measure the axial clear nce. Set the shaft in its extreme position until it stops, at which point the indicator hand should be set in the zero position, and move the pinion gear shaft along its axis with a pry bar.

The deviation of the hand from the zero position shows the amount of axial clearance in the shaft bearings.

Axial clearance in the bearings is not allowed.

The method of checking axial clearance in the shaft bearings of a two-axie motor vehicle is shown in Plate 10-21, and that for a three-axie vehicle is shown in Plate 10-21, b. If a clearance is discovered, it is necessary to unpin the flange fastening nut and attempt to tighten it with a wrench.

If after tightening the nut the axial clearance is not eliminated or the shaft rotates tightly, with great effort, then the bearings must be adjusted.

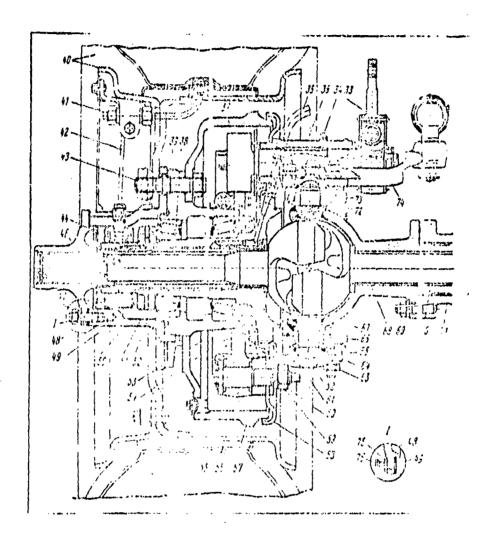
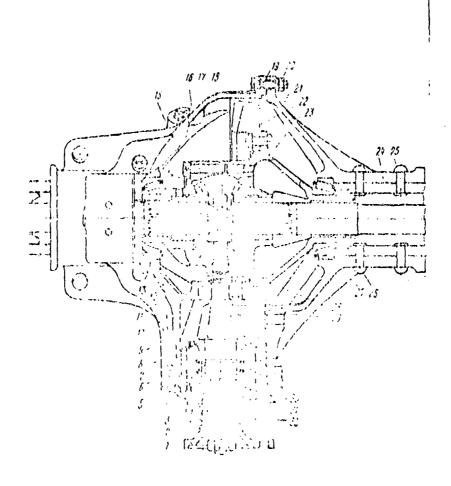


Plate 10-3. Front drive axio of the ZIL-157K motor vehicle in section:
1, 20, 47, 59, 60, 63, and 69) nuts 2) flange 3, 26, 53, 54, and 67) seats
4) cover 5) bearing carrier 6) adjusting garkets 7) adjusting washers
8, 10, 27, 38, and 73) bearings 9) pinion gear 11, 15, and 31) support
washers 12) differential pinions 13 and 23) differential box care
14 and 68) half-shafts 16) half-shaft gear 17 and 30) bolts 18) axio
housing 19) gasket 21) housing cover 22) ring gear 24) half-shaft tube
25) rivet 28) cross 29) support plate 32) deflector 33) brake adjusting
lover 34) lubrication fitting 35) spreader cam bracket 36 and 42) air
supply tubes 37) spreader cam 39) wheel hub 40) wheel 41) valve



[Plate 10-3, continued]

43) lug stud 44) air supply head 45) air supply passage 46) spindle
48) splined flange 49) hubcap 50) stop nut 51) lug washer 52) nut
55) shoe shaft 56) brake shoe 57) brake drum 58) backing plate 61) stub
axle 62) bearing cover 64) spacing ring 65) adjusting gaskets 66) bolt
70) ball support 71) half-shaft jacket 72) king pin 74) stoering arm
75) stop nut 76) puller bolt

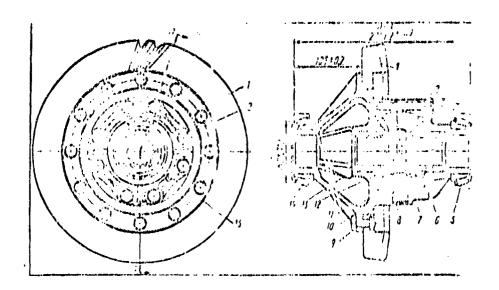


Plate 10-4. Drive axle differential of the ZIL-157K motor vehicle:

1) ring gear 2) bolt 3, 11, and 12) support washers 4 and 10) differential box cups 5 and 14) becrings 6 and 13) half-shaft gears 7) differential pinion 8) cross 9) rivet 15) safety wire

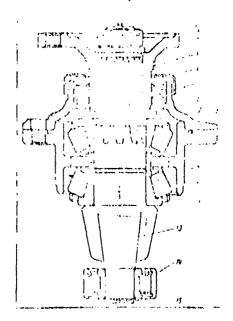


Plate 10-5. Pinion gear in assembly with bearing carrier:

1) nut 2 and 6) support washers 3) flange
4) deflector 5) seal 7) cover 8) sealing ring 9, 12, and 14) bearings 10) adjusting washers 11) bearing carrier 13) pinion gear with shaft 15) stop ring

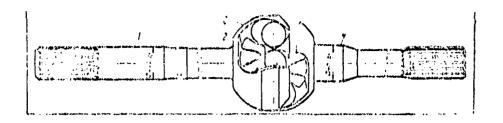


Plate 10-6. Front axle half-shaft assembly:
1) inner half-shaft 2) middle ball 3) outer ball 4) stub
axle

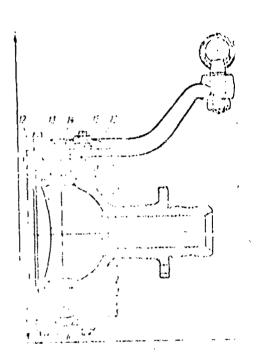


Plate 10-7. Ball support (left) in assembly with cone:

1) ball support 2) seal 3) bolts
4) rubber packing 5 and 13) nuts
6 and 17) support rings 7 and 14) covers
8 and 15) bearings 9 and 16) adjusting gaskets 10) body 11) kingpin
12) bevoled split bushing

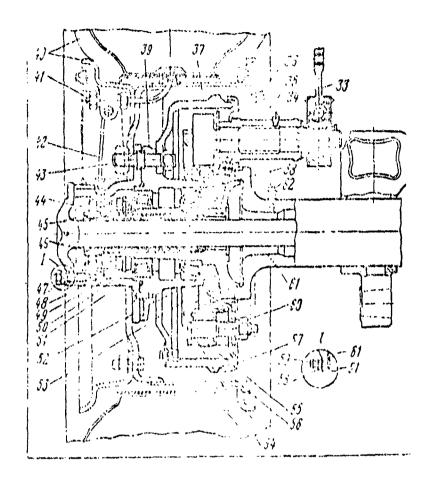
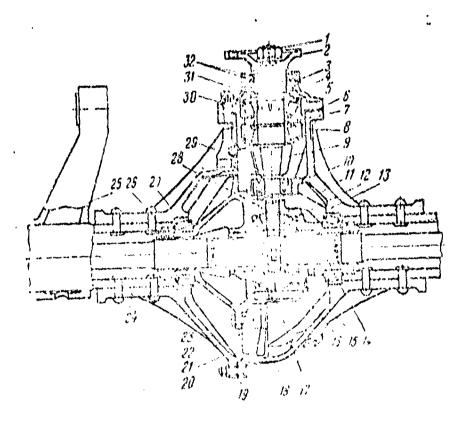


Plate 10-8. Rear drive axle assembly of the ZIL-157K motor vehicle:
1,20, 47, and 60) nuts 2) flange 3) seal 4) cover 5) bearing carrier
6) adjusting gaskets 7) adjusting washers 8,10, 27, and 38) bearings
9) pinion gear 11, 15, and 31) support washers 12) differential pinion
13 and 23) differential box cups 14 and 61) half-shafts 16) half-shaft
gear 17 and 30) bolts 18) axle housing 19) pasket 21) housing cover
22) ring gear 24) half-shaft tube 25) torque rod bracket 26, 52, and
53) seals 28) cross 29) support plate 32) deflector 33) brake adjusting
lever 34) lubrication fitting 35) spreader cam bracket 36 and 42) air
supply lines 37) spreader cam 39) wheel hub 40) wheel 41) valve 43) hub
lug stud 44) air supply head 45) air supply passage 46) spindle 48) stop
nut 49) lock washer 50) bearing nut 51) hubcap 54) shoe shaft 55) brake
shoe 56) brake drum 57) backing plate 58) stop nut 59) puller bolt
62) vent



[Plate 10-8, continued]

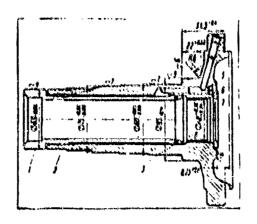


Plate 10-9. Spindle assembly:

1) steel spindle bushing 2) spindle

3) bushing seal 4) air supply passage 5) passage plug 6) support washer

7) bronze spindle bushing

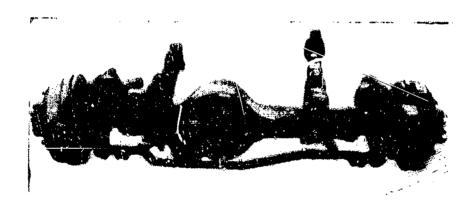


Plate 10-10. Overall view of ZIL-131 motor vehicle front axle

For adjustment of bearings on the final drive hevel pinion sheft in twoaxie and three-axie motor vehicles, see the "Disassembly and Assembly" section in this chapter.

The method of checking tightness of bearings on the bevel gear shaft in the rear axle of a two-axle motor vehicle is shown in Piate 10-22, a, for drive axles of the ZIL-137K motor vehicle, it is shown in Plate 10-22, b, and for drive axles of the ZIL-131, it is shown in Plate 10-22, c.

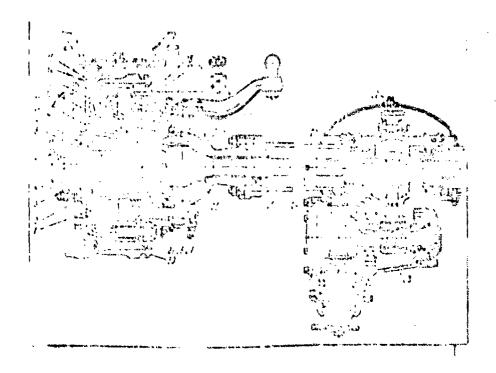


Plate 10-11. Front axle of 211-131 motor vehicle in section:

1) hub 2) spindle 3) hub bearing fastening nut 4) protective jacket 5) valve 6) stop nut 7) stub axle splined flange 8) lock washer 9 and 11) hub bearings 10) air supply hose to tire 12, 14, and 29) seal* 13) fitting for air supply 15) nut 16) spreader cam bracket 17) angle fitting 18) lubrication fitting 19) inner half-shaft 20) ball support assembly 21) vent 22) control hole plug 23) front axle reduction gear assembly 24) reduction gear housing cover 25) axle carrier 25 ball support centrol plug 27) air supply head 28) plug 30) backing plate

Lubrication of drive extes. Changing and adding oil should take piece within the period shown in the lubrication charts. It is necessary to change the oil in the drive extes of two-exte and three-exte motor vehicles immediately after stopping the motor vehicle, when the drive exte is still ward.

Before changing and adding oil to the drive axles, clean off dust and diff from the housing around the filler hole plug.

Oil should be drained through all the existing drain holes,

After draining the cil, it is necessary to pour 4-5 liters of low viscosity cil (industrial 12 or 20, COST 1"07-51) and wash out the housing.

Pouring in oil for washing should be done the same as for for housing.

In the 211-131 motor vehicle, there is a drain hole located in the lower part of the front axle housing which serves to drain used oil from that housing. The rear and middle axles each have two drain holes: in the lower part of the housing cover and in the front wall of the reduction gear housing. Used oil should be drained through all existing drain holes.

Control holes during this operation must be closed.

Oil must be poured into the rear axie of two-axis motor vehicle and the drive axies of the ZIL-157K motor vehicle up to the edge of the control hole.

After adding or changing the oil, remaining oil should be carefully cleaned off the surface of the drive axles so as to avoid the adherence of dust and dirt to it.

On the ZIL-131 motor vehicle, oil is powed into the housing of the front drive axle through the control hole located on the front part of the axle in the housing cover. Oil should be added to the reduction gear of the rear and middle axles through the plug in the inspection hole located on the upper wall of the reduction gear housing until a flow of oil appears from the open control hole.

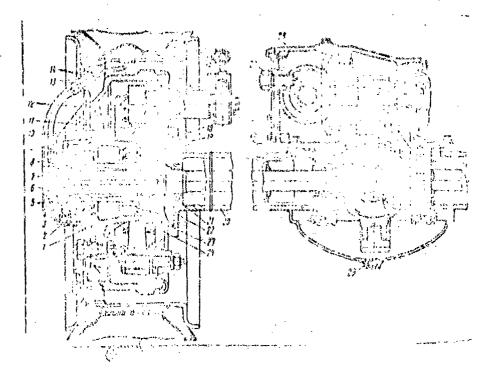
Oil level in the rear and middle axles should be checked during the process of operating the ZiL-131 motor vehicle with oil level indicator 1 (Plate 10-23) which is in the tool set, for which it is necessary to unscrew the rear holt fastening the reduction gear to the axle housing and insert the oil level indicator in the solt hole until it rests against the boss of the reduction gear housing flange.

the proper level of oil is marked by a line on the oil level indicator. If the sil level has sropped to below the line, it is necessary to add oil to the housing up to the level of the control hole.

After fording streams or filled ditches with two-axle or three-axle motor vehicles, check and see that no water has gotten into the drive axle housing.

The presence of water in the oil may be determined by a change in the color of the oil. It is checked immediately after stopping the automobile or otherwise it may settle out of the oil. Unacrewing the drain hole plug, drain the water. If water is discolored, it is recessary to drain the old oil from the housing and fill the housing with fresh oil according to the lubrication chart.

During TS-2, it is necessary to add lubrication to the stub axis joint and the king pin bearings of the front drive sale in three-sale motor vehicles. Grease must be pressed in in a warm condition.



Piate 10.2. Middle and rear axie assemblies of IL-131 motor webicle;
1) hub 2) spreader hushing 3) stub axie 4) spindle 5) protective jacket
6) valve 7) stub nut 8) bearing nut 9) lock washer 10) hose for rir
supply to tire 1!) ficting for air supply to stub oxie 12) spreads cam
13) seal 14) nut 15) spreader cam bracket 16) angle fitting 17) lubrication
2itting 18) hose connection backing 19 and 25) vent 20) axis housing
21, 23, and 24) seals 22) air supply head 26) reduction gear cover
27) policy belt 28) reduction gear assembly 29) drain hole plug

Before lubricating the stub axle joint of a 21L-157K motor vehicle, it is necessary to unscrew the vent installed on the upper portion of the turning spindle body and add great until it begins to essarge from the vent help.

Grease must be added to the stub axle joint of the ZIL-131 motor vehicle through the lubrication fitting located on the top cover plate of the right turning spindle body, and the turning arm installed on the left spindle turning body. Grease must be pressed in until it begins to emerge through the control hale located beneath the ball support. The control hale plug must have been previously unscrowed.

The Lubrication in the stub axle ball joint of three-axle motor vehicles must be changed every 5,000-17 000 km of operation. When changing the oil, washout all parts of the turning spinsies and stub exterball joints with low viscosity oil

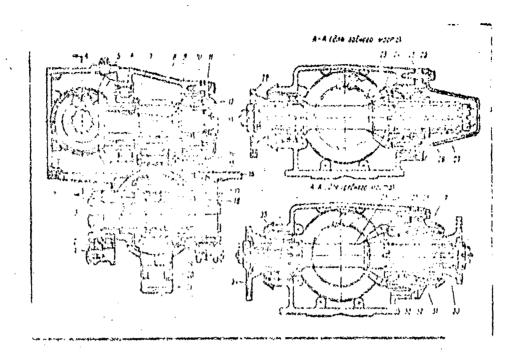


Plate 10-13. Reduction gear assembly of rear and middle axles in the ZIL-131 motor vehicle:

1) bearing pover 2) nut lock 3) adjusting nut 4; drain hole plug 5) driven bevol gear 6) key 7) spacing ring 8) driving cylindrical gear 9) traing recess 10 and 25) adjusting washers 11 and 26) bearing covers 12) two-row reller bearing 13) adjusting ring 14 and 19) support washers 15) differential pinion (6) reduction gear housing 17) cross 18) half-shaft gear 20; differential box cup 21) ring gear 22, 30, and 34) propellor shaft fastening flanges 23) transfer shaft 24) bevel pinion gear 27) spacing bushing 28) washer 29) bearing cover 31) oil blocking washer 32) tapered reller bearing 33) adjusting washers 35) seal

Fresh grease is packed inside the ball support, in the king pin bearings and in the stub axle ball joint.

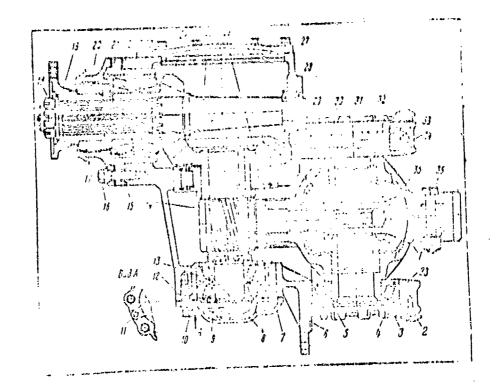


Plate 10-14. Front axle reduction gear of the ZIL-131 motor vehicle:

1) differential box cup 2) bolt 3) stop 4) adjusting nut 5, 8, 22, 26, and 28) bearings 6) reduction gear housing 7, 20, 27, and 33) covers 9, 18, and 34) nuts 10) bearing recess 11) plug 12 and 15) adjusting gaskets 13 and 23) adjusting rings 14) driving cylindrical gear 16 and 36) bolts 17) seal 19) flange 21) bevel pinion gear shaft housing 24) bevel pinion gear 25) driven bevel gear 29) differential pinion support washer 30) half-shaft gear support washer 31) differential pinion 32) half-shaft gear 35) cross

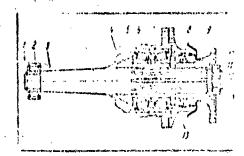


Plate 10-15. Front axle pinion gear with bearings in assembly:
1) stop ring 2 and 5) bearings
3) shaft 4) pinion gear 6) bearing carrier 7) adjusting washer
8) cover 9) flange 10) washer
11) nut 12) cotter key 13) oil deflecting support washer

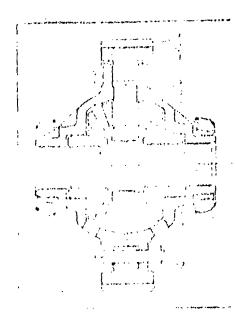
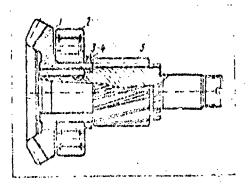


Plate 19-17. Differential assembly:
1) differential ring gear 2) differential box cup 3) cross 4 and 6) support washers 5) differential pinion 7) half-shaft gear 8) bearing 9) bolt



Place 10-16. Driven bevel and driving cylindrical gear assembly of the reduction gear;

1) driven bevol gear 2) bearing
3) key 4) spacing ring 5) driving cylindrical gear

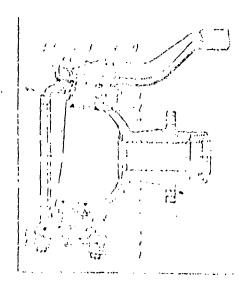


Plate 10-19. Ball support assembly:
1 and 15) plugs 2) king pin bearing
cover 3 and 5) adjusting gaskets
4) turning spindle body 6) conic
spreader bushing 7) cover with spindle
arm 8) lubrication fitting 9 and 19)
nuts 10 and 18) bearings 11) packing
ring 12) ball support seal 13) halfshaft soal 14) support washer 16) ball
support with king pins in assembly
17) plug

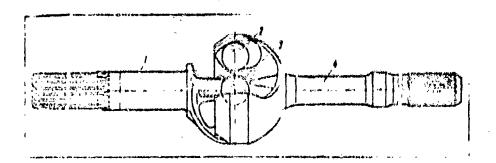


Plate 10-18. Half-shaft assembly:
1) stub ax1e 2) driving ball 3) center ball 4) inner half-shaft

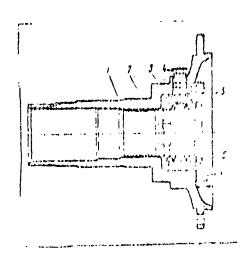


Plate 10-20. Turning spindle in assembly:
1) spindle 2) bushing 3) air supply head
assembly 4) fitting 5) support ring
6) support washer

Disassembly and assembly

The ZIL-130 motor vehicle

Removing the rear axle from the motor vehicle. In order to roll out the rear axle of the ZIL 130 motor vehicle, it is necessary to stand the motor vehicle on a level surface or on an inspection pit which is equipped with a hoisting device. With the hoisting mechanism, raise the rear part of the frame so that the rear springs are unloaded.

Disconnect the ends of the rear suspension springs from the frame brackets and raise the frame (Plate 10-24). Disconnect the propellor shaft from the rear axle input shaft flange, having previously set blocks or a jack beneath the reduction gear.

Roll the rear axie out from beneath the frame, holding on to the reduction gear. Lower the frame onto supports.

Disassembly of the rear axle. Remove the wheels, springs, and brake chambers. Drain the oil, knock off the dirt, wash the axle off in degressing solution, and blow it off with compressed air.

For disassembly of the rear axle, the GARO trust puts out a special stand, model 689-00-00 (Plate 10-25). If this stand is not available, it is possible to disassemble the axle by installing it on supports.

Removal of the half-shafts and hubs. Unscrew the nuts fastening the half-shaft to the hub, remove the spring washers and withdraw the conic split bush is. Screw two M12 X 1.75 bolts into the heles in the half-shaft flange intended for removing the half-shaft, move it from its place, and then withdraw the half-shaft from the axle housing space and remove the half-shaft flange gaskets. Withdraw the other half-shaft from the rear axle housing in the same manner.

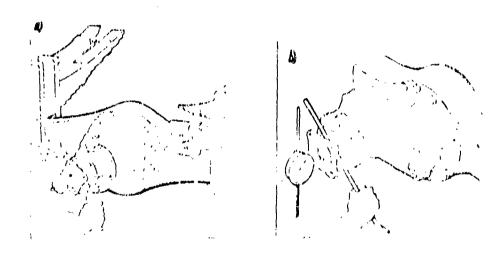
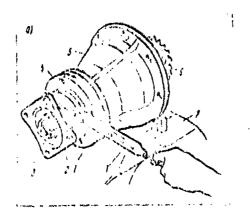
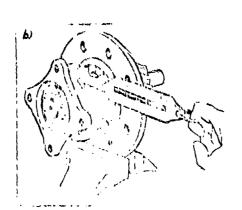


Plate 10-21. Method of checking axial clearance in the hearings of the final drive bevel pinion shaft:
a) ZIL-130 motor vehicle b) ZIL-131 motor vehicle





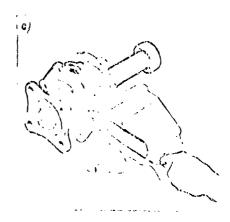


Plate 10-22. Checking tight ss of the bearings on the bevel pinion goer shaft:

- a) ZIL-120 b) ZIL-157K c) ZIL-131 1) dynamometer 2) flange
- 3) nut 4) cover 5) bearing recess 6) bevel pinion goar
 7) vise

Unscrew the hub bearing outer fastening nut with a special wrench, and remove the lock washer and seal. Unscrew the inner nut fastening the bearings and remove the wheel hub in assembly with the brake drum. Remove the wheel hub bearing and ring with its seal.

Removal and disassembly of the rear extereduction gear. Turn the rear axle so that the reduction gear is positioned vertically, pointing upward. Unscrew the bolts fastening the reduction gear housing to the rear axle frame rail. Install the bracket (Plate 10-26) on the flange of the final drive reduction gear and withdraw it with a hoist. The reduction gear may be disassembled on a stand or on a level working bench in the following order.

Removal and disasammbly of the bevel pinion gear shaft unit of the reduction gear. Unscrew the bolts fastening bearing carrier 8 (see Plate 10-1) and,

lightly tapping on the bearing carrier with a hammer, remove the pinion gear shaft 33 in assembly with the carrier. Remove the adjusting gaskets.

For disassembly, set carrier 4 (Plate 10-27) with the bevel pinion gear shaft in device 2 and fasten it with presses 3 and catch lock 1. which will keep the gear from turning. Unpin and unscrew the nut fastening the flange, remove the nut support washer and flange, tapping on them with a hammer. Unscrew the bolts fastening cover 4 (see Plate 10-1), and remove the cover with its gasket and support washer. If the seal is not in good condition, press it out of the cover and replace it with a new one.

For pressing the bevel pirion gear shaft out of the carrier, the unit in assembly should be set on supports of a press, and the shaft pressed out. If a press is not available, this same operation may be performed by striking the end of the pinion gear shaft on a wooden support and withdrawing the bevel pinion gear shaft together with the inner race of rear bearing 10, adjusting washers 9 and spacing bushing 34, from the carrier. Remove the front bearing from the carrier. Press the front bearing outer race from the carrier with a mandral (Plate 10-28). Press the rear bearing outer race out of the housing by the same method, but using a different mandral.

It is recommended that the rear bearing be removed from the pinion gear shall with a 20P-7984 GARO puller (Plate 10-29).

Removal and disassembly of the differential. Bend the blocking plates away from the bolt heads 26 (see Plate 10-1), unscrew the bolts fastening the step from both sides, and remove the locking plates and adjusting nut stops. Unpix the nuts fastening the bearing covers 18 of the differential box cups, unscrew these nuts with an angular socket whench, mark the housing supports and covers with a punch or paint, remove them. Also mark and remove adjusting nuts 25 and remove the differential together with its bearings. If necessary, unserow the study with a stud turner, having already removed the pin. If the study are not unscrewed, it is recommended that the bearing cover be set in piace and the nuts screwed on.

For disassembly, see the differential in a visu, grasping the ring gear by its rim. Unpin and unscrew the nuts of the bolts fastening the differential box cups and the ring gear. Mark the relative position of the differential box cups with a punch (machining of the recesses for the differential cross takes place with the differential in assembly, and during disassembly the relative positions of the cups must be maintained, not mixing them).

Remove the right cup and right half-shaft gear 17 with its support washer 19, remove the cross with the differential pinions and differential pinion support washers, and after this remove the left half-shaft gear with its support washer.

Remove ring gear 21 from the left differential box cup 23 with a copper mandrel and hammer.

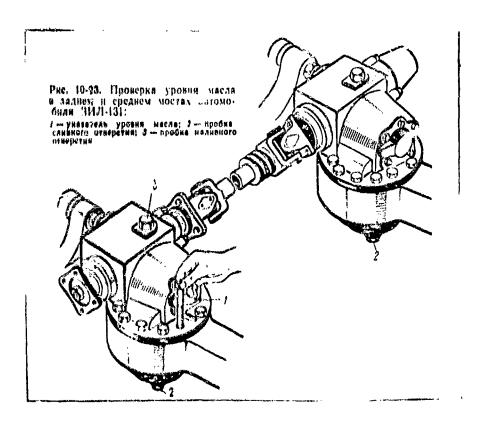
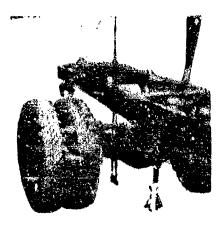
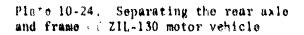


Plate 10-23. Checking the oil level in the middle and rear drive axles of a ZIL-131 motor vehicle:

1) oil level indicator 2) drain hole plug 3\ filler hole plug





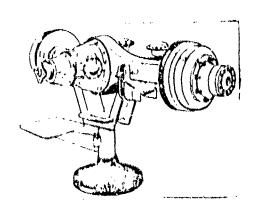


Plate 10-25. GARO model 689-00-00 stand for disassembling and assembling motor vehicle axles



Plate 10-26. Removal of the reduction gear from the rear axle housing of the ZIL-130 motor vehicle

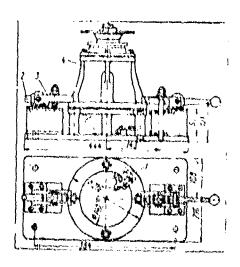


Plate 10-27. Device for disassembling and assembling the pinion shaft bearing carrier

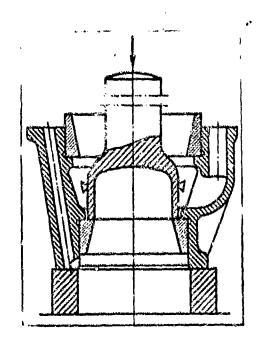


Plate 10-28. Pressing the outer bearing race from the bevel pinion gear carrier



Plate 10-29. Removal of the rear bearing from the bevel pinion gear shaft:

1) crosspiece 2) clamp 3) catch 4) tip 5) screw

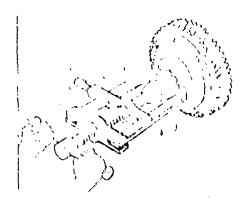
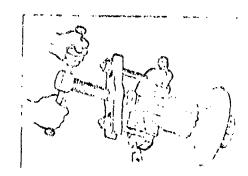


Plate 10-30. Removal of differential box bearings:
1 and 3) screws 2) crosspiece
4) clamp 5) catch 6) tip



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Plate 10-31. Pressing the bearing off the driving cylindrical gear shaft journal

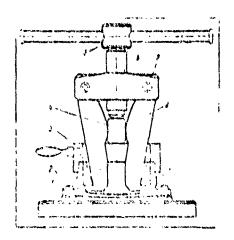


Plate 10-52. Pressing the cylindrical driving gear shaft bearing outer race from its cover:

- 1) support 2) pin 3) puller ring
- 4) bar 5) serew 6) crosspiece
- 7) pin 8) catch 9) bearing race

Plate 10-30 shows the bearing being pressed off the differential box cup journal with a model 2482 puller. In this operation, the nuller is installed so that the puller catches 5 more under the face of the inner range of the bearing.

Removal and disassembly of the cylindrical driving gar. Unscrew the bolts fastening bearing cover 15 (see Plate 10-1) with a box and wrench, and remove them in assembly with the adjusting gaskets 13 and with the bearing outer races. Before removal, it is recommended that the covers be marked, and during removal, lightly tap or them with a hammer. The packet of adjusting gaskets for one side should not be confused with the packet of gaskets for the other side, and it is recommended that they be fastened onto their covers by tying them with thin wire. Pull the shaft of the driving cylindrical gear 16 in assembly with the driven bevol gear 12 of the reduction gear housing. A model 2502 puller (Plate 10-31) is used for removal of the bearings with half circles which are installed on the rollers with supports on their faces.

The method of pressing the bearing outer race out of the cover with the model 2480 puller is shown in Plate 10-32.

If there are cracks or chips in the reduction gear housing or bearing covers, the housing and covers should be replaced. Cracks which do not penetrate through the housings can be welded up. Damage to threads is not allowed to cover more than two turns.

Oscillation of the half-shaft, measured at a distance of 80 mm from the flange, is not allowed to be greater than 1.0 mm.

The allowable oscillation of the half-shaft flange face must not exceed 0.2 mm. The allowable amount of half-shaft tube bend is 0.2 mm.

If there are chips, traces of twisting, bending, or cracks on the half-shafts, the shafts should be replaced.

The requirements for rear axle gears are similar to the requirements for gears in transfer cases (see Chapter 8).

If there is lossening in the rivets fastening the ring gear to the flange of the cylindrical driving gear shaft, the rivets should be replaced.

If either the driven or driving bevelod gears are replaced, it is necessary to also replace the gear paired with it.

Assembly of the rear axis. Before assembling the parts of the reduction ar, wash them in the degreesing solution, blow them off with compressed air, and check their usability. It is recommended that the assembly surface and sealing gaskets be coated with AK-20 or LB-11 lacquer. The bearings are lubricated with solid type grease.

Assembly of the bevel pinion gear shaft unit and adjustment of its bearings. Press the outer ring of front bearing 7 into the bevel pinion gear shaft bearing housing 8 (see Plate 10-1) with a sandrel until it rests against the fillet in the housing (interference is 0.010-0.068 mm). Turn the housing and press in the outer race of the rear shaft bearing 10 (interference is 0.009-0.059 mm). Mount the inner race of rear bearing 10, spacing bushing 34, adjusting washers 9, front bearing 7, and housing 8 on the shaft of bevel pinion gear 33. Set the sassembled bevel pinion gear shaft with a support under a press, and press on both bearings until they stop. The fit of the bearings must be for the rear bearing, an interference of 0.03-0.038 mm, and for the front bearing, a fit from clearance of 0.015 mm to interference of 0.16 mm.

Install support washer 5. Close the bevel pinion gear shaft housing with cover 4 and its gasket, having previously pressed seal 3 into the cover.

Install flange 2 with its deflector on the shaft splines and press it on. The flange fit on the splines takes place with a clearance of free 0.067 am to zero. Mount the washer for nut 1 and tighten flange 2 with the nut (the cover is fastened with bolts, and the nut is pinned only after adjusting bearing tightness).

The necessity for adjustment may also be determined by measuring the axial clearance with an indicator, which is installed at the pinion gear shaft face. If the axial clearance in the bearings exceed 0.05 mm, it is nacessary to adjust the bearings. Adjustment of the bearings takes place by means of select

ing the thickness of the two adjusting washers 9 from those washers put out by the factory in the following dimensions: 2.00-2.02; 2.05-2.07; 2.15-2.17; 2.25-2.27; 2.35-2.37; 2.45-2.47; 2.55-2.57; and 2.60-2.62 mm. The torque moment on the nut fastering the flames is 20-25 kg meters.

Checking the tightness of bearings on the bevel gear assembly is shown in Plate 10-22, a. The moment necessary for rotation of the pinion gear shaft in bearings lubricated with oil must be 0.1-0.35 kg meters, which corresponds to a force of 2.7-9.7 kg. If a smaller or larger moment is required to turn the pinion gear shaft, it is necessary to once again disassemble the unit and change the adjusting rashers 9 (see Plate 10-1), assemble the unit, and again check the shaft rotation moment.

While checking the moment of rotation of the pinton gear shaft, bearing cover 4 must be moved to the side of the flange so that the centering projection on the cover goes into the recess in bearing housing 8, and so that seed 3 does not cause resistance to shaft rotation.

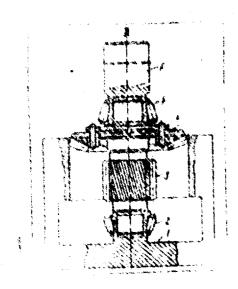
After finally adjusting the bearings, fasten cover 4 with holts and opring washers and flange nut 1. The flange fastening nut on the pinion gear shaft must be tightened until it is seated (torque moment is 20-25 kg meters) and pinned. While tightening the nut, turn the pinion gear shaft so that the bearing rollers are in the proper position between the conic surfaces of the bearing races.

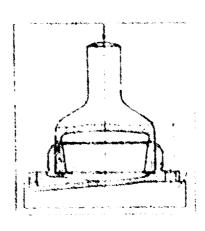
Associty of the driving cylindrical goar shaft. In a case where the driven boxel gear 13 is removed from the driving cylindrical goar shaft for replacement of the rivets, it is necessary to install the driven bevel on the shaft and rivet it to the shuft flange. It is recommended that before the driven basel goar is installed on the chaft it he heated to a temperature of 130-160°C, after which it is installed on the shaft flange, with the holes in the gear and flange aligned

After the driven basel goar couls, its fit on the ables what have an interference of U in 11.1146 and. When the driven bevel goar is replaced it in since hereafter to replace the heavy plates was paired of the fit.

The the shaft of the extendrical driving game I [Finte 19-33] vertically on the support of degree to present on the race of hearing I with a present install the same of hearing I with a present the same the present hearings with addition the shaft follow. Hearing fit on the shaft follow, hearing fit on the shaft follow of an interference of 688 as

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Pince 10-33. Pressing the bearing onto the cylindrical driving year shaft:

- 1) device 2 and 5) bearings
- 3) cylindrical driving gear
- 4) bevel pinion gear 6) mandrel

Plate 10-34. Pressing the outer race into the rocess in the cylindrical driving gear shaft bearing cover

Assembly of the differential. During assembly, the differential goars should be lubricated with TAp-15 of (GOST 8412-57). Set the right cup 1 (Plate 10-35) of the differential box on the plate, install bearing 2 on the sace of the cup journal, and press it on with mandrel 3. Interference between the bearing and the shaft journal must be within the limits of 0.010-0.048 mm. The sequence of assembly operations for the left differential cup is the same as the sequence for the right one.

Assemble the cross and differential pinions. The differential pinions must be installed on the cross journals with a clearance of 0.03-0.10 mm. The fit of the cross journals in the cups is accomplished with a clearance of 0.05 mm or an interference of 0.01 mm.

Install the left differential hox cup on support 12 (Plate 10-36) which has a hole into which the journal with bearing 15 must fit freely. Install the ring gear on the cup, lightly tapping on it with a copper hummer, and set the support washer and left half-shaft gear in the cup. Mount the four pinion gears on the journals of the cross with their supporting spherical washers. Lay the cross in assembly with the pinions on the differential box cup, lay the right half-shaft gear with its support washer on the differential pinions.

Plate 10-35. Pressing the bearing onto the differential box cup journal

Plate 10-36. Assembly of the differential:

1) ring gear 2) differential box cup

3) cross 4, 8, and 14) support washers 5) differential pinion

6) differential pinion bushing 7 and 15) bearings 9 and 13) half-shait gears 10) bolt 11) nut 12) support

install the right differential cup, aligning the cups in accordance with the marks placed on them with a punch during disassembly, insert the bolts into the holes in the ring gear cups, and screw the nuts onto the bolts by hand. Remove the differential from the support and install it in a vise. The nuts are tightened with an angular socket wrench, grasping the ring gear in a vise (nut tightening moment is 12-15 kg meters). Turning the nuts, align their grocves with the holes in the bolts and tie them off with safety wire.

Before tying off the nuts, rotation of the differential gears should be checked. Engagement of the differential gears and their rotation in the assembled differential must be free with rotation of the half-shaft gear by a mandrel installed in its splined hole.

Olearance between the half-shaft gear face and the support washer must be 0.50-1.20 mm on each side. The clearance is checked through the control holes formed in the differential cups.

Assembly of the reduction gear. During assembly of the reduction gear, the cylindrical gear shaft bearing tightness, ongagement between the bevel gear

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tooth, and differential bearing tightness are all adjusted simultaneously.

Installation of the cylindrical driving gear shaft assembly and adjustment of the tightness of its bearing. Install the shaft of the cylindrical driving gear 16 in assembly with the driven bevel gear 12 and inner bearing races into reduction gear housing 29 (see Flate 10-1). Lay the set of adjusting gaskets 13 on the flange of covers 15, install the covers in place in assembly with the bearing outer races pressed into them, and fasten the cover with bolts. Check the preliminary interference of the bearings. The set of adjusting gaskets put out by the factory consists of five pieces of dimensions: 1.0; 0.5; 0.2; 0.1; and 0.05 mm.

It is mardatory that gaskets 0.05 and 0.1 mm thick be placed beneath each cover in the reduction gear housing, with the remaining gaskets being placed according to necessity. During adjustment, the gaskets are removed from both sides in identical thickness and in equal number. After adjusting the bearing rightness, the twisting moment necessary to rotate the shaft in the bearings must be 0.1-1.35 kg meters, which is checked on a dynamometer by fastening it to the driven gear (Plate 10-37).

installation of the driven bevel gear smaft and adjustment of the bevel gear tooth engagement. Having finished adjustment of the cylindrical driving gear sheft bearing tightness, install the bevel pinion gear shaft in assembly in the reduction gear housing and fasten it with bolts and spring washers.

During installation of the bevel pinion gear shaft assembly, it is necessary to check the cooth engagement between the driving and driven bevel gears (on paint along the contact spot) and, if required, adjust the engagement and set the required clearance between the teeth. The position of the contact spot on the working side of the tooth of a new driven gear with an adjusted gear engagement must correspond to the spot of contact shown in Plate 10-38. A clearance between the teeth must be maintained within the limits of 0.15-0.40 mm for new gears and no greater than 0.5 mm for gears having already been in operation.

The clearance between the teeth is measured with a leaf gauge at the wide part of the tooth on no less than three or four driven gear teeth, located at appreximately equal angles around the circumference. The clearance may also be checked with an indicator, whose knife rests against the gear tooth (Plate 10-9). For normal setting of gear teeth engagement according to a point of contact, it is necessary to fasten the housing in assembly with the driven bevel gear shaft on the reduction gear housing, and place a thin layer of oil base paint on the working surfaces of several of the driven bevel gear teeth. After this, rotate the bevel pinion gear shaft is one direction and the other, braking the driven gear by hand. The character of gear engagement is determined according to the spots formed. The method of correcting the contact spot and the proper setting of gear engagement is shown in Table 10-2.

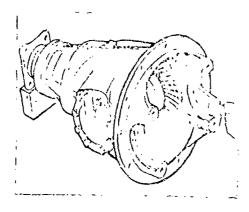


Plate 10-37. Checking tightness of bearings on driving cylindrical gear shaft

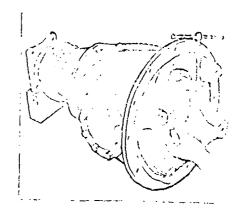


Plate 10-39. Checking axial clearance in bevel gear teeth engagement



Plate 10-38. Proper position of contact spot during assembly of final drive gears:

a) without load b) under load

If the position of the slots in not correct, the normal engagement should be attained by moving the driving and driven gears in an axial direction. Movement of the bevel pinion gear shaft is accomplished by changing the thickness of the set of adjusting gaskets installed between the flange of the ginion shaft carrier and the reduction gear housing. The set of adjusting gaskets put out by the factory consists of five pieces of dimensions: 1.0° 5; 0.2; 0.1; and 0.95 mm. Movement of the driven bevel gear is accomplished by moving gaskets from beneath the flanges of one cover of the reduction gear housing to beneath the flange of the other cover, without changing their total chickness, which does not alter the adjustment of the cylindrical gear shaft bearings.

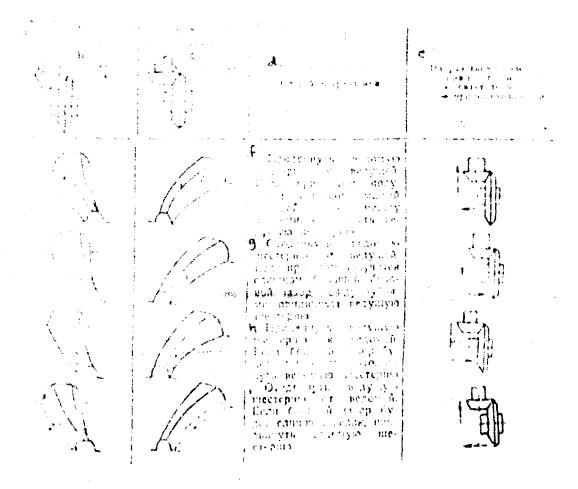


Table 10-2. Methods of correcting points of contact and propor adjustment of final drive gear engagement in two-axle motor vehicles

Key:

- a) Position of contact spots on driven gear teeth
- b) forward
- c) backward
- d) method of correction
- e) direction of gear movement: mandatory if necessary
- f) Move the driven gear to the driving one. If too small a lateral clearance between the teeth results from this, move the driving gear away.
- g) Move the driven gear away from the driving one. If too large a lateral clearance between the teeth results from this, move the driving gear closer.

- h) Move the driving gear toward the driven one. If the lateral clearance is too small, move the driven gear away.
- i) Move the driving gear away from the driven one. If the lateral clearance is too large, move the driven gear closer.

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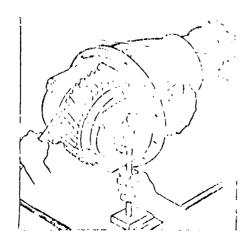
After finally adjusting the position of the driving and driven bevel goars, the torque moment necessary to rotate the cylindrical driving goar shaft in the bearings must remain unchanged within the limits of 0.1-0.35 kg meters.

After finally adjusting the positions of the driving and driven bevel gears, it is necessary to final tighten the bolts fastening the bevel pinion gear shaft housing. Tightening torque must be 6-8 kg meters.

Installation of the differential in the reduction gear housing and adjustment of its bearings. Install and fasten the differential in the reduction gear housing. In a case where the differential fastening stude have been unscrewed, it is necessary to screw them into the threaded holes in the reduction gear housing and pin them.

The differential bearings must be adjusted with a preliminary interference. For elimination of axial clearence, the adjusting nuts 25 (see Plate 10-1) are equally tightened en both sides, so that the toothed ring of the ring gear 21 is symmetrically located relative to the toothed ring of cylindrical driving gear 16. During adjustment of the bearings, the differential is retated several times to attain a normal distribution of the rollers in the bearing races.

To attain the proper preliminary interference in the differential bearings, the adjusting nuts are tightened on both sides by one slot from he position of zero axial clearance, and the groove in the nut is simultaneously placed beneath its lock. The absence of axial clearance is checked with an indicator, whose knife is installed on the rim of the ring gear (Plate 10-40). Recking the gear by hand (Plate 10-41), check clearance between the testh of the paired cylindrical gears with the indicator also, resting the indicator rod on a tooth of the ring gear. Clearance must be within the limits of 0.1-0.7 mm in new gears, and 0.1-1.0 mm for gears which have been in operation.



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Plate 10-40. Checking axial clearance in differential bearings

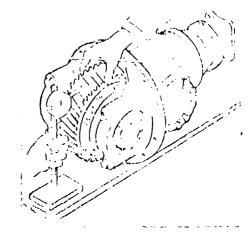


Plate 10-41. Checking clearence between the teeth of the cylindrical gear pair

Having finished adjusting the differential bearings, tighten covers 18 (see Plate 10-1) with their nuts (torque moment is 17-19 kg m. rs) and pin them. Install the stop with the lock washer on each adjusting nut 25, fasten the stops with bolts 26, and compress the lock washers.

Installation of the reduction gear in the rear axle housing. Screw the plugs into the filler and drain holes, and screw in the rear axle housing vent. Set the rear axle housing on a stand (see Plate 10-25) or on a special support.

Install the reduction gear assembly in the receptacle in the housing, having previously laid its gasket, coated with AK-20 lacquer, on the housing flange. Mount spring washers on the bolts, and fasten the reduction gear assembly with the bolts.

Installation of the brakes and wheel hubs on the rear axle. Install the brake bucking plate, spreader caus, adjusting levers, brake shoes, and chambers. Install the hubs and adjust the wheel bearings. For assembly and adjustment of the brakes, see Chapter 16. For assembly and installation of the hubs and adjustment of the wheel bearings, see Chapter 15.

Installation of the half-shafts. Insert the splined end of the half-shaft in the half-shaft tube. Align the splined ands of the half-shaft with the spline holes in the half-shaft gears in the differential, and insert them into the gears. Mount the half-shaft flanges on the wheel hub studs. Place conic spreader bushings and spring washers on the studs and, having screwed on the stud nuts by hand, tighten them with a weench until they are firm.

Installation of the rear axle on the motor vehicle. Before installing the rear axle on the motor vehicle, it is necessary to install the springs on the axle housing and fasten their U-bolts, install the wheels and fasten them on the lug studs.

Raise the rear part of the frame with the hoist mechanism, and roll the rear axle, in assembly with springs, beneath the frame (see Plate 10-24), install the front ends of the spring in their brackets and fasten them.

Install the rear ends of the springs in the brackets and fasten them. Release the frame onto the motor vehicle suspension, and remove the hoisting apparatus.

Connect the propellor shaft flange yoke to the flange of the rear axle reduction gear, and fasten it with bolts. Put lubrication in the rear axle.

The ZIL-157K motor vehicle.

Removal of the front drive axle from the motor vehicle. Park the motor vehicle on a level space, disconnect the front and rear ends of the front suspension springs from their brackets on the frame, disconnect and remove the shock absorbers, and disconnect the flexible hoses for the brake chamber and

contralized system of air pressure regulation in the tires. Disconnect the propellor shaft from the flange of the front axle pinion gear, having previously placed a stand or jack beneath the axle reduction gear.

Raise the frame with a hoist and roll the front axle from beneath the frame. Lower the frame, placing stands beneath it. Remove the wheels and springs.

Removal of the rear and middle drive axles from the motor vehicle. Disconnect the top torque rods from the brackets fastened onto the frame, the flexible lines for the brake chamber and centralized system for air pressure regulation in the tires, and the propollor shafts. Unscrew the puts fastening the suspension brackets to the frame brackets.

Raise the roar part of the frame and roll the rear axle carriage in assembly with its suspension and wheels from beneath it. Setting a stand beneath it, lower the frame.

Remove the whoels. Disconnect the balancing suspension from the drive axle rail brackets. Before disassembling the drive axles, it is necessary to drain the oil from them. Knock the dirt off the axles, wash them off with degreasing solution, and blow them off with compressed air.

It is possible to recove the middle and rear drive axies or one of them without removing the balancing suspension from the frame. For this, the rear part of the frame should be raised, the heads of the torque rods disconnected from the levers, and one or both axies rolled from beneath the frame. Having placed a stand beneath it, lower the frame.

Disassembly of the front axle. The front axle should be disassembled on a GARO model 689-00-00 stand (see Place 10-25). If no such stand is available, disassembly may be conducted on a bench.

It is recommended that the front axle be disassembled in the following sequence.

Removal of the half-shafts. Unscrew mits 47 (see Plate 16.3) fastening the splined half-shaft flange, and screw in the two puller bolts in the threaded help in splined flange 48. Having previously loosened the stop nuts 75, remove the flange. Remove the flange gasket and pull the deflector ring out of the groove in spindle 46. Unscrew the fitting from the air supply head. Unscrew the screws fastening hubcap 49 and remove it from the hub, lightly tapping on it with a hammer. Remove air supply head 44 from the spindle.

Unscrew stop not 50 with a special wrench and remove the lock washer. Unscrew nut 52 fastening the bearing and, lightly tapping with a hammer, remove the hub with the brake drum and outside bearing. Press the inside wheel hub bearing off the spindle (see Chapter 15 for disassembly of the wheel hub).

Remove the brake shoes, brake chambers, adjusting lever 33, bracket 35 and spreader cam 37, backing plate 58, and, unscrowing nut 59, remove spindle 45 (see Chapter 16 for brake disassembly).

Pull the inner half-shaft 68 in assembly with the ball joint and stub axle 61 from its jacket. For removal of the second inner half-shaft, the same operation should be conducted.

Disassembly of the ball support. For disconnecting the ball upport 70 from half-shaft jacket 71 of the housing and cover, it is necessary to unscrew nuts 69, remove the washers, and press the ball support journals out of the half-shaft jackets with the puller bolts, screwing the bolts into the two threaded holes on the flange of the ball support body with a wrench.

Remove the consistent grease from the body and wash it out with regreasing solution. Unscrew nuts 5 and 13 (see Plate 10-7), fastening the lower and upper body covers. Remove the washers and, lightly tapping with a hammer, remove conic bushings 12 and covers 7 and 14 from the stude. Remove the adjusting gaskets 9 and 16 and the support ring 6. Unscrew bolts 3 fastening seal 2, and remove it in assembly. Remove the rubber seal 4 from its slot in the body. Unscrew the stude from the body flanges.

Set the body with the ball support on a stand, and press the outer race of lower bearing 8 out with a mandrel. Press the inner race of bearing 8 from the bottom king pin of the ball support.

Turn the ball support 5 (Plate 10-42), directing the lower king pin 4 into slot 3, and remove the support from body 2 in assembly with the upper king pin bearing. Press the upper bearing off the king pin journal with a 20P-7968 puller, and a 20K-103-2 ring or other similar puller.

Removal and disassembly of the differential. Disconnect and remove the steering tie rod. Unscrew nuts 20 (see Plate 10-3), remove the washers and bolts fastening the housing and cover, and then, lightly tapping with a hammer, separate cover 21 from housing 18, remove gasket 19, and remove the differential in assembly with the ring gear. Press the outer races 5 (Plate 10-43) of the bearings from their recesses in the cover and 1 using, and press out the seals (Plate 10-44). Press the bearings off the differential box cup journals with a 20P-7968 pullir (Plate 10-45).

Fasten the differential in a vise and unpin and unscrew the bolts 2 (see Plate 10-4) fastening the differential box cups. Remove cup 4 together with the bolts, and remove the bolts. During removal of the cup, it is necessary to remove half-shaft gear 6 with support washer 3, remove cross 8 with the differential spindles 7 and support washers 11, and remove half-shaft gear 13 with support washer 12.

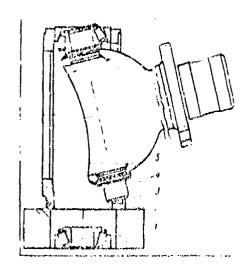


Plate 10-42. Method of separating the ball joint and body:
1) stand 2) body 3) suxiliary slot 4) king pin 5) ball support

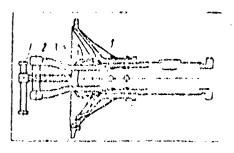


Plate 10-43. Pressing the differential bearing outer race from the cover recess:

1) handle 2) screw 3) grip 4) support bracket 5) bearing race

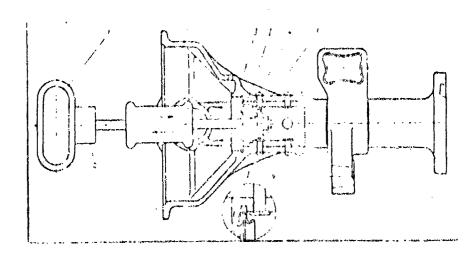
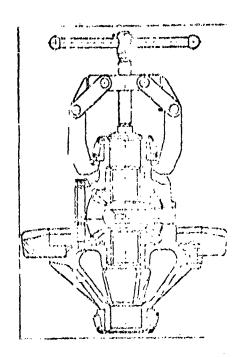
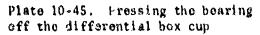


Plate 10 44. Pressing the seal out of the housing recess:
1) handle 2) movable weight 3) weight guide 4) seal
5) support plate 6) stop





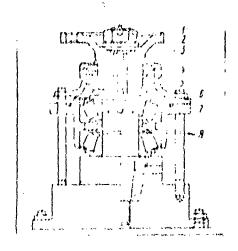


Plate 16-46. Installing the bearing carrier in assembly with the pinion goar shaft

Removal and disassembly of the bevel pinion gear shaft. For removal of the bearing carrier in assembly with the hevel pinion gear shaft, it is necessary to unscrew holts 30 (see Plate 10-3) and, using the puller bolts, remove the bearing carrier assembly and adjusting gaskets 6. Remove stop ring 15 (see Plate 10-5) and press bearing 14 off the journal.

Install the bearing carrier in assembly with the bevel pinion gear shaft in the device (Plate 10-46), fasten it, and conduct the disassembly. Umpin nut I fastening the flange, and unscrow it. Remove support washer 2 and flange 3, tapping on it with a hammer. If the flange fits tightly on the splines, it must be removed with a 20P-7968 puller. Release the housing from its fastening, remove cover 6 by pressing it out of its recess with the two puller bolts, remove packing ring 7 from its circular groove, and remove support washer 5. If necessary, press seal 4 out of its recess in the cover with a mandrel.

Sot the bearing carrier under a press, and press out the pinion shaft in assembly with the rear bearing. Remove the front bearing from the carrier, and remove the adjusting washers 8 from the shaft. Press the rear bearing off the shaft journal.

Press the outer bearing rane out of the carrier with a 20P-7968 puller (Plate 10-47) using a special 20K-101 fitting.

In ooth cases, the outer bearing races are pressed out only if they are worn or damaged, and it is necessary to replace the bearings.

Disassembly of the rear and middle drive exles. Remove the brake chambers, withdraw the half-shafts, unscrew the nuts fastening the housing to the cover, separate the cover from the housing, remove the gasket, and withdraw the differential in assembly with ring gear. Unscrew the pinion gear shaft bearing carrier bolts and, using the puller bolts, remove the bearing carrier assembly and the adjusting gaskets.

Disagrembly of the hevel pinion gear unit and differential is the same as disassembly on the front axle.

For disassembly of the balancing suspension, see Chapter 17. If there are cracks on axle parts, the parts hould be replaced.

Loosened rivers fastening the half-shaft jacket should be cut and new ones installed.

The beveled ring gear and pinion are paired, and this condition should be maintained.

If there is wear on the journals of the spindles, half-shafts, and ball supports above the *llowable dimensions, the worn out parts are replaced.

Requirements for goars and half-shafts of the ZIL-157K motor wehicle drive axles are similar to the requirements for the rear axle on two-axle motor vehicles.

Assembly of the drive axlo. Assembly of the bearing carrier with the pinion shaft. Press the outer bearing races into the carrier (interference, 0.025-0.075 mm). Press the rear hearing onto the pinion journal shaft until it rests against the face of the gear (interference, 0.018-0.047 mm).

Connect the pinion shaft with the bearing housing and mount the two adjusting washers on the shaft. Install the front bearing on the shaft. The bearing fits with a clearance of 0.008-0.35.

Install the pinion gear shaft in assembly with the carrier in a device (see Plate 10-36). Lay packing ring 7 in the circular slot, mount support washer 5, install cover 6, aligning the fixing pin of the housing with the hole in the cover, and fasten the shaft carrier with the cover in the device. Install flange 3 on the splines of the shaft, mount support washer 7 and, screwing on the nut, eighten it until it is firm. Tightening moment is 20-25 kg meters. Remove the bearing carrier from the shaft in assembly, fasten it in a vise, and check bearing tightness with a dynamometer. With properly tightened bearings, the pinion gear shaft must rotate due to the action of a someont of 6-14 kg cm, which corresponds to a force of 0.8-2.3 kg applied at the flange at one of its four holer. The method of checking is shown in Plate 10-22, b.

If the torque second is less or greater than that required, it is necessary to disassection the pinion housing, change the adjecting weater: 8 (Plate 10-46), assection it again, and check the second of goar shaft rotation in the bearings. The adjusting paskets are pursuit in the following thicknesses: 7.25, 7.30, 7.40, 7.50, 7.50, 7.70, 7.80; and 7.85 am.

After finishing sasembly and adjusting, press the bearing onto the journal of the tail part of the gear (interference 6.040-0.015 mm) and favour the rearing with a stop ring (the bearing outer race is installed in the housing with a clearance of 0.038 mm or an interference of 0.005 mm).

After assembling and adjusting the bearing carrier assembly, it is teconmended that it be spun for a period of one minute at a share speed of 200 nom. After this, shaft rotation in the bearings is again checked with a dynamometer. It must rotate under action of a moment of 6-14 kg cm.

Assembly of the differential. Before assembly, the parts are when with a dry soft wieth. During assembly, the assembled part. Should be conted with transmission lubricant.

Fress the bearings onto the differential box cup journals (see Plate 10-35).

Install support washer 12 and half-shaft geer 13 in the loft cup 10 (452 Plate 10-4).

Mount the support washers and differential pinions on the cross, and install the great assembly in the left differential cup.

Mount the support washer on the second half-shaft gear, set the gear in the right cup, and install the unit on the left cup, aligning the hole with the bolts in both cups. Serew the bolts in and tighten them. Torque moment is 9.0-11 kg meters.

Check the proper assembly of the differencial. Insert a leaf gauge 0.8 mm thick between the supporting surface of half-shaft gear 13 and support washer 12. In this operation, the gears must be rivoted.

The half-shaft geggs and differential pintons in an assembled differential must retate easily. Tight setation of the gears or the binding is not allowed. After checking the differential, the off bolts 2 with safety wire 15. The ends of the wire as bone incu a lock as shown in Flate 10-4.

Tinstall one of emblod differential on the supports of a device by its bearings (Pinto 10-40) and, curving it by bomb, check escillation along the lever face of the ring goar. Allowable escillation is no greater than 0.16 mm.

Ass: Diy of the ball support (left and right). If the support ring 17 is nown (so. Plata 10-7), it must be replaced. The ring fits with an interference of 0.05 1.21 mm. Lay the ball support with the king pins in assembly in the nody of the turning spindle. Set the ball support in assembly with the body in device 1 (Plate 10-49), guiding the ... ng oir onto support 2.



ulate 10-47. Pressing the pinion shaft bearing outer race from the carrier:

- 1) screw 2) link 3) grip 4) tip
- 5) 2014-101 puller fitting 65 body

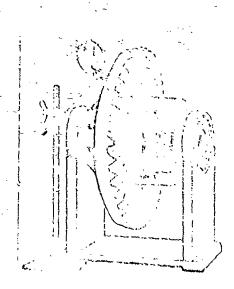


Plate 16-48. Checking differential ring goar oscillation



Plate 10-49. Pressing bearings ento the ball support king pins: 1) device 2) support 3) body 4) ball support 5) hearing 6) mandrel

Set bearing 5 on the face of the king pin, pippe undrel 6 on the bearing and press it onto the kingpin. Itstall the outer race and least it into the recess in the turning spizale bear.

Turn the ball support in assembly with the body in the device, press the other hearing onto the king pin, and pross the outer hing investes recess in the body.

The bearings fit on the king pin journals with an interference of 0.002-9.7927 ms, and the outer rages fit into their regards in the Sade with a clearance of From 0.065 mm to ture.

Screw in the cover fastening study with a stud turner, install the support ring 5 (see Plate 16-7), the adjusting garkets 9 and 15 in the lower bearing recess, requit covers 7 and 14 on the study, mount the split conic bushings 12 on the study, mount spring vashers, and serve on the nuts, hightening them until they are firm. The hightening messest of the nuts is 12-15 kg meters. Forting tightening of the cover hurs, it is necessary to turn the housing so that the bearing rollers are distributed bround the races properly.

Thick bearing tightness with a dynamiseter (Plane 10-50, — f the force applied to the Opening in the turning spindle necessary for its roration is within the limite of 2.25-2.75 kg, the amount for rotation of the spindle is 0.45-0.55 kg meters, and bearing adjustment is not required in this case. If the required force moves outside the indicated limits, it is necessary to change the thickness of the set of gaskets 9 and 16 (sed Place 10-7) in a larger of smaller direction, so that the thickness of the gashet set pack between the upper and lower covers must not differ by more than one 0.05 mm thick gasket in the selected gasket packet, there must be thicknesses of: 0.1, 0.2, 0.5, and 0.05 mm. In each packet must be two thin ones, 0.05 mm thick, and one thick one, 0.1 mm thick.

Having finished adjustment of bearing tightness, place the rubber packing 4 in its slot, set seal 2 on the ball support, and fasten it with bolts 3 and spring washers.

Screw the adjusting support screw into the hole in the ball support body and adjust the angle of turn, which must be 28-29°, with it, so that the bolt head rests against the ball support. Sold—the support bolt to the body with brass solder. Assemble and adjust the right ball support of the front drive axle in the same manner.

Installation of the ball support. Set the axle housing and the half-shaft jacket so that the half-shaft jacket is pointed upward, and screw the stude (in case they are replaced) into the holes in the flunge to half their depth.

Install the turning spindle by the ball support bearing surface into the hole in the half-shaft jacket so that the turning arm of the ball support body is directed toward the pinion goar flange and the ball support flange holes are aligned with the study in the half-shaft jacket flange.

Fress the bearing surfaces of the ball support into the bale in the halfsheet jacket until the ball support slange to seated. The bearing surface fit
as monaplithed from a clearynce of 0.249 mm to zero interference. Inventy
apring slaners on the stude, sores on the nuts, and tighten them until they
are seated. Her torque account to 12-15 kg metars.

Content the right ball support to the half-shaft jacket in the seme manner as the late one. If there is wear in the ring gets support plate, it should be replaced with a new one. Thickness of the plate must be 5.38-5.50 ms.

The epindie. If there is weer on the support ring and bushings, they must be restained with new pace. The ring should be fix with an interference of 0.03-0.21-m, and the bushing should be fit with an interference of 0.69-0.21 m.

Assembly of the front sale half-shaft boll joint. Parts of the ball joint are shown in Flate 10-51, w. For assembly, fasten the inner half-shaft into a device or in a metal working viae, and connect it with the stub axle. Select the balls beforehand, using a vachnological ball with a flat surface piaced in the center apheto of the assembled parts. Then, sequentially, one driving ball at a time, install the balls in any of the four recesses (Flate 10-51, b). The stub axle must be easily manually degring this operation. The last locking criving ball is installed in the recess only after coincidence of its formed surface with the flat on the tacknological ball.

Having assembled the stop sale with the inner half-shaft, wheek the operation of the ball joint with a dynamometer, terming the stop sale by an angle of 10-15° in three directions in the plane I-1, in the plane III. and in the plane III-III (Flate 10-51, b).



Plate 10-50. Checking the fightness of the turning spindle king pin bearings



Plate 10-51. Assembly of the front axle half-sheft bail joint:

a) buil joint parts b) installation of the balls in joint recesses c) diagram for checking the assembled joint

1) stub axle 2) running paths of the balls 3) inner half-shaft 4) center ball spherical recess 5) center ball 6) driving bails 7) dynamometer

The moment necessary for turning the stub sxls by an angle of 10-15° must be within the limits of 2.0-8.5 kg meters.

The difference between the maximum values of the turning moment in the three planes must be no greater than 1.5 kg meters. After turning the stub axis by an angle greater than 10-15°, a decrease in the turning moment to zero is allowed. While the stub axis is being turned, there must be no binding of the balls.

The ascembled half-shafts should be checked on a stand at 30 rpm with a load of 80 kg meters, and with the stub exte being turned relative to the inner half-shaft by an angle of no less than 30° to one side and to the other. During this operation, there must be no catching between the driving balls and the center ball, or catching between the two shafts.

If the requirements listed above are not satisfactorily performed, the joint must be disassembled, and the driving (lateral) balls of the joint must be replaced with ones of larger dimensions, if the moment required for turning the stub axle is less than that indicated, or must be replaced with case of samiler dimensions if the moment required is greater than that indicated. The balls range in dismeter from 34.83-35.010 mm, and are divided into nine groups, differing by 0.02 mm in dimensions.

Having finished selection of the balls, remove the technological ball with the flat from the central recess, and replace it with the central ball (central ball diameter is 31.50-32.00 mm), and assemble the joint with the newly selected driving balls.

In installation of the fourth power ball, draw out and turn the stub axle to an angle which allows insertion of the fourth driving ball. Release the inner half-shaft, insert the stub axle in the vise and, with a smooth force applied by hand to the end of the inner half-shaft, turn it into the straight position.

If assembly is accomplished using drive balls from various groups according to diameter, these drive balls must again be placed in their previous recesses during exchange of the center ball.

If necessary, repeat the check on the operation of the assembled half-shaft ball joint. When the stub axle is turned by hand, there must not be any noticeable binding of the balls in the joint.

See Chapter 15 for assembly of the wheel hub and Chapter 16 for installation of the brake drum.

Overall assembly of the frint drive axle. It is recommended that the axle be assembled on a GARO model 689-00-00 stand (see Plate 10-25). In case no such stand is available, the axle may be assembled on a bench.

Install the axle housing and scrow the two auxiliary pins into the holes in the flange, mount adjusting gaskets of 1.6 mm overall thickness on the pins. In this operation, there must be no less than two gaskets 0.2 mm thick, and no less than two gaskets 0.1 mm thick in the gasket set.

The gaskets must not have nicks or creases from shalp bending.

Installation of the pinion gear shaft. Install the pinion gear shaft in assembly with its bearing carrier in the front axle housing so that the p n in the pinion shaft bearing housing goes into the hole in the axle housing flange.

Screw the auxiliary stude out of the holes in the flange. Placing spring washers beneath the bolt heads, screw the bolts fastening the pinion shaft bearing housing to the holes in the flange. (Torque moment is 3.5-5.0 kg meters.) Installation of the differential. Coat the working edges of the rubber cups in the half-shaft jackets with consistent type grease, and install

the differential assembly in the front axle housing, checking to see that the paired pinion and ring gear have the same unit serial number.

Smear the assembly surface of the housing cover with grease, and install the gasket, aligning the holes in the gasket and the holes in the cover. Install and connect the cover to the housing so that the areas for fastening the front springs are located in the same plane, and the holes in the cover and axle housing are aligned. Install the bolts, whose heads must be located on the side of the housing, install spring washers, screw on the nuts, and tighten them with a wrench. The moment for nut tightening must be 5.0-6.5 kg. The two bolts screwed into the housing body are pinned with safety wire.

Check the installation and assembly of the axle mechanism by rotating the pinion gear manually by the shuft flange. There must be no catching of the gears or differential box on the housing and support plate when the pinion gear is turned.

Adjustment of the clearances and engagment of new final drive bevel goars. With the proper selection of adjusting gaskets installed with the pinion goar housing flange, the lateral clearance between the teeth must be 0.1-0.5 mm at the wide part of the tooth, which will correspond to a pinion goar shaft frange rotation of 0.25-1.00 mm with the installation of an indicator rod on the flange along the diameter where the boit hole is located. The method of checking the clearance with an indicator is shown in Plate 10-52.

In a case where the clearance between the gear teeth does not correspond to the value 0.1-0.5 mm, it is necessary to perform adjustment by means of changing the thickness of the gasket set installed beneath the bearing carrier flange of the pinion gear shaft. In this operation, one thin gasket, 0.1 mm or 0.2 mm, should first be installed or removed. After each decrease or increase in the adjusting gasket set thickness, the bearing carrier should be fastened on and the clearance between the gear teeth checked by the method shown in Plate 10-52.

Having ensured that the clearance between the bevel goar teeth corresponds to that established, it is still necessary to check the engagement of the gear teeth on their spot of contact, which must be located on the working convex side of the touch profile (Table 10-3).

For checking the position of the contact spot, it is necessary to discurnect the color, withdraw the pinion gear shaft assembly from the housing, apply a thin layer of paint on the working part of the teeth, and again install the assembly in place. Turn the pinion shaft by several revolutions, rotating the flange by hand, after which the pinion gear shaft is removed and the position of the contact spot checked on the teeth. The spot of contact on the teeth of a new ring gear must have a length of 28-35 mm and he removed from the narrow end of the tooth by 3-6 mm, from the wide end of the tooth by no less than 5 mm, and from the top of the tooth by no less than 1 mm.

The position and size of the spot is adjusted by maying the engagement of the gears, changing the thickness of the set of adjusting gaskets beneath the flange of the pinion gear bearing carrier.

In order to cove the pinion gear away from the ring gear, it is necessary to increase the thickness of the gasket set, adding one thin gasket, 0.1 mm in thickness, each time and, conversely, so as to bring the pinion gear nearer to the ring gear, it is necessary to remove the same amount of thickness. After each change in the gasket set thickness, the pinion gear shaft bearing carrier is again installed in place, and the amount and position of the spots of contact are checked by turning the gears.

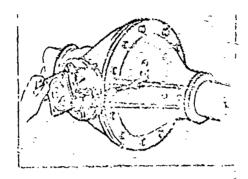


Plate 10-52. Method of checking the clearance between the drive axis final drive goar teeth of a ZIL-157K motor vehicle

The axial clearance (stack) of the ring gour depends on the fit of the differential bearings, whose preliminary fit was provided during assembly of the precision dimension parts and installation of the 0.15-0.25 mm thick gasket on the assembly surface between the housing and the drive axia cover.

The fit of the differential bearings in an assembled new drive axis must be within the limits of from interference of 0.5 mm to clearance of 0.09 mm. The axial clearance 0.09 mm is also the maxisum axial slack in a ring gear in assembly with the differential. The axial clearance of the ring gear shaft may be measured with a leaf gauge by inserting it between the ring of the ring gear and the copper plate riveted to the axis housing cover. This slack may be measured with an indicator, setting its knife against the toothed ring of the ring gear. While measuring this clack, the pinion gear shaft in assembly with the bearing carrier must be removed from the drive axis housing.

During the process of operation of the drive axle, the axial clearance in the ring gear is allowed to increase to 0.2 mm. In connection with the fact the that the differential bearings are not adjusted, the axial clearance in the ring gear may be decreased by replacing the gasket on the assembly surface between the housing and the cover with a thinner one, or by replacing the worn out differential bearings with mer ones.

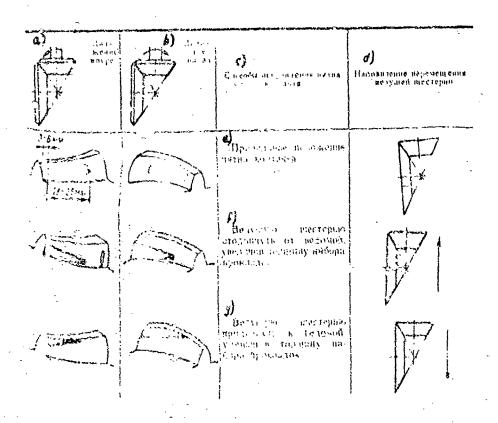


Table 10-3. Position of spots of contact for assembly of the final drive years in three-axle motor vehicles

Key: a) movement forward

- b) movement backward :
- c) method of correcting the spot of contact
- d) direction of pinion gear movement
- e) Correct position of the spot of contact
- f) Move the pinion goar away from the ring goar, increasing the thickness of the gasket set
- g) Move the pinion goar closer to the rin, year, decreasing the thickness of the gasket set

Installation of the half-shafts. Screw the spindle fastening stude into the ball support body (if they were unscrowed).

Install the stub axis and inner half-shaft assembly into the half-shaft jacket of the wais, having previously applied type AM grease (Universal GOST 5730-5) in the half-shaft bull joints and the space in the body.

Installation of the spindles, brake units, wheel hubs, and air supply heads. Install the spindles in assembly with the ball joint stub axles, install the backing plate assembly on its studs, mount the ring with its seal in assembly on the stud after servicing the seal with liquid oil. Install the return spring hooks on the two studs, mount the spring washers on the studs, screw nuts onto them, and tighten them with a wrench. (To eque moment is 3.6-4.8 kg meters.)

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Install the spreader cams, adjusting levers, brake shoes, and brake chambers. Install the wheel hub and adjust the wheel beatings. Install the air supply head and hubcap. See Chapter 16 for assembly and adjustment of the brakes, and Chapter 15 for installation of the wheel hubs and adjustment of the bearings.

Installation of the half-shaft flange. Install the gaskets and half-shaft flange on the hubbap stude, install spring washers on the stude, screw nuts onto them and tighten them (tightening moment is 3.5-5.0 kg meters).

Scrow the puller bolts into the threaded holes in the half-shaft flange, having previously mounted stop nuts on the bolts, and tighten the bolts and stop nuts until they are seated.

Assembly of the components and overall assembly of the rear and middle drive axles are similar to assembly of the front axle, with the exception of the ball support and half-shafts. Therefore, during assembly and adjustment of the rear and middle drive axles, it is necessary to be guided by the information presented for the front axle.

Testing of drive axles. The assembled drive exles must be serviced and checked on the stand or during a run.

While being checked on a stand, the pinion gear shaft must have a rotation speed of 1000 xpm. Checking must take place with reversing and braking for a period of 7-10 minutes.

The following are not permissible: sharp noises of the final drive gears, and knocks and sharp noises from the differential with one brake drum being braked; catching of the retating parts on the stationary ones (for instance, catching of the ring gear and differential cups on the housing and axle cover, catching of the brake drum on the backing plate and the brake shoes, catching of the half-shaft ball joints on the ball support of the rotating spindle, etc.); heating in the places where the pinion goar shaft bearings and differential bearings are located in the housing and housing cover, and also in the places where the wheel hub bearings are installed; heating of the brake drum and ball supports (checking is done with touching by hand); oil leaks through the seals and connections; catching of the ball joints either with the turning spindles in the straight position or in the extreme angles of right and left turn.

Installation of the drive exles in the motor vehicle. Raise the front part of the motor vehicle frame with the hoist mechanism and roll the front axle beneath the frame. Install the spring ends in their rubber cushions, bring them into the brackets, close them with their cups, and tighten the bolts.

Lower the motor vehicle frame. Raise the rear portion of the motor vehicle frame, roll the paired middle and rear axles underneath the frame and lower the frame onto the suspansion pads, guiding the stude into the holes in the pad flanges.

Screw nuts onto the stude and eighten them with a wrench until they are seated. Connect the upper torque rod to the bracket on the frame.

Connect the flexible hoses to the brake chambers, to the air supply unit tee, and to the spindle flanges. Connect the propellor shafts to the flanges of the spindle gear shafts of the front, middle, rear axles, and to the intermediate propellor shaft support. Lower the motor vehicle frame.

The 2IL-131 motor vehicle

Removal of the front, middle, and rear axles from the ZIL-131 motor vehicle is similar to the removal of the drive axles from a ZIL-157K motor vehicle.

Disassembly of the front drive axle. Flate 10-11 shows the front drive axle. Disassembly of the front axle should take place on a GARO model 689-00-00 stand (see Plate 10-25). If such a stand is not available, disassembly may take place on a bench. The recommended procedure for disassembling the front axle is as follows.

Removal of the half-shaft. Remove valves 5 (Plaze 16-11). Unscrew the nuts fastening the splined flange 7 of the half-shaft and remove it by the puller holts, screwing them into the holes in the flange. Remove the gasket.

Unacrew the stop nut 6 with a special wrench, and remove the lock washer 8. Unscrow nut 3 fastening the hub bearings and, lightly tapping on the hub 1 with a hammer, remove it with the brake drum and outer bearings. So Chapter 15 for disassembly of the wheel hub. Remove the brake adjusting levers, bracket 16, and spreader came. Unserew fixing 13 with the hose from air supply head 27. Remove the bruke chambers and brake machanism. See Chapter 16 for brake disassembly. Remove spindle 2, for which the nut fastening the spindle to the boay should be unscrewed, screw M12 dimension bolts into the threaded holes in the Spandle flage, and disconnect the spindle from the body with them. The spindle assembly is shown in Plate 10-20. The spindle must be removed very carefully, attempting not to damage the air supply head seals. If necessary, ramove the outer race with the rollers of wheel hub bearing 11 from the spindle with a puller (see Plate 10-11). For removal of the air supply head 3 (see Plate 10-20), it is necessary to unscret the bolts and remove stop ring 5 of the spindle, and then remove the head. Remove the innor half-shafts 19 in assembly with the stub axis (see Plate 10-11) from the axis rail. The halfshaft assembly is shown in Plate 10-18. For removal of the second inner half-shaft, the same operation should be performed.

Removal and disassembly of the reduction gear. Disconnect and remove the steering tie red. Turn the front axle so that the supporting flange of the reduction gear is in the horizontal position, and the bev-1 pinion gear shaft flange is directed apward. Unserew the holts fastening the reduction gear to the front axle housing. Besides the exterior bolts, the reduction gear is fastened to she axle housing with two more bolts located inside the reduction gear carrier. In order to unserew these bolts, it is necessary to remove cover 24 (Plate 10-11). Having unserewed the bolts, again fasten the cover on the reduction gear carrier. Install a bracket on the final drive reduction gear flange, and remove the reduction gear from the front axle housing with a hoist. The method of removing the reduction gear is shown in Plate 10-53. Carefully remove the sealing gasket from the housing. Disassembly of the reduction gear takes place on a stand or on a bench.

Removal and disassembly of the bevel pinion goar shaft. Unscrew bolts 16 (Plate 10-14) fastening the cover and pinion gear shaft bearing carrier to the reduction gear housing. Remove the shaft in assembly with pinion gear 24, carrier 21, and bearings 22, from the reduction gear housing with M12 X 1.75 bolts, which are screwed into the threaded holes in the flange of carrier 21. Remove the adjusting gaskets 15.

For disassembly of the bovel pinion gear shaft, fasten it in a metal working vise. Remove stop ring 1 (see Plate 10-15) of the front bearing of the bevel pinion gear shaft with a screwdriver and hammer. Remove front bearing 2 with a puller. Unpin nuts 11 fastening flangs 9. Then, preventing the flange from turning with a bar, unscrew the nut fastening the flange. Remove support washer 12 and the flange, tapping on it with a barmer. If the flange fits tightly, use a 20P-7968 puller. Remove cover 8 with its seed, packing gasket, and supporting oil-deflecting washer 13. In case the seal in cover 8 is damaged, it may be pressed out of the body with a hammer and mundrel.

For removal of shaft 5, it is necessary to install the pinion gear shaft in assembly on the support of a press, and press out the shaft as shown in Plate 10-54. Set carrier 6 (Plate 10-15) on its flange on a support, as shown in Plate 10-55, and with a mandrel and hammer (or press), press the bevel pinion gear shaft together with the inner races of the front tapered bearing 5 (see Plate 10-15) out of carrier 6. Remove the inner race in assembly with the rollers of the rear tapered bearing. Remove adjusting washers 7. Press the inner race with the rollers of the front tapered bearing off the bevel pinion gear shaft. Press the outer races of the bearings out of the carrier with a 20P-7968 puller, using a 20K-101 fitting (Plate 10-56). The outer races of the pinion gear bearings are pressed out of the carrier only in the presence of wear above the allowable amount, or if the races are dainged.

Removal and disassembly of the differential. Bend the locking plate: away from the heads of bolts 2 (see Plate 10-14) fastering stop 3, unscrew the bolts and remove the locking plates and adjusting nut stops.

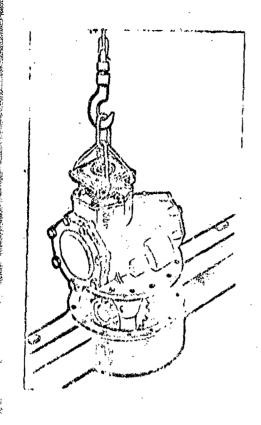


Plate 17-53. Removal of the reduction gear from the front axle rail

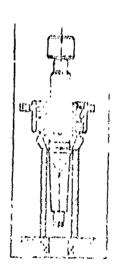


Plate 10-54. Prossing the shaft out of the bevel pinion goar

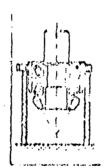


Plate 10-55. Pressing the bevel pinion goar out of the bearing carrier

Unpin and unscrew nuts 34 Pastening the covers 33 of the differential box cup bearings with an angular socket wrench, mark the covers 33 and remove them, mark and remove both adjusting nuts 4, and remove the differential together with its bearings. If necessary, unscrew the stude with a stud turner, having previously pulled out the pins. If the study remain in place, it is recommended that bearing covers 33 be installed in place and have their nurs eightened. If necessary, press the bearings out of the differential box cups, without disassumbling the differential. The method of pressing the bearings out with a 20P-7968 buller, using a 20K-992 fitting and a 20K-104-2 ring is shown in Plate 10-57.

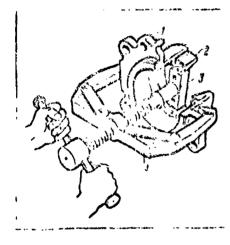


Plate 10-56. Pressing the outer bearing races of the spindle pinion gear shaft out of the carrier with a 20P-7968 pullor: 1) bearing carrier 2) bearing outer

race 3) puller fitting 4) puller

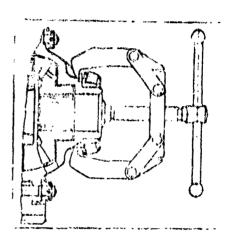


Plate 10-57. Removal of beering from differential cup

For disassembly, the differential should be set in a vise, clamped by the sim of the ring gear. Unpin and unscrew the nuts from the bolts fustening the differential box cups and the ring gear. Mark the relative positions of the cups with a punch, since the recessor for the differential cross in the differential box are machined with the unit in assembly. During disassembly, the unity of the differential cups should be maintained. Romove any cup 2 (see Plate 10-17) of the differential together with one of the half-shaft gears 7 and support washer 6. Remove cross 3 with differential pinions 5 and differential pinion support washers 4. Remove the half-shaft gear with its support washer from the other differential cup. Remove the ring gear I from the differential cup with a copper mandrel and hazzer.

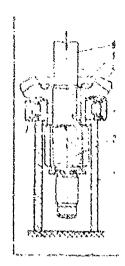


Plate 10-58. Freezing the cylindrical driving gear off the driven bevel gear:
1) support 2) cylindrical driving gear 3) bearing 4) driven bevel gear 5) toy
6) mandrel 7' spacing ring

Removal and disassembly of the cylindrical driving year shaft. Unscrew the bolts fastening cover 7 (see Plate 10-14) and recess 10 of the double tapered bearing for the driving cylindrical goar shaft. Remove the ever and scaling gashet. Black the shaft of the cylindrical driving gear 1 to prevent it from rotating. Unscrew nut 9 tensioning the inner race of the double tapered bearing 8. Remove the support washer, unscrew the bolts, and remove cover 27 with its scaling gasket. Using a manded and hammer, press the shaft in assembly with the driving cylindrical gear 14, the driven conic gear 45, bearing 26, and the inner race of double bearing 8 out of the recess 10 and out of the carrier 6 (from the side of the cylindrical gear).

Puti the other inner race of bearing 8 and adjusting ring 13 from recess 10. Mark the inner races of bearing 8 and the adjusting ring 13 in the positions that they were in during assembly. Press the remaining inner race with the rollers of double bearing 8 from the driving cylindrical gear shaft.

For removal of the driven bevel gear from the driving cylindrical goar shaft, it is necessary to let this unit on support 1 (Plate 10-58), and press the shalt of driving cylindrical year 2 from the receptacle in driven bevel gear 4. Drive out the key 5. Press off the cylindrical roller bearing 3 and spacing ring 7 with the driven bevel gear 4.

Nitidan the recess for the double tapered bearing from the reduction gear housing with MIR X 1.75 puller bolts. Remove the adjusting gaskets and press the euror race 3 (Plate 10-59) of the roller bearing out with mandrel 4. During this operation, support 1 must be placed beneath the receptable.

leaders and disassembly of the ball support. To separate the ball support 20 (see Plate 10-11) from front axis housing 25, it is necessary to unsersy the nuts, remove the washers, and press the fitting band of the ball support out of the bousing with puller bolts, which are screwed into the threaden heles in the flange of the ball support.

If the half-shaft soal is not in proper condition, it must be pressed out of the half support with a 209-7968 puller (Place 10-60) together with the seal ring. Remove the consistent greate from the turning spindle body, and wash the body with degreasing solution. Unscrew nuts 9 (see Plate 10-19) fustoning the cover with the rotating spindle lever, and nuts 19 on lower cover 2 of the king pin bearing. Remove the washers, and, lightly tapping with a hammer, remove the conic bushings 6 from the stude, and then remove the cover with the turning spindle lever and lever king pin bearing cover.

Remove the adjusting gaskers 5 and, unscrawing the belts fastening the seal, remove packing ring 11 tegether with seal 12 in assembly. Remove the rubber play 17 from the slot in turning spindle body 4. Unscrew the stude from the flanges of the turning spindle body. Set the turning spindle body with the ball support on a support and press out the bettom bearing outer race with a mandrel. Press the inner race of the bearing off the bottom king pin of the ball support.

To separate the ball support from the turning spindle body, it is necessary to turn the ball support, directing the lower king pin into the slot, and pull the ball support out of the body together with the inner race of the upper king pin bearing (see Plate 10-42). Press the inner race of the upper bearing on the king pin journal with a 20P-7968 puller and 20K-105-2 ring, or with another similar puller. The outer race of the bearing is removed from the rotating spindle body with a hammer and mandrel.

Disassembly of the rear and middle drive axies. Remove the brake chambers, pull out the half-shafts, remove the wheel hubs and brake mechanism, remove the spindles, and withdraw the reduction gears. Disassembly and removal of the parts and components mentioned above are similar to disassembly of the front drive axie, with the exception of the disassembly of the reduction gear. Removal and disassembly of the differential and driving cylindrical gear shaft is identical in all reduction gears of the three drive axies. Reduction; ears differ only in construction of the bevel pinion gear shafts. In order to remove the bevel pinion gear shaft of the rear axie reduction gear, it is necessary to lock the splined flange or ring goar, and unpinning the nut, unscrew it and remove the washer and flange. If necessary, use a puller.

Unscrew the bolts fastening the rear bearing cover of the bevel pinion gear. Remove the cover with its sealing gasket. Using the puller bolts screwed into the bearing flange, press the cup in assembly with the shaft and gear out of the reduction gear body. Further disassembly is similar to disassembly of the bevel pinion gear shaft of the front axic. Removal and disassembly of the bevel pinion gear of the middle axic reduction gear is the same as that for the rear axic.

If there are cracks on axle parts, the parts should be replaced. Damaged threads on the spindle and other parts of the axles are not allowed to cover more than two turns.

If the half-shaft journals, ball supports, and journals of the spindles for the sezis are worn above the allowable dimensions, the worn-cut parts are replaced. If the journals of the spindles, shafts, and reduction gears for the bearings are worn more than the allowable dimensions, the worn-out journals may be renewed. If there are breaks, twisting, or bends in the half-shafts, the shafts should be replaced. Allowable oscillation of the half-shaft at the half-shaft seal and air supply head seal is no greater than 0.1 mm. Oscillation of the flange of a new half-shaft is allowed to be no greater than 0.8 mm, and allowable oscillation of the flange without repair is no greater than 0.15 mm. The driving and driven conic gears of the reduction gear are paired according to contact spot, noise, and lateral clearance. If either cma of the paired gears is repaired, the gears should not be used except with each other. Ouring replacement, it is necessary that both gears be replaced together.

Assembly of the front axle. Before assembling the front drive axle, the parts must be washed in degreasing solution, blown off with compressed air, and checked in accordance with their technical requirements.

During assembly of axles, it is necessary to ensure the tightness of components needed for the motor vehicle to ford streams. All connecting flanges and scaling gaskets must be coated with scaling pasts (VTU MKnT 3336-62) during assembly.

Before their installation, steel adjusing gaskets must be washed and coated with spindle oil (GOST 1642-50).

Thin adjusting gaskets must be installed on both sides of the gasket set.

The control drain hole in the ball support is coated with type UN-25 pasts before its installation ir place.

Before installation of the half-shafts into place, the half-shaft journals for the seal and for the air supply head must be coated with 1-13c (VTU NP5-58) or YaNZ-2 (GOST 9432-60) lubricant.

The inner hollow of the half-shaft seal ring must be serviced with the same lubricant.

Before installation of the turning spindles, the working surfaces of the collar and surfaces of the centering holes in the air supply head must be coated with a thin coat of the same lubricant. The inner hollow of the air supply head must be serviced with lubricants, but the hole for the fitting must be free of lubricant.

The journals on the stub axle of the ball joint for the air supply head and for the bronze bushing must also be lubricated.

The space between the air supply head and the protective hushing, the space between the inner half-shaft seal and the support collar on the rea and middle axle housings, and also the space between the spindles and the seme lubricant.

When pindles are installed in place, it is necessary to ensure the proper p to of the holes for the air supply formed in the spindle journals.

of the front axle reduction gear should be accomplished on a stand or on h. Press the outer races of the front and rear bearings 5 into hous see Plate 10-15) with a mandrel until they rest against the housing fil reference is 0.025-0.075 mm).

ant the inner race of front bearing 5 on the shaft of driving gear 4 and sess it with a mandrel or press until it rests against the face of the gear discreterence is 0.019-0.048 mm).

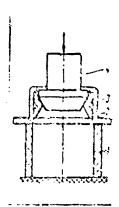


Plate 10-59. Pressing the outer race of the double tapged bearing out of its recess:

1) support 2) recess 3) outer bearing race 4) mandrel

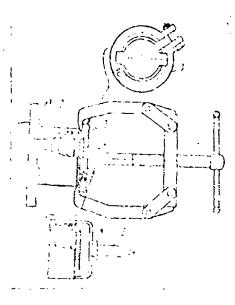


Plate 10-60. Method of pressing out half-shaft seal:

- 1) turning spindle body 2) half-shaft seal 3) puller auxiliary ring
- 4) puller support bracket 5) screw

Hount the bevel pinion gear 4 in assembly with the inner race and rollers of the front hearing on shaft 3 with a mandrel and press, and press them on until they rest against the shaft fillet. A clearance of 0-0.44 mm is allowed in the fit.

Press bearing 2 onto the journal on the front end of the pinion gear shaft until it rests against the face of the shaft (interference is 0.015-0.040 pm). Install stop ring 1 on the shaft with a screwdriver and hanser. Set the shaft in .. device (Plate 10-61) in the vertical position with the splined end up. wount the adjusting washers 7 and carrier 6 in assembly with the outer races of the bearings on the pinion gear. Install the inner race with the rollers of the rear bearing with a harmer and mandrel until the race rests against the adjusting washers (fit from interference of 0.003 mm to clearance of 0.052 mm).

Hount the oil deflecting washer 13 on the shaft with glue on face P. Mount the sealing gasket and cover 8 with its seal in assembly on the housing. Instail flange 9 with the deflectors on the splines of the shaft, and press them until they are seated (fit with a clearance from 0-0.67 mm). Install the support washer 10 and fasten the flange with nut 11. The torque moment on the nut must be 20-25 kg meters. Remove the unit from the device.

Install the bevel pinion gear shaft in a vise, lightly press in the bearing carrier, and check the preliminary interference of the bearings.

The tapered roller bearings of the bevel pinion gear shaft are adjusted with a small amount of preliminary interference, and exial clearance is not allowed. The merent of torque necessary to rotate the shaft in the bearings must be within the limits of 0.08-0.16 kg meters, which corresponds to a force of 2.2-4.5 kg applied at the flange hub for the first, middle, and rear drive axles. The method of checking is shown in Plate 10-22, c.

Measure the torque moment required for continuous smooth rotation in one direction after no fewer than five full rotations of the shaft. The bearings must be lubricated with transmission oil during this operation.

While the rotation moment of the bevel pinion gear of the front (middle) axle is being checked, bearing cover 20 (see Plate 10-14) must be moved away so that the centering projection of the reduction gear housing 6 goes into the recess in the cover and the seal does not form resistance to rotation of the gear shaft.

Adjustment of the preliminary tightness of the bearings on the pinion gear shaft should be adjusted with a selection of adjusting washers having the required thickness. Two of these are installed between the faces of the bearing inner races.

The factory puts out adjusting washers having thicknesses or: 7.25, 7.40, 7.50, 7.60, 7.70, 7.80, and 7.85 ms.

After final adjustment of the rearings has been completed, the nut fastening the pinion gear flange must be tightened and pinned. Torque moment for tightening the nut must be 20-25 kg meters. While tightening the nut, turn the pinion gear shaft so that the bearing rollers occupy the proper positions between the bevoled surfaces of the rings.

After assembly and adjustment of the shaft, it is recommended that the pinion gear in assembly with its housing and bearings also be set in a device and turned for a period of one minute with a shaft speed of 200 rpm. After this turning, the moment for shaft rotation in the bearings is again checked with a dynamometer. It must be within the limits of 0.08-0.16 kg meters.

Assembly of the cylindrical driving gear and rin, gear. Install bearing 2 on the journal of the ring gear 1 (see Plate 10-16), and plass the bearing until it rests against the face of the gear with a mandrel and press (interference is 0.003-0.038 mm). Install spacing ring 4 on the journal of the ring gear with a hammer until it rests against the face of the bearing (from a clearance of 0.197 mm to interference of 0.023 mm). Press key 3 into the keyway in the driving cylindrical gear journal. To ease fitting, it is recommended that the ring year in assembly with its bearings be previously heated in oil to 120°C and pressed onto the shaft journal while hot with a mandrel and press until they rest against the face of cylindrical gear 5 with an interference of 0.033-0.987 mm. After assembly, the outer race of the bearing must rotete freely.

Assembly of the differential. Before assembling the parts of the differential, it is necessary to rub them off with a soft cloth and lubricate the assembly surfaces with transmission oil. The recommended order of differential assembly is as follows.

Set the differential box cup on a plate or bench. Install the bearing inner race with the rollers on the cup journal, and press it with a mandrel until it rests against the face of the cup (see Plate 10-35) with an interference of 0.010-0.045 mm. Assembly of the other differential cup is performed in a similar manner.

Install one of the differential box cups on the support on a bench. Install the ring gear 1 (see Plate 10-17) on the differential bex cup. Insert support washer 6 and half-shaft gear 7 in the cup (clearance from 0.065-0.165 mm). Mount the four differential pinions 5 with their supporting spherical washers 4 on the journals of cross 3. The differential pinions must be installed on the journals of the cross with a clearance of from 0.050-0.105 mm. Lay the cross in assembly with the differential pinions on the differential box cup. The cross journals have a fit in the cup with a clearance of up to 0.05 mm, or an interference of up to 0.01 mm.

Lay the other half-shaft gear with its support washer on the differential pinions. Install the second differential box sup, aligning the marks made with a punch during disassembly. Insert the boits into the holes in the differential box cup, aligning them with the holes in the ring gear. Screw the nuts onto the boits and tighten them with an angular socker wrench. Torque moment on the nuts must be i2-14 kg meters.

Check the correctness of the differential assembly. Insert a leaf gauge between the supporting face of the half-shaft gear and a support washer opposite each of the four openings in the differential box cup. The clearance must be within the limits of 0.05-1.2 km for each side. Deviation of the clearance for one gear must not be greater than 0.2 mm. The differential pinions and half-shaft gears must turn easily. Tight rotation of the gears or their binding is not allowed. After checking, the nuts fastening the differential box cups must be pinned.

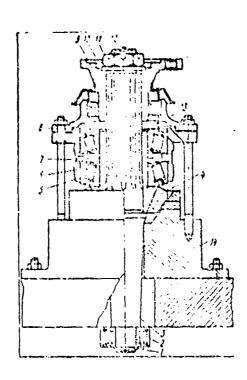


Plate 10-61. The bevel pinion gear in assembly with the bearings, installed in a device for assembly and disassembly:

- 1) stop ring 2 and 5) bearings 3) shaft
- 4) goar 6) bearing carrier 7) adjusting washer.
- 8) pinion gear bearing carrier cover 9) flange
- 10) washer 11) nut 12) cotter key 13) oil. deflecting support washer 14) device

Assembly of the reduction goar. Install the driven bovel gear and driving cylindrical gear (see Plate 10-16) in the recess in housing 6 (see Plate 10-14) of the reduction gear. The fix of the outside roller bearing race is accomplished with a clearance from 0-0.058 mm. Install the outer race of the bevel tapored bearing 8 in recess 10 of the driving cylindrical goar

with a clearence from 0-0.05 mm. Assemble the inner races of the bevoltapered roller bearing, installing an adjusting ring between them. Before assembly, the bearings must be lubricated with transmission oil. Lay the adjusting gaskets on the fixing of the recess.

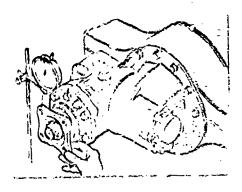


Plate 10-62. Measuring lateral clearance between bevol gear teeth

Install the assembled rocess with its double bearings in housing 6, guiding the hole of the inner bearing race onto the journal of the driving cylindrical gear shaft. Press the inner bearing race onto the shaft journal with a mandrel and hammer until it is sested. The fit of the bearing racess in the reduction gear housing is accomplished with a clearance from 0-0.08 mm. The fit of the double bearing on the shaft journal is accomplished from clearance of 0.027 mm to interference of 0.002 mm.

Mount the support washer on the end of the shaft and, scrowing on the nut, tighten it (moment is 20-25 kg motors).

The double roller bearing 8 of the driving cylindrical gear shaft is put out by the manufacturing plant with selected adjusting rings 13, and therefore requires no additional adjustment. The parts of this bearing are not interchangeable, and therefore changing parts from one bearing to another is not allowed. The inner race of the bearing, which has the letter V stamped on its face, must be installed on the side of the stamped face of the outer race.

Install cover 7 with its gasket and fasten it with bolts. The bearing recess is simultaneously fastened.

After mounting the adjusting gaskets 15 on the flange of housing 21 (see Plate 10-14), install the assembled bevel pinion gear sheft (see Plate 10-15) in the reduction gear housing. Fasten housing 21 in assembly with the cover

with bolts. The front bearing 28 of the bovel pinion geer shaft is inctalled in its recess with a fit from clearance of 0.037 mm to interference of 0.006 mm. The besel pinion gear shaft bearing housing is installed in the reduction goad bousing recess with a clearance from 0-0.067 mm.

The bevel pinion gear 24 and driven goer 25 of the reduction gears are matched as a unit at the factory according to spot of contact and lateral clearance in the engagement. They are lapped together, and stamped with a unit serial number. During the process of the motor vehicle's operations, the goars are worn in, and therefore, if it is necessary to replace one of the gears, simultaneous replacement of both of them is recommended. Newly installed bevel gears must have the same unit serial number.

When the new bivel gears of the reduction goar are installed, they must be adjusted according to point of contact and according to rateral clearance in their engagement.

The point of contact on the pinion gear may reach the top edge of the tooth. The methods for correcting the point of contact and achieving the proper gear engagement are presented in Table 10-3.

The point of contact is marked by applying a thin layer of paint on several teeth of the driven gear and rotating the pinion gear shaft in both directions, simultaneously braking the driven gear by hand.

The lateral clearance between the teeth of the pinion and driven bevel gears must be within the limits of 0.15-0.40 mm at the wide part of the tooth, which corresponds to a rotation of the bevel pinion gear shaft flange by an amount of 0.16-0.48 mm, measured at the radius of the bolt hole on the flange with the driven gear remaining stationary (Plate 10-62). For the middle axle reduction gear, the measurement is taken on the smaller flange. It is necessary to check the lateral clearance on no fewer than four teeth of the driven gear, located at equal distances from the circumference.

When new goars are installed in the reduction goar, it is necessary to install adjusting gaskets 15 (see Plate 10-14) having 2 mm total thickness beneath the flange of the pinion goar shaft bearing cerrier. After this, adjust the lateral clearance, moving the driven bevel goar by changing the number of gaskets 12 beneath the flange of bearing recess 10 of the driven goar shaft, and then check the point of contact. If a proper point of contact is not achieved as a result, it is necessary to move the bevel goars as shown in Table 10-3, changing the number of gaskets beneath the flanges of the pinion goar shaft bearing carrier and driven goar bearing recess.

After finally adjusting the point of contact, no fewer than two gaskets 0.1 mm thick must be installed in each gasket set. Thin gaskets must be located on both sides of the gasket set to attain a tight hermetic connection.

The bolts fastening the carrier, recess, and covers of the bearings must be tightened after final adjustment (tightening moment is 6-8 kg meters). If the gears have an increased lateral clearance in their engagement as the result of tooth wear, they should not be adjusted, since this would spoil their proper engagement. The bevel gears must work until they are fully worn without additional adjustment.

When installation of the reduction goar components and adjustment of the goar engagement have been completed, it is necessary to install the differential.

If the stude fastening the differential bearing covers have been replaced, they must be acrewed into the reduction gear housing, tightened (mement is 22-25 kg meters), and then pinned.

Mount the outer races on the rollers of differential box cup 5 (see Plate 10-14) and install the differential in the reduction gear housing, guiding the outer races of both bearings 5 into the recess in the housing. Install differential bearing cover 33 and adjusting nut 4, aligning their threads. If the cover does not sit in place, this means that the adjusting nuts are cross-threaded and they must be corrected on the threads. Installation of the covers with excessive force may lead to damage of the housing, covers, and adjusting nuts. After installation of the bearing covers, it is necessary to screw nuts 34 fastening the covers until they are seated and, after this, loosen them enough so that adjusting nuts 4 can be turned. Adjusting nuts 4 must be installed so that the ring gear occupies a position which is symmetrical in relation to its driving year.

The differential bevel roller bearings must be adjusted with a small amount of preliminary tightness. For this, the adjusting nuts must first be set so that the differential has a lateral movement not exceeding 0.01 mm. The amount of lateral movement must be checked with an indicator installed opposite the ring gear rim and fastened on the bearing cover.

After this, tighten each adjusting nut by one slot, lock them in this position with stop 3, and tighten the stop. Tighten the nuts 34 fastening the bearing c vers (moment is 17-19 kg meters) and pin them.

While adjusting the bearings, it is necessary to turn the differential several times so that the bearing Follers occupy their correct position between the bevoled surfaces of the rings. Before assembly, the bearings must be lubricated with transmission oil.

Check the operation of the reduction gear, turning the pinion gear shaft flange by hand. During this operation, the gears must turn freely without binding or catching on the reduction gear housing.

Before assembling the ball support, it is necessary to check the usability of the support washers 14 (see Plate 10-19). If the washers are worn, they must be replaced. The washers fit into the ball support turnings with an inter-

ference of 0.105-0.225 mm. If necessary, replace the half-shaft seal (see Plate 10-60). The new seal is pressed into its ring with a mandrel and hammer (interference is 0.05-0.45 mm). The ring in assembly with the seal is pressed into the ball support recess (interference is 0.015-0.135 mm). The order of assembly is as follows. Set the ball support assembled with the king pins in the turning spindle budy. Set the ball support in assembly with the body in a device (see Plate 10-49). Set the bottom king pin on support 2. Mount the inner race of bearing 5 on the top king pin and press it onto the king pin with mandrel 6 until it rests against the face with an interference of 0.003-0.032 and. Install the outer race in the top hole of the rotating spindle body, and fit it in the body with a hammer and mandrel, with a cleurance of from 0-0.05 mm. Turn the ball support together with the turning spindle body in the device, and press the inner race of the other bearing on the king pin and the outer race into the body hole by the indicated method. Screw the cover fastening stude into the turning spindle body. Ley the adjusting gaskets on the face surface of the body. Install the bottom and top covers on the stude, and mount the conic split bushings and spring washers on the stude. Screw on the nuts and tighten them until they are seated. The tightening moment of the nuts must be 16-18 kg meters. (heck rotation of the king pins in the ball support bearings, and if necessary adjust them.

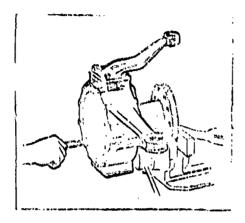
The turning spindle king pin bearings of the front drive axle are adjusted with a preliminary tightness. The torque moment necessary for smooth turning of the turning spindle body must be 0.5-0.6 kg meters, which corresponds to a furce of 2.0-2.4 kg applied at a hole in the turning arm for the steering tie red (Plate 10-63). During this operation, the bearings must be lubricated (see the lubrication chart).

Axial movement of the bearings is not allowed. The absence of axial movement may be checked with an indicator installed on the face of the lower king pin with a plug screwed into the cover. Using a jack or lever, move the rotating spindle upward, during which the movement of the indicator hand will show the presence of axial movement in the bearings. In order to eliminate axial movement, it is necessary to remove the required number of adjusting gaskets from beneath the lower cover, since the lower bearing is usually worn more severely. If it becomes clear during disassembly that wear of the bearings is identical, it is necessary to remove an identical number of gaskets from beneath the upper and lower covers. If the lower king pin bearing is severely worn, it is recommended that the bearings be switched from place to place. In this case, the adjusting gaskets must be removed from beneath the upper cover.

During installation of new bearings, it is necessary to measure their assembly height (from the support face of the outer race to the support face of the inner race). The overall thickness of the gasket set installed on the side of the large bearing must be larger by the amount of the difference in the bearings' assembly heights. If this rule is not observed, installation of adjusting gaskets may lead to a loss in alignment between the rotating spindle body and the ball support.

After final adjustment of new bearings, no less than ten gaskets 0.1 mm in thickness must be included in each of the gasket sets. Two gaskets 0.05 mm thick and one gasket 0.1 mm thick must be installed in the gasket set on the side of the turning spindle body, and the remaining thin gaskets are installed on the side of the cover or steering linkage turning arm to attain a tight, hermetic connection.

During the process of adjustment, it is necessary to turn the turning spindle body several times so that the bearing rollers occupy their correct position between the races of the bearings.



Plato 10-63. Checking the preliminary tightness of turning spindle king pin bearings

After adjustment of the ball support bearings is completed, install the rubber plug in the slot in the turning spindle body, mount the seal on the ball support, and festen its ring with bolts, previously placing spring washers beneath the bolt heads. Screw the adjusting bolt into the hole in the turning spindle body and adjust with it the angle of turn, which must be within the limits of 29-30°. In this, are bolt head must rest against the ball support. When adjustment is completed, braze the support bolt to the turning spindle body.

Assembly of the front axis half-shaft joint. Before assembling the parts of the joint, it is necessary to rub them off with a clean, soft cloth, and lubricate them (see the lubrication chart). Assembly of the joint takes place in the following order. Fasten the inner half-shaft 3 (see Place 10-51) in a device or in a metal working vise. Connect the stub axis with the inner half-shaft (see Plate 10-51, b). Select the drive balls 6, using the installation ball with the flat. For this, place it in the center sphere of the assembled parts. Sequentially install the balls (one at a time) in the four recesses with the stub axis being lightly rocked back and forth. The final,

locking ball is installed in its recess only after its formed surface coincides with the flat on the installation ball. After assembly, check the operation of the joint with & dynamometer, turning the stule axis by an angle of 10-15° in three directions: in plane I-I (see Plate 10-51) of the spindle; in plane I-II of the half-shaft, and in plane III-III of the two opposite balls. The moment necessary to turn the stub axis by an angle of 10-15° must be within the limits of 3-9 kg meters, which will correspond to a force of 10-30 kg.

The difference between the largest moments of turning in the three planes what be no greater than 1.5 kg meters, which will correspond to a force of 5 kg. After turning the stub axle at an angle greater than 10-15°, the turning moment is allowed to decrease to zero. When the axle is turned by hand, there must be no noticeable binding of the balls.

The assembled half-shaft should be checked on a stand at 30 rpm with a load of 100 kg meters, and the stub axle of the joint should be turned at an angle no less than 31 to one side and the other, relative to the inner half-shaft. During this operation, there must be no knocks or gritting, binding of the drive balls on the central ball, or grinding of the joint parts on the half-shaft.

In a case where the cited defects appear, the joint is disassembled and the driving balls are changed, using a larger dimension if the moment required for turning the stub axie is smaller than that indicated, or a smaller dimension if the moment for turning is larger than that indicated. The driving balls range in diameter from 42.757-42.947 mm, and are divided into nine groups, differing according to dimensions by 0.02 mm. The dimensions of the balls according to groups are represented in Table 10-8.

After selection of the balls is completed, it is necessary to disassemble the joint. Pull out the selected driving balls and the installation ball with the flat. Insert a central ball in its place, and assemble the joint with the newly selected driving balls. The diameter of the center ball is equal to 41.25-41.30 mm. During installation of the fourth driving ball, the stub axle is pulled out and turned at an angle allowing the fourth ball to slip into place. When assembly is finished, it is necessary to turn the stub axle until it is aligned with the inner half-shaft and remove it from the vise. If the joint is assembled with driving balls from various groups according to diameter, these driving balks must again be installed in their former recesses when the central ball is exchanged. If necessary, repeat the operational check of the assembled half-shaft ball joint.

Assembly of the front axle turning spindle. The spindle assembly is shown in Plate 10-20. If worm-out bushing 2 was pressed off the spindle, a new bushing replacing it is pressed on with an interference of 0.09-0.21 mm. The new bushing should first be smoothed out to a dimension of 52.95-53.01 mm, and then machined with a reamer to a dimension of 53.4-53.6 mm. Install air supply head 3 in the spindle recess in assembly. Insert fitting 4 in resembly with its seal in the hole in the spindle, and screw it into the body of the sir

supply head. If support washer 6 is norm out above the allowabse dimension, a new support washer is pressed into support ring 5 with an interference of 0.03-0.21 mm and rowed into the slots in the support ring. Install the ring in assembly with its support washer on the face of the spindle and fasten it with bolts. Place stop washers beneath the bolt heads before this is done. After the bolts are tightened down firmly, they are blocked with the washers (bent up against the bolt flats and ring). After replacement, machine the face of support washer 6 to a dimension of 2.15-2.25 mm.

If the inner race of the wheel hub inside bearing has been removed from the spindle, it should be again pressed onto the spindle journal until it rests against the fillet.

Assembly of the ball support with the front axle housing. Screw the saids halfway into the holes in the front axle housing 25 (if they were unscrewed) (see Plate 10-11). Connect the ball support body with the axle housing in such a way that the turning arm connected with the steering tie rod is directed toward the side of the flange on the final drive pinion gear shaft. Align the holes in the ball support flange with the stude on the axle housing flange. Press the journal of the ball support into the hole in the axle housing flange until it seats with the axle housing flange, with a fit from clearance of 0.05 mm to interference of 0.02 mm.

Install spring washers on the stude, screw nuts onto them, and tighten them until they are seated (torque moment is 16-18 kg meters). Apply fresh grease inside the ball support (see lu. ication chart).

Assembly of the front axle is conducted on a stand. Assemble the front axle in the following order. Set the axle housing on the stand. Lay the sealing gasket on the face of the large housing flange, and install the reduction goar asnesbly (see Plate 10-14) in the rocess in the axle housing. Fasten the reduction gear housing to the axle housing with the exterior bolts and the two bolts on the inside, first installing spring washers beneath the bolt heads. The torque moment on the bolts is 9-11 kg meters. Install side cover 24 (see Plate 10-11) of the reduction gear housing with its sealing gasket, and fasten it with bolts. Scraw the stude into the turning spindle body if they were unscrewed during disassembly. Install the inner half-shaft 19 in assembly with the stub axle on the ball support and axle housing in such a way that you do not damage the seal, and so that the splined end of the inner half-shaft goes into the splined hole in the half-shaft gear. The fit in the splined connection has a clearance of 0.035-0.235 mm. Install spindle 2 in assembly with the stub axis, guiding the holes onto the stude of the turning spindle body in such a way that hole 2 (Plate 10-64, b) for all supply to the front axle spindle journal is in the proper position.

Install the orindle by its centering collar in the hole in the ball joint body with a mandrel and hommer, attaining fit from clearance of 0.96 mm to interference of 0.024 mm. Install the brake backing plate 30 in assembly (see Plate 10-11) on the stude, and mount the ring with the outside seal 12 in assembly on the stude after servicing the seal in oil. Mount spring washers on the stude, sorew nuts on them, and tighten them with a socket withch (moment is 5.5-6.0 kg meters). Screw fitting 13 with its hose into the air supply

head. Install the spreader cams, adjusting covers, brake shees, and chambers. Install wheel hub I and bearing 9, screw on nut 3 fastening the bearing, inatall lock washer 8, and tighten step out 5. Adjust the wheel hub bearings. For installation of the whoel hubs and adjustment of the bearings, see Chapter 15. For installation and adjustment of the brakes, see Chapter 16.

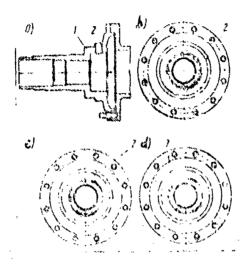


Plate 10-64. Diagram of location of the heles in the spindle for air supply to the drive axle tires of the ZIL-131 motor vehicle a) longitudinal section of spindle b) for front axle c) for middle axle d) for rear axle

1) spindle 2) hole in spindle for air supply

Mount the gasket on the hub stude and then gount splined half-shaft flangs 7, previously fitting it onto the splines of the stude axis. The fit at the splined connection is with a clearance of 0.035-0.205 mm. The splines must be labshcated with the grease used in packing the wheel hubs. Install spring mashers on the stude, screw nuts onto them, and then tighten them (meant is 7.9 kg poters). Insert valve 5 and fasten it to the half-shaft flange.

Assembly of the rear and mildle drive taken is similar to assembly of the front drive axio.

adjustment of the boarings and grave of the middle and rear axle reduction gear is similar to adjustment of the reduction gear bearings in the front

drive axic. During assembly of the bovol pinion goar shall of the axic reduction goar, the support washer for the inner race of the relier bearing should be installed with the stamp C on its face. This shows that the washer is equipped with an oil-slinging passage with a right-hand spiral. It is necessary to remember that when the motor vehicle is moving forward, the convex side of the tooth for the middle and rear axies and the concave side of the tooth for the front axie is the tooth's working side in the driven bevel goar. The spindles of the middle and rear axies should be installed according to Plate 10-64, c and d.

Testing drave axles. The assembled rear, middle, and front axles must be checked on a stand or with a run of the motor vehicle. The tested axle must satisfy the same requirements as the axle on a ZIL-157K motor vehicle.

The absence of binding in the joints of the front axle must be checked with the turning spindle set in the straight position, and also when they are at the extreme turning angles to the right and left.

Before installing the drive axles in the motor vehicle, it is necessary to assemble the wheels and fasten them ento the axles. Install the springs on the front axies, and on the middle and rear axles, first connect the balancing appension, and then install the springs.

for installation of the axles, first raise the front part of the motor vehicle from with a hoist mechanism and roll the front axle beneath the frame. Connect the front and rear ends of the springs to the frame brackets. Install the shock absorbers and lower the front part of the frame. Raise the rear part of the frame, roll the rear drive axle carriage together with the balancing suspension beneath the frame, and lower the frame onto the brackets of the balancing suspension. Insert the bolts fastening the balancing suspension brackets to the longitudinal rails and frame cross numbers, screw on and tighten the suck until they are firm, and release the motor vehicle frame.

Connect the flexible hoses to the brake chambers, the hoses for air supply to the tires, the longitudinal steering rod and the propellor shafts of the front, middle, and rear axles.

Dimonsions of parts

Dimonsions of parts are presented in Tables 10-4, 10-5, 10-6, 10-7, and 10-8.

Table 10-4. Basic dimensions of rear axle parts of the ZIL-130 motor vehicle,

Dimension	Nominal	Allowable without repair
	Rear axle housing (cast)	
KCh 35-10 iron (GOST 1215-59)	•	
Diameter of hole for firs; half-shaft tube journal Diameter of hole for second	74.92-74.96	74.98
half-shaft tube journal Diameter of hole for third	73.00-73.12	73.14
half-shaft two journal Diameter of hole for fourth	72.00-72.12	72.14
haif-shaft tube journal Diameter of housing journal	71.00-71.12	71.14
for rear axle hub seal	93,20-93,50	. 93 , 1 0
Roar	axle housing (wolded)	<u>)</u>
Type 20 steel (GOST 1050-60).		
Diameter of journal for whoch hub inner roller bearing race	84 .925-84 .960	84,9C
Diameter of journal for wheel hub outer bearing		04.30
race Diameter of journal for whool hub inner bearing	74.94-74.97	74.92
seal ring Diameter of threads for	93.060-93.085	93.04
whool hub outer bearing fastening nut	M72 X 2, class 2	
	Half-shaft tube	
Type 45 steel (TU 78-85); har axle housing.	dnessHB 235-321 used	i only with the cast rear
Internal tube diameter Diameter of helf-shaft	56.5-58.5	~ "
tube journals for roller bearing race Diameter of tube journals for rear axle housing;	"4,94-74,97	74.92

Pirst	74.94-74.97	74.92
Second	73.165-73.225	73.145
Third	72.165-72.225	72.145
Fourth	71.165-71.225	71.145
Diameter of threads for	•	
wheel hub out *		
bearing fastening mut	472 X 1.5, class 2	
Redi	uction goar housing and its cove	E
KCh 35-10 from (GOST 1215-	-59).	
Diameter of hole for		
pinion goar shaft		
roller bearing	140.018-140.060	140.19
Diameter of hole for		
housing cover	135.00=135.04	135.06
Diameter of hole for		
differential roller	110 00 180 04	150 03
bearing	130.00-130.04	139.08
Diameter of threads		
for reduction gear		
housing cover festening bolts	M12 X 1.75, class 2	
Diameter of through	M12 A 1./5, C1895 2	
for fastening bevel		
pinion goar shaft	•	
bearing housing	M12 X 1.75, class 2	• •
Diameter of hole in	(120 K 21/0) 02/00 =	
left cover for		
bearing	109.941-109.976	109.985
Diameter of hole in		
right cover for		
bearing	119.941-119.976	119.985
Diameter of journal in		
left and right covers	134.845-134.900	134.81
Navol :	ulaton gan shock annulan	

Bevel pinion gear thaft carrier

KCh 35-10 iron (GOST 1215-59).

Diameter of hole for		
large roller bearing	139.932-139.972	139.99
Diamoter of hole for		
small roller bearing	109.941-109.976	109.29

devol pinion gear

Number of teath--13; 30khST steel (GGST 4545-61); hardened layer depth--1-1.4 ma; hardeness of surface layer--HRC S6-62.

Diameter of larger journal for roller		
bearing	65.003-65.023	64.9
Dismoter of scaller journal for roller		-
bearing	49.985-50.004	49.91
Longth of your teeth Thickness of splined	43,86-43,00	* 4
testy	6.94-6.99	6,85

Front bearing cover

kCh 35-18 iron (COST 1215-59).

Diameter of enver recess	93.00-93.07	93.2
Diameter of cover journal for hole in pinion		• • • •
gear shaft bearing carrier	109,86-109,95	199,70

Bovol pinion goar shaft flange

Type 45 steel (GOST 1050-60); depth of case hardened Laver--1.0-2.5 mm; hardness--HRC 56-62.

Diameter of flange		
journal for seai	61.94-62.00	61.80
Diameter of holes for		
boits	14.24-14.36	15.00
Width of grooves in		
flange splined portion	7.00-7.05	7.2

Differential box cup

Type 6 steel (GOST 380-60).

Diameter of hole for		
half-shaft gear journal	75.00-75.06	75.20
Diameter of journal for		
roller bearing	75.01-75.03	75.00
Diameter of hole for		
differential cross pins	28.02-28.05	28.10

Diameter of hole for compression boils 14.24-14.36 14.8 Diameter of turning end cup for ring goer:

Inner 198.004-198.035 197.97 Cater 249.7-250.0

Ring geer

55 PP steel; depth of case hardened layer--1-2.5 gm; hardness of surface layer-HRC 52-63; number of teeth--47.

Diameter of fitting hole
for differential cups 198.008-198.027 198.03
Tauth length 70 -Touth thickness
(Measured at height of 3.42 mm) 8.2 7.7

Differential cross

18KhGT steel (COST 4543-61); depth of hardened layer--0.8-1.2 mm; hardness of surface layer--HRC 56-62

Diameter of cross journal 28.00-28.03 27.97

Differential pinion

25khúT steel (ChMTU TsNIIChM 561-61); depth of hardened layer--0.9-1.3 mm; hardness--RRC 58-65; number of teeth--11.

Dismeter of hole for cross journal 28.960-28.105 28.15 External dismeter of bushing 29.67-29.70 -- Internal dismeter of bushing 28.060-28.105 28.15

Half-shaft goar

18KhGT stool (GOST 4543-61); depth of hardened layer--1-1.4 mm; hardness--HRC 56-62; number of teeth--22.

Diameter of goar 74.895-74.935 74.75

Marie San Carle Land William Hill Street

Driven bevel goer

Number of teach--25; 30KhGT steel (GOST 4543-61); depth of hardened layer--1-1.4 we; hardness of surface layer--HRC 56-62.

Tooth length	39.83-40.00	
Diameter of hole for rivet	10.2	 1មិ.5
Biameter of hole	AU, a	1963
for driving	3.60 AOU 110 AP1	*** 0.0
cylindrical goar	110.090-110.054	116.08

Driving cylindrical gear

Number of teach--14; 20%hM steel (GOST 4543-51); depth of hardened layer--0.9-1.3 mm; touth surface hardness--KRC 54-62.

Disactor of larger	: :	
journal for roller bearing	54.982-55.005	4.97 ماريان 14.97 ماريان
Disseter of smaller		•
journal for roller	•	
dearing	49.985-50,004	49.97
Diameter of support		•
surface for driven	-	
bayel gear	110.070-110.095	110.37
Tooth leagth	75	
Toosh thickness	10.3	₩, ₩
Diazeter of hole for		
rivees	10.2	10.5

Half-shafes

45 RP secol (GUST 1063-63); depth of case hardwood layer--6.0 mm; hardness--HRC 52-60; number of holes for hub studs--12 (6.0 mm in diameter).

1005-121;	* "
16.₹	17.0
S.17	5.90
M12 X 1.75, class 2	
	5.17

Table 10-5. Basic dimensions of the drive axle parts of the ZIL-157 motor vehicle, mm

Dinansion	Nominal	Allowable without repair
•	Housings and covers	
KCh 35-10 Brought from (GOS	T 1215-59).	
Diameter of hole for differential box roller bearing Diameter of hole for	199.941-109.976	110.000
pinion shaft rear roller bearing Dismeter of hole for	61.95-61.98	62.00
pinion shaft bearing carrier	98.50-98.57	98.60
Ax	ie half-shaft jacket	•
Type 45 steel (1029 X 169, HB 197-229.	tube, GOST 8732-58 and 1	GOST 8731-58); hardness
Digmeter of hole for seal in front, middle, and rear drive axles Diameter of hole in	80.06~80.06	80.20
jucket for ball support journal of front axle Diameter of turning in half-shaft jacket flange in middle and rear drive axles for	70.000-70.046	70.080
spindie	160,000-160,063	160.120
	Spindle	
40Kh steel (GOST 4543-61); HRC 50-62.	depth of case hardened l	layer1-3.5 mm; hardness
Diameter of journal for wheel hub outer bearing	74.94-74.97	74.92
Diameter of journal for wheel hub inner bearing Diameter of journal in	79.94-79.97	79.92
spindle for air supply head seal	67,94-68,00	67.83

Diameter of journal in spindle for inner hub	\$4.86-95.00	94.70
Diameter of journal in	54.60-53.00	54.70
spindle for hole in turning spindle body Disseter of threads for	159.982-160.022	159.950
wheel hub outer bearing fastening nuts	M72 X 1.5, class 2	.
	Turning spindle body	
KCh 35-10 iron (GOST 1215-	-59).	
77		
Diameter of hole for king pin bearing Diameter of hole for	72.00-72.03	72.05
spindle	160.000-160.063	160.120
Diameter of hole for		2001727
turning spindle body	35 000 25 058	
bushing	25.000-25.033	••
	Spindle ball support	
40KhN steel (GOST 4543-61)	; herdnessHB 229-269.	
Dinastes of emposes	·	
Diameter of support journal for half-		
shaft jeckot	69.97-70.00	69.94
Diameter of turning		•
for half-shaft	10 00 15 10	
support washer	65.00-65.12	65.3
Diameter of hole for king pin:		
First grip	38.000-38.027	*-
Second grip	38,500-38.527	* •
·	King pin	
ABIS, name (MARRY LEAS CA)	handman tibe 25 45	
40Kh steel (GÖST 4543-61);	naronessnac 35-42.	
Diameter of king pin		
journal for inner		
bearing race	30.002-30.017	29.98
Diameter of king pin		
journal for ball support:		
First group	38,035-38,052	+ •
Second group	38.535-38.552	

Bearing carrier

KCh 35-10 iron (GOST 1215-59).

Diameter of hole for front and rear bearings Diameter of hole for	99.925-99.960	99.980
bearing carrier fastening bolts	12.5	12.8

Bevel pinion gear

20Kh2N4A tteel (GOST 4543-61); depth of hardened layer--1.2-1.6 mm; hardness--HRC 58-65; number of teeth--6.

Diameter of journal for rear bearing	45.018-45.035	45.00
Dismeter of journal for	401010 401000	40,00
front bearing	44.965-44.980	44,95
Diameter of tail journal		
for bearing	25.015-25.030	25,0
Gear tooth length	45.0	
Gear tooth thickness		
(measured at height of		
9.85 mm)	13.46	13.2
Tooth thickness of gear		
splined portion	5.925-5.975	5.85
Diamotor of threads	M24 X 1.5, class 2	

Bearing carrier cover

KCh 35-70 iron (GOST 1215-59).

Dismotor of hole in		
cover for seal	82.00-82.07	82.25

Pinion goar shaft flange

Type 45 steel (305T 1050-60); depth of case hardened--1.3-1.3 mm; hardness--HRC 54-62.

Diameter of flange		
journal for seal	54.88-55.00	54.70
Groove width on flange		
splined portion	6.00-6.05	6.10
Diameter of holes for		
fastoning bolts	14.24-14.36	15.0

Differential box cup

KCh 35-19 wrought iron (GOST 1215-59).

Diameter of journal for roller bearing Diameter of recess for	65.01-65.03	64.99
haif-shaft gear journal Diameter of holes for differential cross	58.000-58.046	58.10
pins Diameter of spherical surfaces for differ-	22.150-22.175	32.20
ontial pinion washers	119.60~119.690	119.00
Diameter of holes for tension bolts	12.12-12.24	12.60

Driven bevol gear

20%h2N4/A steel (GOST 4543-61); depth of hardened layer--1.2-1.6 mm; hardness of surface layer--HRC 58-65; number of teeth--40.

Tooth length Tooth thickness	44.2	
(measured at height of 2.52 mm)	5.94	5.70
Diameter of hole for gear fastening bolts	11.5	11.7

D'fferential cross

20Kh2N4A steel (GOST 4543-61); depth of hardened layer--1.0-1.4 mm; hardness--

Diameter of cross journal

22,125-22,175

22.0

The same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the same of the sa

Differential pinion

Number of teeth--11; 12KhNZ steel (GOST 4543-61); depth of hardened layer--0.9-1.3 mm; hardness--HRC 58-65.

Tooth length	12.0	
Tooth thickness		
(measured at height of 5.67 mm)	8.05	7.8
Diameter of holes for	22 25 22 205	22.40
cross journals	22.25-22.295	22,40

Half-shaft goar

Number of teeth--20; 12Kh2N4A steel (GOST 4543-61); depth of hardened layer--0.9-1.3 mm; hardness--HRC 58-65.

Diameter of gear journal for hele in differential		
box	57.898-57.935	57.85
Gear touth length	19.0	
Gear tooth thickness		
(measured at height of	a	
3.85 mm)	7.63	7.40
Width of groove in gear		
splined portion	4.43	4.5

Rer & and middle drive axle half-shafts

40KhGTR steel (ChMTU TsN1/Ch. 974-63); hardness--HB 388-444.

Diameter of half-shaft journal for seal Tooth thickness of half-shaft splined	44.4-44.5	44.2
portion	4.17-4.25	4.0
Half-shaft longth:		•
Loft rear axle	1051	~ ~
Räght year axle	972	***
Left middle axle	887	e w
Right middle axle	1137	m* ++

Front axle hal f-shaft

20Kh2N4A steel (GOST 4543-61); hardened layer depth--1.2-1.6 mm; hardness--HRC 58-65.

Inner half-shaft length:		
Right	953.5-954.5	*-
Left	463.5-464.5	••
Stub axic length (right		
and left)	373.45-375.0	••
Diameter of stub axle		
journal for spindle		
bushing	47.9-48.0	47.8
Diameter of inner half-		
shaft journal for seal	44.4-44.5	44.2
Touth width of inner half-		
shaft splined portion	4.17-4.25	4.0
Tooth width of stub axle		
splined portion	3.60	3,4

Diameter of center ball 31.50-32.00 - Diameter of drive balls 34.83-35.010 -

Front axle half-shaft splined flange

40Kh steel (GOST 4543-61); hardness--HB 241-270.

Diameter of flange journa for huboap	1 110,43-110.50	110.40
Groove width of flange splined portion Diameter of holes for	3.64	3.7
flange fastoning bolts	12.5	12.8

Table 10-6. Diameter of half-shaft ball joint driving balls of the ZIL-157K motor vehicle, mm

۵	f py nne	в ливить
	l	34,83 - 34,45
	11	34,85 -34,87
	111	PR, ME TH, M.
	11	.54,8934,01
	١.	11,9114,01
	VI	14,721 34,98
	VII	41,95 34,97
	VIII	भ % आ फ
	13	10 /2 str. H.

Koy: a) Group

b) Diameter

Table 10-7. Basic dimensions of drive axle parts of the ZIL-131 motor vehicle,

Dimension	Nominal	Allowable without repair
	Drive axle housings	
Type 35 steel (GOST 1050-60)	•	
Diame or of hole for		
reduction gear housing Diameter of hole for	315.00-315.34	315.50
	88 00-88.035	88.060
Diameter of turning in middle and rear axle hering flange for		
spindle journal	133.000-183.045	183.080
	Spindle	
1095 1 (658m 4647 41) . J	landh ac aga bundanad	Source 1 O 7 E mm. handage
HRC 56-62, hardness of non-c	ase hardened surfaces-	layer1.0-3.5 mm; hardness -HB 229-255.
Diameter of journal for		
drive axle housing Diameter of journal for	182.977-183.024	182.945
wheel hub outer		
bearing	74,94-74,97	74.92
Diameter of journal for		
wheel hab inner	NO 04 NO 05	80. 0.0
boaring	79,94-79,97	79.92
Diameter of spindle journal for wheel		
boaring inner soal	114.36 115.00	114.60
Inner diameter of front		
axlo spindle bushing	53.4-53.6	54.00
Diameter of threads for		
wheel hub outer bearing	MM 2 12 A #	
fastening nuts	M72 X 1.5	
	Spindle ball support	
Type 45 steel (GOST 1050-60)	; hardnessHB 217-255	· •
Diameter of support		
journal for front axle housing	87.985-88.020	87,95
Diameter of turning for	011540 401 0 40	G. 120
inner naif-shaft support		
washer	74,00-74,06	74.30

[Teblo 10-7, continued]

Standard W. Santa Mari		
Diamete. of hole for king pin	42.000-42.027	₩ €
	King pin	
40Kh steel (GOST 4543-61);	nardnessHRC 35-41.	
Diameter of king pin journal for inner bearing race Diameter of kign pin	40.00 -40.020	39.985
journal for ball support	42.035-42.052	***
	Rotating spindle body	
KCh 35-10 from (GOST 1015-	-59).	
Diameter of hole for spindle journal Diameter of body hole	183,000-193,073	187.100
for king pin bearing outer 1400	90.000-90.035	90.055
	Reduction year housing	
RCh 15-10 from (GOST 1215)	-59).	
Diameter of hole for recess for driving	-59).	
Diameter of hole for	-59). 105.000-10\$.035	108.050
Diameter of hole for recess for driving cylindrical gear shaft bearing Diameter of hole for driven conic gear- shaft roller bearing Diameter of hole for		108.050 150.060
Diameter of hole for recess for driving cylindrical gear shaft bearing Diameter of hole for driven conic gear- shaft roller bearing	105.000-105.035	
Diameter of hole for recess for driving cylindrical gear shaft bearing Diameter of hole for driven conic gear-shaft roller bearing Diameter of hole for differential Foller bearing Diameter of hole for bevel pinion gear shaft bearing carrier Diameter of reduction	105.000-10\$.035 150.006-150.040	150.060
Diameter of hole for recess for driving cylindrical gear shaft bearing Diameter of hole for driven conic gearshaft roller bearing Diameter of hole for differential Foller bearing Diameter of hole for bearing Diameter of hole for bevel pinion gear shaft bearing carrier	105.000-105.035 150.006-150.040 125.060-125.040	150.060 125.066

Diameter of hole for front axle bevel pinion go: shadt roller bearing

61.949-61.979

62.000

Driving cylindrical gearshaft bearing rocess

KCh 35-10 iron (GOST 1215-59).

Diameter of hole for outer race of driving cylindrical gearshaft double tapered bearing

90.000-90.035

90,060

Outer fatting diameter of recess in reduction goar

housing

104.977-105.000

104.960

Bearing carrier for bevel pinion gearshaft

KCh 35-10 iron (GOST 1215-59).

Diameter of hole for

outer race of tapered bearings

109.925-109.960

109.980

Exterior fitting dismotor

of carrier

124.973-125,000

124,950

Front axle bevel pinion gearshaft

40Kh steel (COST 4543-61); depth of case hardened layer--1.5-4 mm; hardness--HRC 45-62; hardness of non-case hardened surfaces--HRC 28-33.

Diameter of journal for		
roller bearing	25.015-25.030	25.000
Diameter of journal for		
bevel pinton gear	45.983-45.000	45.965
Exterior diameter of		
shaft along splines	44.983-45.000	44.965
Thickness of spline tooth	6.940-6.990	6.850
Diameter of threads for		
flance fastoning nut	MIT Y 1 G class 2	

Bevol pinion gearshaft of middle and rour axle reduction gears

*OVERTR SECOL (CHMTU TSNITCHM 974-63); hardness--HF 42-46.

13

Diameter of journal for roller bearing

49.992-50 008

49.975

Diameter of journal for bevel pinion gear Exterior diameter of	45.983-46.000	45.965
shaft along the splines for Thickness of spline	44.983-45.000	44.965
tooth Diameter of threads	6.940-6.990	6.850
for flange fastening nut	M33 X 1.5, class 2	

Bovol pinion goar

Number of toeth--11; 29Kh2N4A steel (GOST 4543-61); depth of hardened layer--1.2-1.6 mm; surface hardness--8RC 60-65; core hardness--HRC 35-45.

Diameter of journal for front tapered roller bearing inner race		
(at a length of 27 mm) Diameter of journal for rear tapered roller	60.019~60.033	60.000
bearing inner race		
(at a length of 40 mm)	59.968-59.988	59.950
Diameter of hole for		
shaft journal	46,000-46, 0 27	46.045
External dismeter of		
spline hole	45.34-45.50	45.70
Width of spline groove	7.00-7.05	7.14
Thickness of gear teeth		
(measured at height of		
10.13 mm)	11.38	11.10

Bevel pinion gear shaft flange

Type 45 steel (GOST 1050-60); depth of case hardened layer--1-2.5 mm; surface hardness--HRC 56-62.

Diameter of journal for seal	61.94-62.00	61.75
Bxternal diameter of	45.00-45.05	45.07
aplined hole Width of spline groove	7.00-7.05	7.15
Diametur of holes for bolts	14.24-14.36	15.00

Driven bevel gear

Number of teeth--19; 20Kh2N4A steel (GOST 4543-61); depth of hardened layer--1.2-1.6 mm; surface hardness--HRC 60-65; core hardness--HRC 35-45.

Diameter of journal for		
bearing	70.003-70.023	69.985
Diameter of hole for		
shaft journal	48.000-48.027	
Tooth length	33	
Gear tooth thickness		
(measured at height of		
5.24 mm)	8.52	8,25

Driving cylindrical gear

Number of teeth--12; 20KhNM steel (TU KO 8-64); depth of hardened layer--1-1.4 mm; surface hardness--HRC 60-64; core hardness--HRC 30-42.

Diameter of journal for driven bevel gear Diameter of journal for inner race of tapered	48.960-48.087	
roller bearings	39.973-39.990	39.955
Tooth length	70	
Tcoth thickness		
(measured at height of		
5.97 mm)	9.39-9.34	9.14
Diameter of threads for		
nut	M36 X 1.5, class 2	~ -

Ring goar

Number of teeth--51; 30KhGT steel (GOST 4543-61); depth of hardened rayer--1-1.4 mm; surface hardness--HRC 60-65; core hardness--HRC 35-45.

Diameter of fitting hole		
for differential box	•	
cups	190.000-190.027	
Tooth length	65	
Tooth thickness		
(measured at height of		
3.24 mm)	7.625-7.675	7.42

Differential cup

KCh 35-10 iron (GOST 1215-59).

Diameter of journal for roller bearing	70.01-70.03	69.99
Diameter of hole for		
half-shaft gear	7F 60 7F 06	96 12
journal	75 .00-75 .06	75.12
Diameter of holes for		
differential cross		
journals	28.02-28.05	28.08
Diameter of differential pinion washer spherical		
surfaces	160.7-160.9	161.4
Diameter of holes for		
tension bolts	14.24-14.36	14 , Š
	Differential cross	•_

25 KhGT steel (ChMTU TsNIIChM 761-62); depth of hardened leyer--1-1.4 mm; surface hardness--HRC 56-62.

Diameter of cross journals

28.00-28

27.98

Differential pinion

Number of teeth--11; 25 KhGT steel (ChMTU TsNII(hM 761-62); depth of nitrided layer--0.8-1.1 mm; surface hardness--HRC 58-55; core hardness--HRC 35-45.

Internal diameter of hole in pinion bushing for cross journal	28.060-28.105	28,15
Thickness of pinion		33.13
tooth (measured at height of 6.68 mm)	10.57-10.72	10.35

Haif-shaft gear

Number of teeth--22; 18KhGT steel (GOST 4543-61); depth of hardened layer--1-1.4 mm; surface hardness--HRC 56-62; core hardness--HRC 30-45.

Diameter of goar journal for hole in differential		
cup	74.895-74.935	74.75
Tooth thickness (measured		
at height of 5.1 mm)	8.65-8.50	8,25
Width of spline groove	5.367-5.452	5,65

Rear and middle drive exte half-shafts

45RP steel (VTU 1063-63); depth of case hardened layer--6 mm; surface har mess--HRC 52-62.

half-shaft length along		
the flanges:		
Laft	895	••
Right	£189	**
Spline tooth thickness	3.217-5.332	5.000
Diameter of holes for		
hab stude	12.5	13.0
Dismeter of threads in		
holes for puller		
fastezing boits	HiO, class 3	
Diameter of formal for		
sir supply head seal	52.85-53.00	52.7
Diameter of journal for		
half-shaft seal	49.9-50.0	49.7

inher half-shafts and stub saies of the front drive axie

70%hGNTR steel (ChMTU TsNIIChW 1285-6' depth of hardened layer--1.2-1.6 mm; surface hardness--HRC 58-65.

Length of stub axle to face of head Length of inner half- shaft to face of head:	238	
Right	760	
Left	590	
Diameter of inner half-		
shaft journal for seal	49.9-50.0	49.7
Diameter of stub axle journal for air supply		
head seals	52.88-53.00	52.7
Spline tooth thickness on stub axle and inner		
half-shaft External diameter of stub	5.217-5.332	5.000
axle along splines	49.950-49.975	49.90

Splined flange of front axie stub axle

40kh steel (GOST 4543-51); hardness--HB 241-269.

Diameter of centering collar for wheel hub Nidth of spline grooves along arc of divided	130.92-131.00	130.90
circumference	5.367-5.422	5. 60 0
Diameter of holes for flange fastening bolts	12.5	13.0

External diameter of splined hole

50.000-50.027

50.060

Ball joint balls

Dismeter of central ball Diameter of driving balls

41.250-41.300

42.767-42.947

Table 10-8. Diameter of half-shaft ball joint driving balls of the ZIL-131 motor vehicle, mm

Q. Frysm	b. Reserve	
. t	42,767 42,767	
11	42,787-42,807	
11.1	42,907 - 42,927	
IV	42,127-42,347	
V	42,847-42,867	
VI	42,56742,597	
VII	42,897 42,907	
VIII	47,907-42,927	
1X	42,927-42,947	

- Key: a) Group
 - b) Diameters